



SR-1447 Fracture Mechanics Characterization of Aluminum Alloys for Marine Structural Applications

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*FTA # SSC 10624-01
Contract Number: W7707-053033/001/HAL
Contract Scientific Authority: Dr. Leon Cheng, 902-427-2601
Defence Scientist, Emerging Materials Section*

The scientific or technical validity of this Contract Report is entirely the responsibility of the contractor and the contents do not necessarily have the approval or endorsement of Defence R&D Canada.

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Abstract

The Ship Structure Committee (SSC) identified a lack of information required for structural integrity and damage tolerance analyses of aluminum marine structures. The development of such data is vital in light of the increased use of aluminum alloys in marine construction. Under SSC project SR-1447, Fracture Technology Associates was contracted to characterize, through experimental fracture mechanics, the fatigue crack growth (FCG) resistance and fracture toughness of three aluminum alloys (5083, 5086, 5383) used in marine structural applications. Fatigue crack growth testing was performed following ASTM Standard E 647-00 in laboratory air at room temperature and in simulated ocean water per ASTM Standard D 1141. Non-linear fracture toughness testing was performed in accordance with ASTM Standard E 1820-01 in laboratory air at room temperature. For the three different grades of material, the difference in fatigue crack growth rate in laboratory air was negligible. In simulated seawater environment, AA5086 showed a slightly superior performance. In addition, all samples showed the same ranking of toughness with the 5086 showing the highest toughness, followed by 5083 and then 5383.

Résumé

Le Comité sur la structure des navires (CSN) a identifié des lacunes dans l'information requise pour l'analyse de l'intégrité structurale et de la tolérance aux avaries des structures maritimes en aluminium. Le développement de ces données est vital en ce sens que l'on utilise de plus en plus les alliages d'aluminium dans la construction maritime. Dans le cadre du projet SR-1447 du SSC, on a donné un contrat à la société *Fracture Technology Associates* pour qu'elle caractérise, grâce à des expériences de mécanique de la rupture, la résistance à la propagation des fissures en fatigue (PFF) et la ténacité (résistance à la propagation brutale de fissures) de trois alliages d'aluminium (5083, 5086, 5383) utilisés dans des applications structurales maritimes. Des essais sur la propagation des fissures en fatigue ont été réalisés, conformément à la norme ASTM Standard E 647-00, hors de l'eau et en laboratoire, à la température ambiante, ainsi que dans un milieu marin simulé en suivant la norme ASTM Standard D 1141. Des essais sur la résistance à la propagation de fissures non linéaires ont été réalisés, conformément à la norme ASTM Standard E 1820-01, hors de l'eau et en laboratoire, à la température ambiante. Pour les trois nuances d'alliages différentes, la différence dans le taux de propagation des fissures en laboratoire et hors de l'eau était négligeable. Dans le milieu marin simulé, l'alliage AA5086 a démontré une performance légèrement supérieure. En outre, tous les échantillons se sont situés à l'intérieur de la même plage de ténacité, l'alliage 5086 étant le plus résistant, suivi de l'alliage 5083, puis de l'alliage 5383.

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Executive summary

Introduction

As part of a Ship Structure Committee (SSC) project (Project SR-1447), Fracture Technology Associates was contracted to characterize, through experimental fracture mechanics, the fatigue crack growth (FCG) resistance and fracture toughness of three aluminum alloys (5083, 5086, 5383) used in marine structural applications. AA5083 is one of the aluminum alloys most widely used for the plate components of high-speed craft. Although 5083 performs well in its marine applications, it was not developed specifically for this environment and 5383 was specifically developed to help optimize aluminum behavior in the marine environment.

Significance

The Ship Structure Committee identified a lack of information required for structural integrity and damage tolerance analyses of aluminum marine structures. To acquire such information requires the characterization of fatigue crack growth resistance and fracture toughness through experimental fracture mechanics. The development of such data is vital in light of the increased use of aluminum alloys in marine construction.

Results

Fatigue crack growth rate and fracture toughness testing were conducted on the three grades of aluminum alloys. The fatigue crack growth testing was performed following ASTM Standard E 647-00 in laboratory air at room temperature and in simulated ocean water per ASTM Standard D 1141. Non-linear fracture toughness testing was performed in accordance with ASTM Standard E 1820-01 in laboratory air at room temperature.

For the three different grades of material, the difference in fatigue crack growth rate in laboratory air is negligible. In simulated seawater environment, AA5086 shows a slightly superior performance. In addition, all samples show the same ranking of toughness with the 5086 showing the highest toughness, followed by 5083 and then 5383.

Donald, J.K., Blair, A. 2007. SR-1447 Fracture Mechanics Characterization of Aluminum Alloys for Marine Structural Applications. DRDC Atlantic CR 2007-019. Defence R&D Canada – Atlantic.

Sommaire

Introduction

Dans le cadre d'un projet du SSC (Comité sur la structure des navires) (le projet SR-1447), on a donné un contrat à la société *Fracture Technology Associates* pour qu'elle caractérise, grâce à des expériences de mécanique de la rupture, la résistance à la propagation des fissures en fatigue (PFF) et la ténacité (résistance à la propagation brutale de fissures) de trois alliages d'aluminium (5083, 5086, 5383) utilisés dans des applications structurales maritimes. L'alliage AA5083 est l'un des alliages d'aluminium les plus couramment utilisés pour fabriquer des composants de plaques pour des embarcations rapides. Bien que l'alliage 5083 se comporte bien dans les applications maritimes, il n'a pas été mis au point spécifiquement pour ce milieu, alors que l'alliage 5383 a été spécifiquement élaboré pour optimiser le comportement de l'aluminium dans le milieu marin.

Portée

Le Comité sur la structure des navires (CSN) a identifié des lacunes dans l'information requise pour l'analyse de l'intégrité structurale et de la tolérance aux avaries des structures maritimes en aluminium. Pour obtenir ces renseignements, on doit caractériser la résistance à la propagation des fissures en fatigue (PFF) et la ténacité (résistance à la propagation brutale de fissures) par des expériences de mécanique de la rupture. L'élaboration de ces données est vitale en raison de l'utilisation de plus en plus grande des alliages d'aluminium dans la construction maritime.

Résultats

Des essais portant sur le taux de propagation des fissures en fatigue et sur la ténacité de trois nuances d'alliages d'aluminium ont été réalisés. Des essais sur la propagation des fissures en fatigue ont été réalisés, conformément à la norme ASTM Standard E 647-00, hors de l'eau et en laboratoire, à la température ambiante, ainsi que dans un milieu marin simulé en suivant la norme ASTM Standard D 1141. Des essais sur la résistance à la propagation de fissures non linéaires ont été réalisés, conformément à la norme ASTM Standard E 1820-01, hors de l'eau et en laboratoire à la température ambiante.

Pour les trois nuances d'alliages différentes, la différence dans le taux de propagation des fissures en laboratoire et hors de l'eau était négligeable. Dans le milieu marin simulé, l'alliage AA5086 a démontré une performance légèrement supérieure. En outre, tous les échantillons se sont situés à l'intérieur de la même plage de ténacité, l'alliage 5086 étant le plus résistant, suivi de l'alliage 5083, puis de l'alliage 5383.

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1. Chemistry and Mechanical Properties

1.1 Introduction

The following alloys were procured as 0.5 inch thick plates measuring 24 x 24 inches.

5083 H321 supplied as 5083 H321

5086 H116 supplied as 5086 H32 (to ASTM B209)

5383 H116 supplied as 5383/5083 H116 (to ASTM B209-01)

Dr. Harold Reemsnyder provided a detailed summary in Annex A.

Dr. Catherine Wong provided metallography analysis on the procured alloys (See Annex A).

Dirats Laboratories was contracted to provide the following services:

1. 3 chemical analysis (one for each alloy)
2. 18 tensile test results (three alloys, 2 orientations, triplicate tests)
3. 15 compact tension samples for fatigue crack growth rate testing (T-L orientation, five per alloy)
4. 9 compact tension samples for non-linear fracture toughness testing (T-L orientation, three per alloy)

1.2 Test Results

Table 1 summarizes the chemical analysis for each alloy.

Table 1. Summary of Chemical Analysis.

| Test ID | Material | Al % | Cr % | Cu % | Fe % | Mg % | Mn % | Si % | Ti % | Zn % | Zr % |
|----------|-----------|------|------|------|------|------|------|------|------|------|------|
| 5083-C-1 | 5083-H321 | Rem. | 0.08 | 0.06 | 0.31 | 4.82 | 0.50 | 0.15 | 0.03 | 0.09 | -- |
| 5086-C-1 | 5086-H116 | Rem. | 0.19 | 0.07 | 0.31 | 3.79 | 0.45 | 0.14 | 0.03 | 0.03 | -- |
| 5383-C-1 | 5383-H116 | Rem. | 0.10 | 0.06 | 0.29 | 4.76 | 0.53 | 0.13 | 0.03 | 0.08 | 0.01 |
| | | | | | | | | | | | |

Table 2 summarizes the mechanical properties for each alloy.

Table 2. Summary of Mechanical Properties.

| Test ID | Material | Orientation | 0.2% Yield Strength (ksi) | Tensile Strength (ksi) | Elongation % | Reduction of Area % |
|--------------------------------------|-----------|-------------|---------------------------|------------------------|--------------|---------------------|
| 5083-L-1 | 5083-H321 | L | 37.8 | 52.3 | 12.1 | 21.1 |
| 5083-L-2 | 5083-H321 | L | 37.8 | 53.0 | 14.3 | 20.5 |
| 5083-L-3 | 5083-H321 | L | 38.2 | 52.8 | 16.8 | 22.4 |
| Average | | | 37.9 | 52.7 | 14.4 | 21.3 |
| | | | | | | |
| 5083-T-1 | 5083-H321 | T | 34.3 | 52.0 | 21.5 | 36.9 |
| 5083-T-2 | 5083-H321 | T | 34.4 | 51.6 | 19.0 | 34.6 |
| 5083-T-3 | 5083-H321 | T | 34.3 | 51.8 | 18.4 | 36.8 |
| Average | | | 34.3 | 51.8 | 19.6 | 36.1 |
| | | | | | | |
| | | | | | | |
| 5086-L-1 | 5086-H116 | L | 27.0 | 45.8 | 14.8 | 17.4 |
| 5086-L-2 | 5086-H116 | L | 26.9 | 45.7 | 15.1 | 16.8 |
| 5086-L-3 | 5086-H116 | L | 27.0 | 46.0 | 15.3 | 16.1 |
| Average | | | 27.0 | 45.8 | 15.1 | 16.8 |
| | | | | | | |
| 5086-T-1 | 5086-H116 | T | 27.0 | 45.7 | 17.1 | 27.4 |
| 5086-T-2 | 5086-H116 | T | 26.9 | 46.2 | 21.1 | 36.6 |
| 5086-T-3 | 5086-H116 | T | 27.1 | 46.1 | 19.9 | 38.7 |
| Average | | | 27.0 | 46.0 | 19.4 | 34.2 |
| | | | | | | |
| | | | | | | |
| 5383-L-1 | 5383-H116 | L | 39.3 | 54.4 | 14.1 | 16.2 |
| 5383-L-2 | 5383-H116 | L | 39.2 | 54.1 | 14.4 | 17.2 |
| 5383-L-3 | 5383-H116 | L | 39.0 | 54.0 | 12.9 | 15.6 |
| Average | | | 39.2 | 54.2 | 13.8 | 16.3 |
| | | | | | | |
| 5383-T-1 | 5383-H116 | T | 35.4 | 53.0 | 17.5 | 35.0 |
| 5383-T-2 | 5383-H116 | T | 35.4 | 53.5 | 16.4 | 24.8 |
| 5383-T-3 | 5383-H116 | T | 35.5 | 53.3 | 18.1 | 23.3 |
| Average | | | 35.4 | 53.3 | 17.3 | 27.7 |
| Temperature: Room Temperature | | | | | | |

2. Fatigue Crack Growth Rate Characterization

2.1 Introduction

Fatigue crack growth rate (FCGR) testing was conducted on three grades of aluminum alloys designated 5083-H321, 5086-H116 and 5383-H116. A compact tension sample having a width of 4.000 inches and a thickness of 0.500 inches was chosen for all FCGR testing. For each grade of material, two replicate tests were conducted in laboratory air at room temperature and two replicate tests were conducted in simulated ocean water per ASTM Standard D 1141. All samples were machined in the T-L orientation and all testing was conducted using a stress ratio (R) of 0.1. A baseline test frequency of 10 Hz was selected for the laboratory air tests with a baseline frequency of 5 Hz selected for the tests conducted in seawater. Some data were generated in seawater at 0.5 and 0.05 Hz to evaluate frequency sensitivity. The testing was performed in accordance with the requirements of ASTM E647-00 "Standard Test Method for Fatigue Crack Growth Rates". Background information on the methodology for testing and analysis is given in Annex B.

2.2 Test Equipment

The tests were conducted on two MTS load frames equipped with a 5,000 lbf load cell. Each test frame and controller was interfaced to an Adwin-Gold FTA computer system. The crack length was monitored continuously using the compliance technique enabling the stress intensity to be precisely controlled as a function of crack length. An MTS model 632.03E-20 clip gage with a gage length of 0.475 inches and a working range of 0.100 inches was used for displacement measurement. Fixture alignment was verified for the compact tension clevises by applying a force on a dummy sample and measuring the distance between the loading pins on the front face and back face of the clevis. If the spacing differed by more than 0.001 inches, the clevises were shimmed to bring that difference to within tolerance. Compliance measurement accuracy was enhanced by mounting needle bearings in both the clevis holes and the specimen holes to minimize non-linearity in the load-displacement signal due to pin friction. In addition to improving the accuracy of crack growth measurements, this procedure is considered essential for accurate crack closure measurement. Laboratory temperature and relative humidity were controlled to 75°F \pm 2°F and 40% \pm 5% R.H. throughout the entire period of testing. Photographs of the test equipment and a close-up of a compact tension sample and test fixtures are shown in Figure 1.

For the synthetic seawater environment, one gallon of distilled water was combined with a sea-salt mix according to the ASTM D 1141 standard. A peristaltic pump was used to aerate the solution and transfer the environment to the test sample. Custom made clear plastic environment chambers were attached to the test sample with silicon

adhesive. These chambers were attached to the sample 24 hours prior to testing to allow a complete cure of the adhesive. A small hole was drilled in the notch to provide flow from one side of the sample to the other. A larger hole was also drilled in the notch and filled with sealant to provide a water-tight seal. The set-up included an air bleed so that the crack remained fully immersed in solution during the entire test. pH readings were recorded daily with a typical range of 8.4 to 7.8. Photographs of the test set-up for the seawater environment are shown in Figure 2.

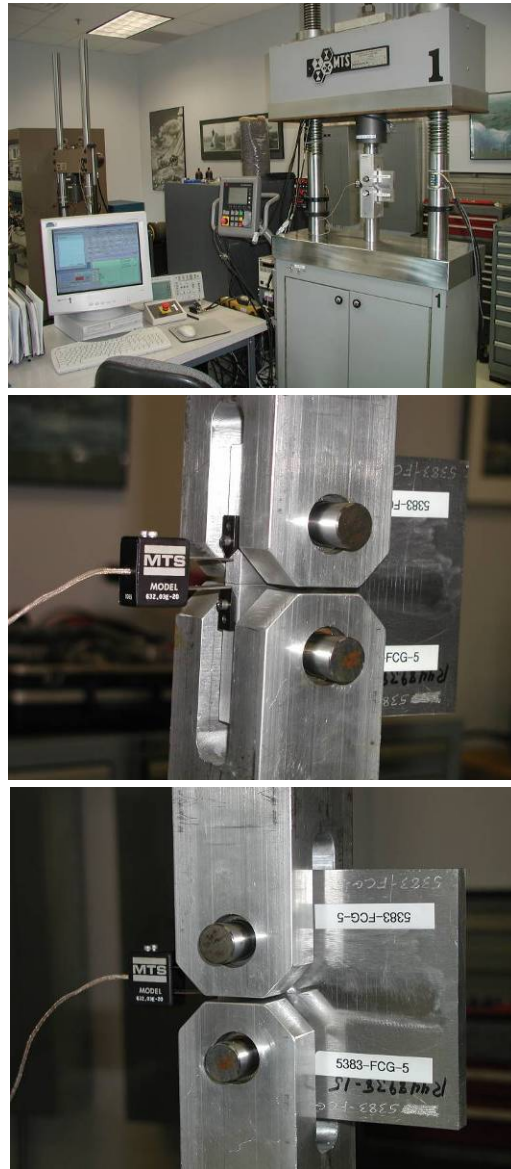


Figure 1. Photographs of test equipment and test set-up (laboratory air environment).



Figure 2. Photographs of test equipment and test set-up (seawater environment).

2.3 Sample Preparation

The test samples were machined according to Figure 3. After machining the blanks to the final dimensions, but before machining the notch, reference scribes were placed on the edge of the sample spanning the location of the notch. The distance between these scribes was measured to a precision of ± 0.0001 inches, both before and after machining the notch. This information was used to estimate the magnitude of residual

K at the notch tip due to residual stress. A summary of these calculations is shown in Table 3 (Section 2.5).

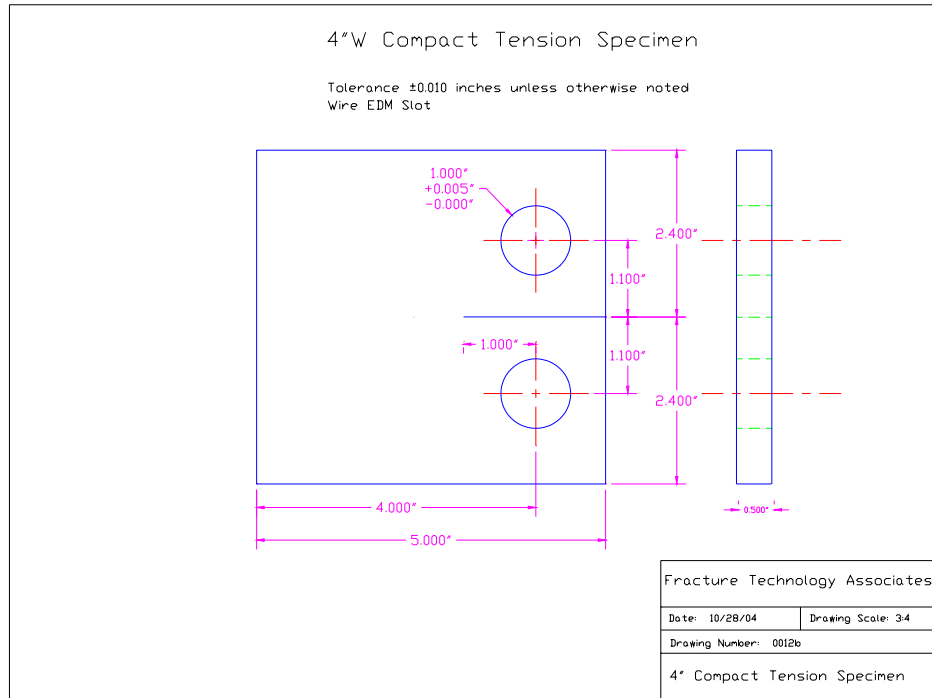


Figure 3. Diagram of C(T) sample for fatigue crack growth testing (diagram reproduction not to scale).

2.4 Test Procedure

The pre-cracking was initiated at low values of K_{\max} ($\sim 4 \text{ ksi}\sqrt{\text{in}}$) in order to initiate a crack at low growth rates. Once initiation was detected and crack evenness was verified, the pre-cracking was continued using a decreasing K-gradient of -4.0 1/inch until a crack growth rate of $\sim 8 \times 10^{-8} \text{ inch/cycle}$ was achieved. At the completion of pre-cracking, the test was switched to an increasing K-gradient of $+4.0 \text{ 1/inch}$ and continued at that K-gradient until a crack growth rate of $1 \times 10^{-5} \text{ inch/cycle}$. A shallower K-gradient of $+2.0 \text{ 1/in}$ was selected for upper region II (up to $1 \times 10^{-4} \text{ inch/cycle}$). Region III crack growth rate data were generated under constant amplitude loading.

Periodic visual measurements of the crack length from each surface were recorded. These measurements, along with the corresponding normalized compliance ($E\nu B/P$), were entered into the post-test analysis software to correct for any discrepancy between the physical crack length and the compliance calculated crack length. The

cover page of each test (Annex E) includes a summary of errors between the physical and compliance calculated crack length as well as an adjustment factor (CAF) to the modulus of elasticity to minimize these errors. Compliance coefficients were selected from the ASTM E647 standard based on a clip gage location at the edge of the sample.

For the near-threshold tests, crack growth rate data were generated using a decreasing K-gradient of -4.0 1/inch and continued until crack growth rates were less than $\sim 4 \times 10^{-9}$ inch/cycle. After establishing threshold, the tests were continued using an increasing K-gradient of +4.0 1/inch and continued at that K-gradient until a crack growth rate of 1×10^{-5} inch/cycle. Both decreasing and increasing K data were generated in laboratory air at a cyclic test frequency of 24 Hz.

During testing, the FTA testing software calculated the effective stress intensity according to the ASTM opening load method. However, another methodology for determining the effective stress intensity was also used and is called the adjusted compliance ratio (ACR) method. Crack growth rates are computed using a combination of the modified secant method and the seven point incremental polynomial technique. The first method is computed as follows:

$$da/dN = (a_{i+2} - a_i) / (N_{i+2} - N_i) \quad (1)$$

and

$$a_{\text{average}} = (a_{i+2} + a_i) / 2 \quad (2)$$

The second method is thoroughly described in Appendix X1 of ASTM E647. This method smoothes the data but misses three points at the beginning and three points at the end of the data set. The combined methods use the seven-point method for the bulk of the data with the modified secant method used for the “missed” points in the beginning and end of the data set.

2.5 Test Results and Discussion

Table 3 summarizes the calculation of K residual at the notch tip using the restoring force model. Table 4 summarizes key test conditions and the cyclic stress intensity at threshold (ΔK_{th}). Threshold determinations were made by applying the data fit as per ASTM E647.

The results of the K residual evaluation (Table 3) showed mostly tensile residual stress at the notch tip. However, the magnitude of the residual stress was small so no attempt was made to account for residual stress in the analysis.

All samples met the crack front evenness requirement according to ASTM E647. All other validity requirements were satisfied as well.

The following files are available.

***.dat files:**

This file is produced by the analysis software and can be exported to Excel or Grapher for plotting or further analysis. For each data point, the following variables are tabulated:

| <u>Description</u> | <u>Units</u> |
|---|---------------------------|
| Index number | |
| Maximum force | (lbf) |
| Cyclic force | (lbf) |
| Normalized compliance | (EvB/P) |
| Crack length | (in) |
| Cycle count | |
| Crack growth rate | (inch/cycle) |
| K_{\max} | (ksi $\sqrt{\text{in}}$) |
| $\Delta K_{\text{applied}}$ | (ksi $\sqrt{\text{in}}$) |
| $\Delta K_{\text{effective}}$ (2% offset opening load method) | (ksi $\sqrt{\text{in}}$) |
| $\Delta K_{\text{effective}}$ (ACR method) | (ksi $\sqrt{\text{in}}$) |
| $\Delta K_{\text{effective}}$ ($2/\pi$ partial closure method) | (ksi $\sqrt{\text{in}}$) |

***.prn files:**

These files include tabular results and additional information such as sample dimensions and visual observation (Annex E).

Table 3. Estimation of K Residual Using Restoring Force Model.

| Test ID | Notch Mouth Displacement Change (inches) | K_{residual} (ksi√in) |
|---------|--|-----------------------------------|
| 5083-1 | +0.0002 | +0.12 |
| 5083-2 | +0.0001 | +0.06 |
| 5083-3 | +0.0004 | +0.24 |
| 5083-4 | +0.0004 | +0.24 |
| 5083-5 | +0.0001 | +0.06 |
| 5086-1 | +0.0002 | +0.12 |
| 5086-2 | +0.0000 | +0.00 |
| 5086-3 | +0.0002 | +0.12 |
| 5086-4 | +0.0001 | +0.06 |
| 5086-5 | +0.0000 | +0.00 |
| 5383-1 | +0.0000 | +0.00 |
| 5383-2 | +0.0001 | +0.06 |
| 5383-3 | +0.0000 | +0.00 |
| 5383-4 | -0.0001 | -0.06 |
| 5383-5 | +0.0001 | +0.06 |

Table 4. Summary of Fatigue Crack Growth Test Conditions and Results (Temperature: 75°F, Stress Ratio: 0.1, Orientation: T-L).

| Test ID | Material | Environment | K-Gradient (1/in) | Frequency (Hz) | ΔK_{th} (ksi \sqrt{in}) |
|---------|-----------|-------------|----------------------|-------------------|---------------------------------------|
| 5083-1B | 5083-H321 | Air | +4.0 | 10.0 | -- |
| 5083-1C | 5083-H321 | Air | +2.0 | 10.0 | -- |
| 5083-1D | 5083-H321 | Air | Constant Load | 5.0 | -- |
| 5083-2B | 5083-H321 | Air | +4.0 | 10.0 | -- |
| 5083-2C | 5083-H321 | Air | +2.0 | 10.0 | -- |
| 5083-2D | 5083-H321 | Air | Constant Load | 5.0 | -- |
| 5083-3B | 5083-H321 | Seawater | +4.0 | 5.0 | -- |
| 5083-3C | 5083-H321 | Seawater | +2.0 | 5.0 | -- |
| 5083-3D | 5083-H321 | Seawater | Constant Load | 5.0 | -- |
| 5083-4B | 5083-H321 | Seawater | +4.0 | 5.0, 0.5 | -- |
| 5083-4C | 5083-H321 | Seawater | +2.0 | 5.0, 0.5, 0.05 | -- |
| 5083-4D | 5083-H321 | Seawater | Constant Load | 5.0, 0.5, 0.05 | -- |
| 5083-5A | 5083-H321 | Air | -4.0 | 24.0 | 2.64 |
| 5083-5B | 5083-H321 | Air | +4.0 | 24.0 | -- |
| 5086-1B | 5086-H116 | Air | +4.0 | 10.0 | -- |
| 5086-1C | 5086-H116 | Air | +2.0 | 10.0 | -- |
| 5086-1D | 5086-H116 | Air | Constant Load | 5.0 | -- |
| 5086-2B | 5086-H116 | Air | +4.0 | 10.0 | -- |
| 5086-2C | 5086-H116 | Air | +2.0 | 10.0 | -- |
| 5086-2D | 5086-H116 | Air | Constant Load | 5.0 | -- |
| 5086-3B | 5086-H116 | Seawater | +4.0 | 5.0 | -- |
| 5086-3C | 5086-H116 | Seawater | +2.0 | 5.0 | -- |
| 5086-3D | 5086-H116 | Seawater | Constant Load | 5.0 | -- |

Table 4. Summary of Fatigue Crack Growth Test Conditions and Results (continued).

| Test ID | Material | Environment | K-Gradient (1/in) | Frequency (Hz) | ΔK_{th} (ksi \sqrt{in}) |
|---------|-----------|-------------|----------------------|-------------------|---------------------------------------|
| 5086-4B | 5086-H116 | Seawater | +4.0 | 5.0, 0.5 | -- |
| 5086-4C | 5086-H116 | Seawater | +2.0 | 5.0, 0.5, 0.05 | -- |
| 5086-4D | 5086-H116 | Seawater | Constant Load | 5.0, 0.5, 0.05 | -- |
| 5086-5A | 5086-H116 | Air | -4.0 | 24.0 | 3.01 |
| 5086-5B | 5086-H116 | Air | +4.0 | 24.0 | -- |
| 5383-1B | 5383-H116 | Air | +4.0 | 10.0 | -- |
| 5383-1C | 5383-H116 | Air | +2.0 | 10.0 | -- |
| 5383-1D | 5383-H116 | Air | Constant Load | 5.0 | -- |
| 5383-2B | 5383-H116 | Air | +4.0 | 10.0 | -- |
| 5383-2C | 5383-H116 | Air | +2.0 | 10.0 | -- |
| 5383-2D | 5383-H116 | Air | Constant Load | 5.0 | -- |
| 5383-3B | 5383-H116 | Seawater | +4.0 | 5.0 | -- |
| 5383-3C | 5383-H116 | Seawater | +2.0 | 5.0 | -- |
| 5383-3D | 5383-H116 | Seawater | Constant Load | 5.0 | -- |
| 5383-4B | 5383-H116 | Seawater | +4.0 | 5.0, 0.5 | -- |
| 5383-4C | 5383-H116 | Seawater | +2.0 | 5.0, 0.5, 0.05 | -- |
| 5383-4D | 5383-H116 | Seawater | Constant Load | 5.0, 0.5, 0.05 | -- |
| 5383-5A | 5383-H116 | Air | -4.0 | 24.0 | 2.67 |
| 5383-5B | 5383-H116 | Air | +4.0 | 24.0 | -- |

A series of plots have been prepared to facilitate the investigation of reproducibility, environment, material, frequency, threshold and crack closure.

2.5.1 Reproducibility

Figures 4 through 9 show duplicate test results in both laboratory air and seawater for each grade of material. Agreement is excellent within identical test conditions. For simplicity, the comparisons among the various materials, environments, etc. are made with only one of the duplicate tests.

Fatigue Crack Growth Rate vs. Stress Intensity

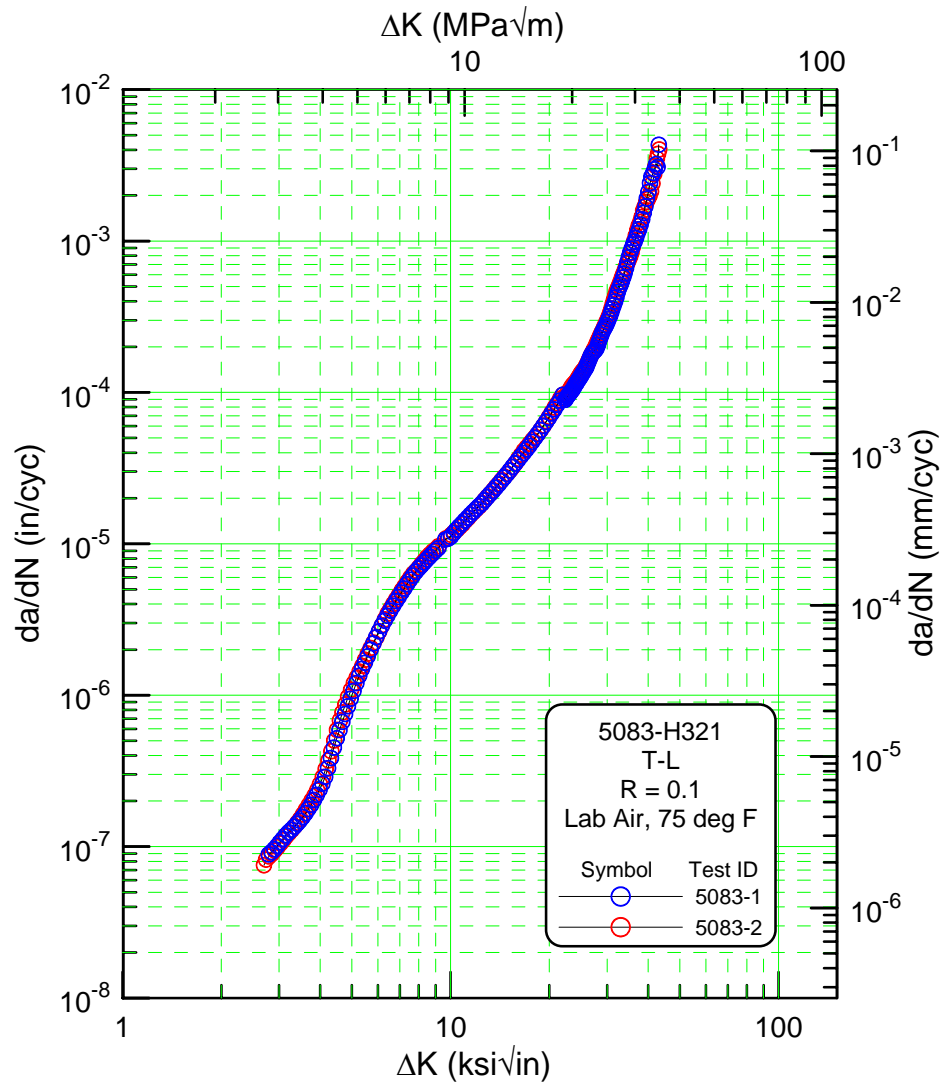


Figure 4. FCGR response comparing duplicate tests for the 5083-H321 alloy in laboratory air.

Fatigue Crack Growth Rate vs. Stress Intensity

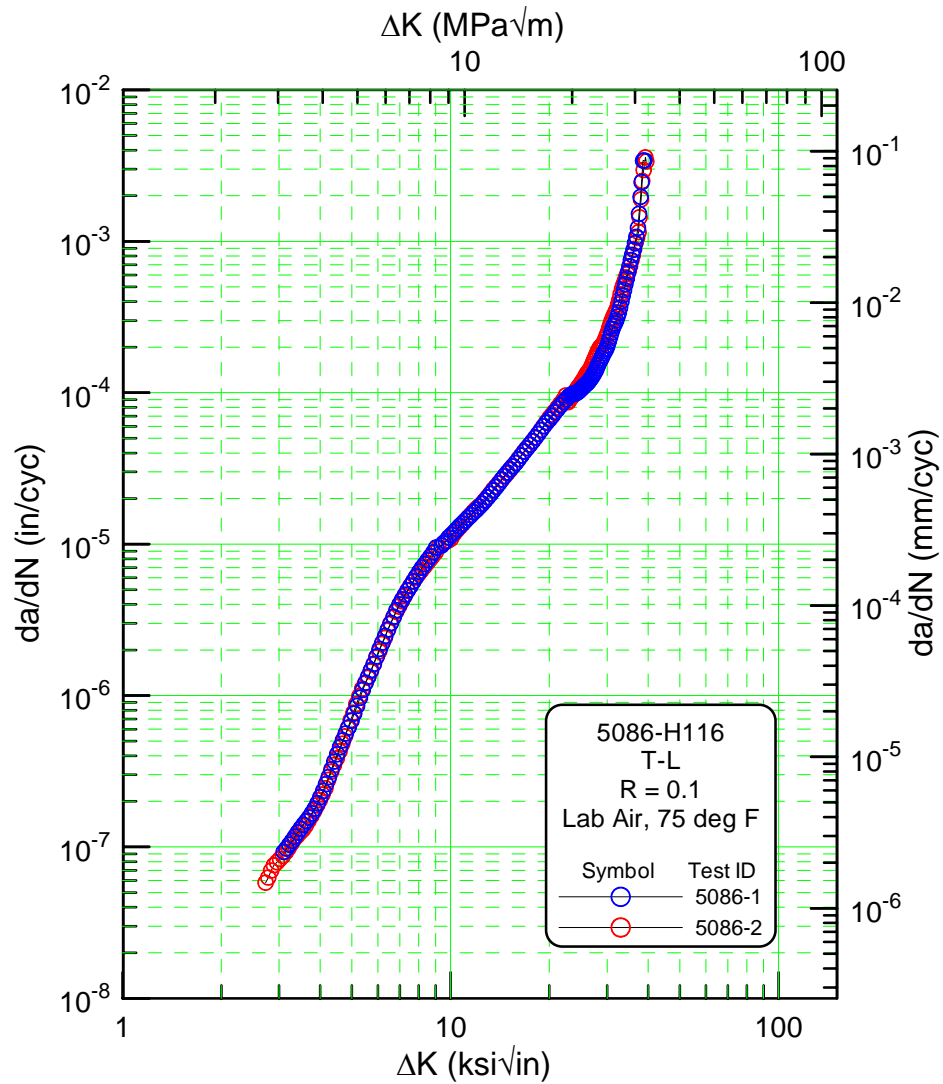


Figure 5. FCGR response comparing duplicate tests for the 5086-H116 alloy in laboratory air.

Fatigue Crack Growth Rate vs. Stress Intensity

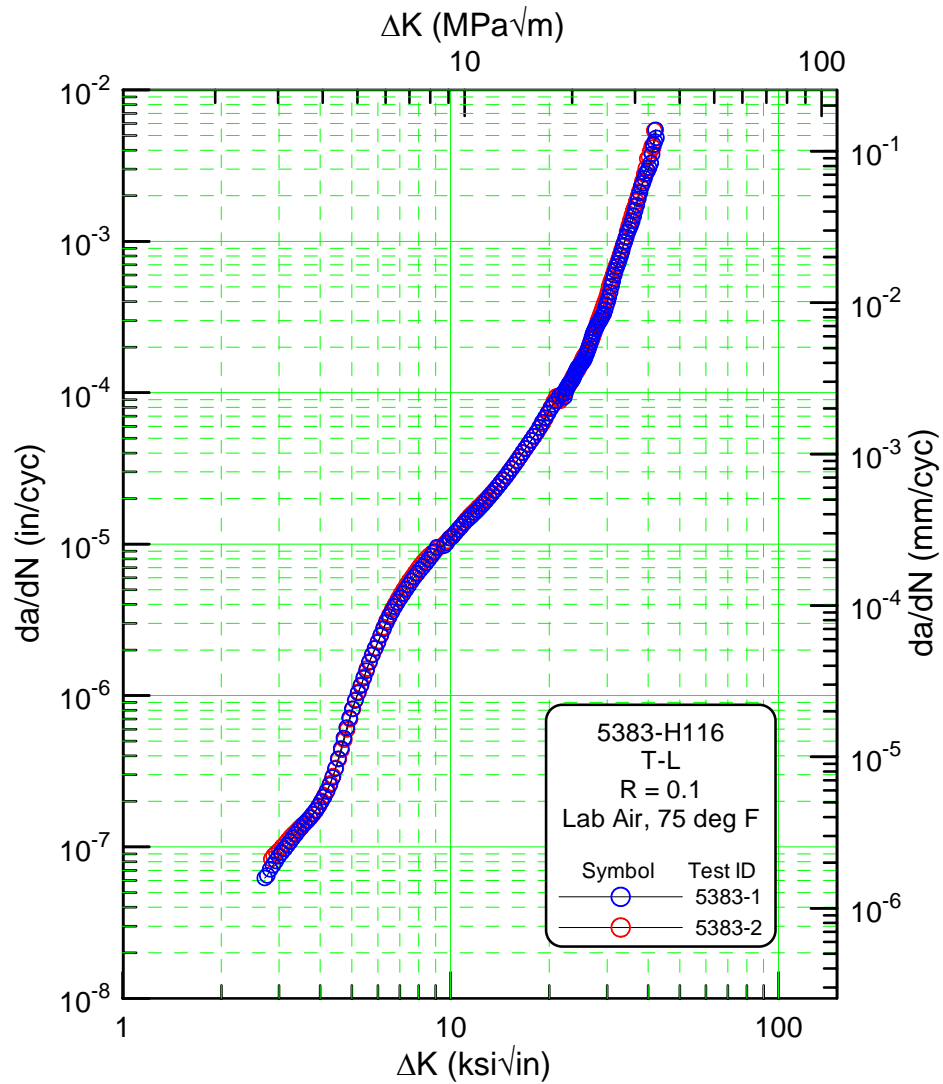


Figure 6. FCGR response comparing duplicate tests for the 5383-H116 alloy in laboratory air.

Fatigue Crack Growth Rate vs. Stress Intensity

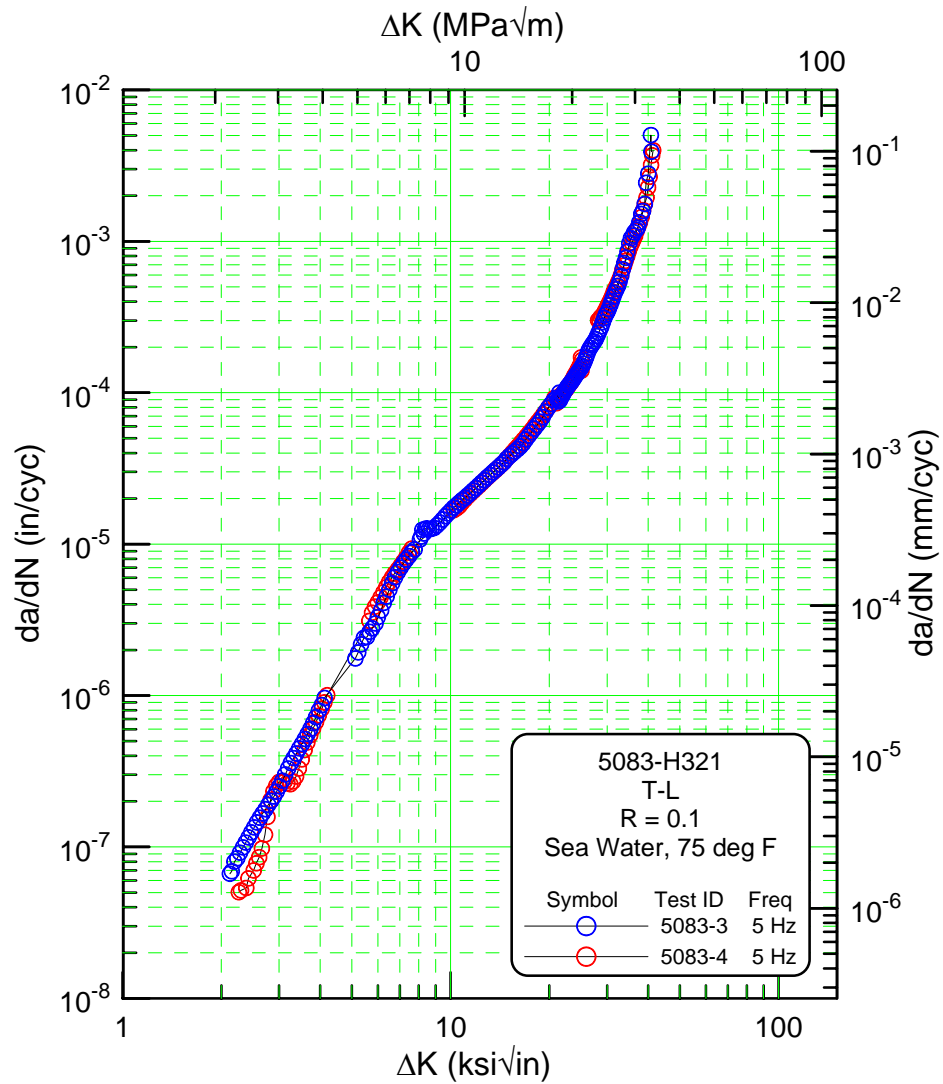


Figure 7. FCGR response comparing duplicate tests for the 5083-H321 alloy in seawater.

Fatigue Crack Growth Rate vs. Stress Intensity

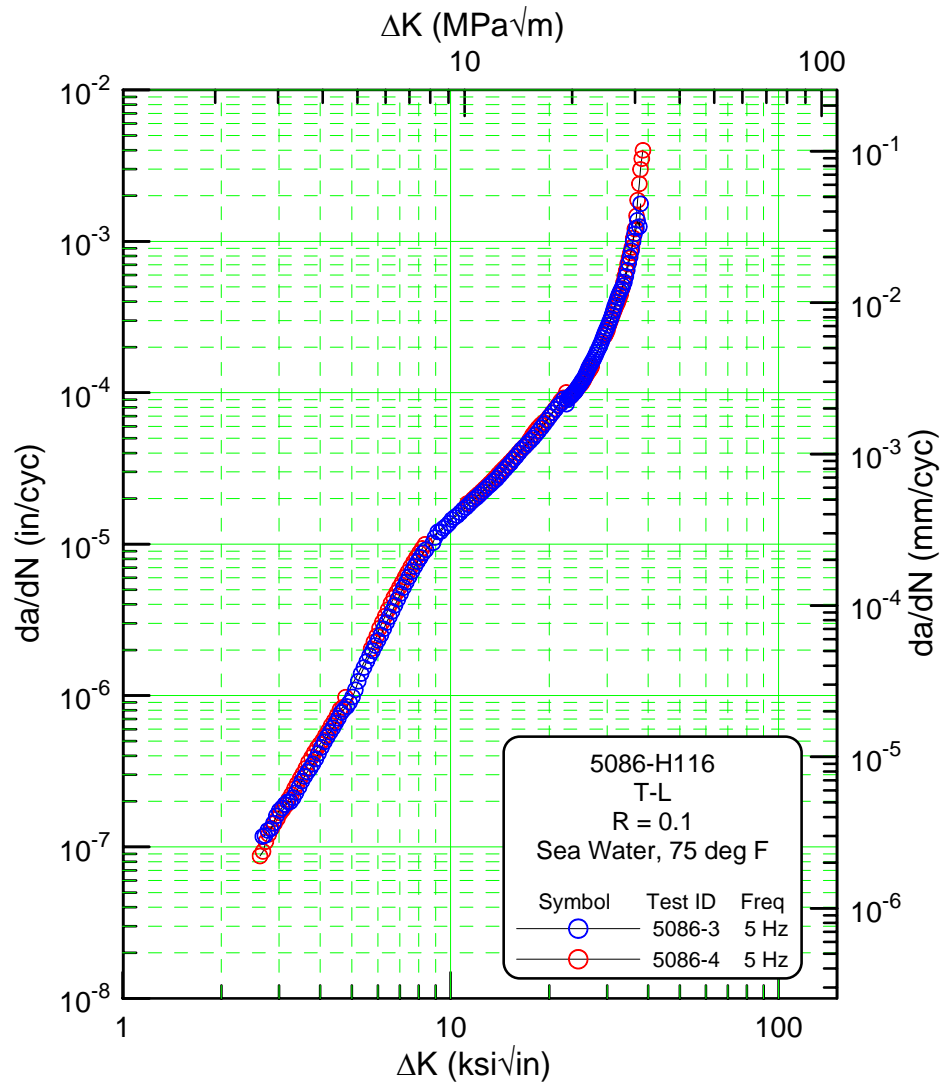


Figure 8. FCGR response comparing duplicate tests for the 5086-H116 alloy in seawater.

Fatigue Crack Growth Rate vs. Stress Intensity

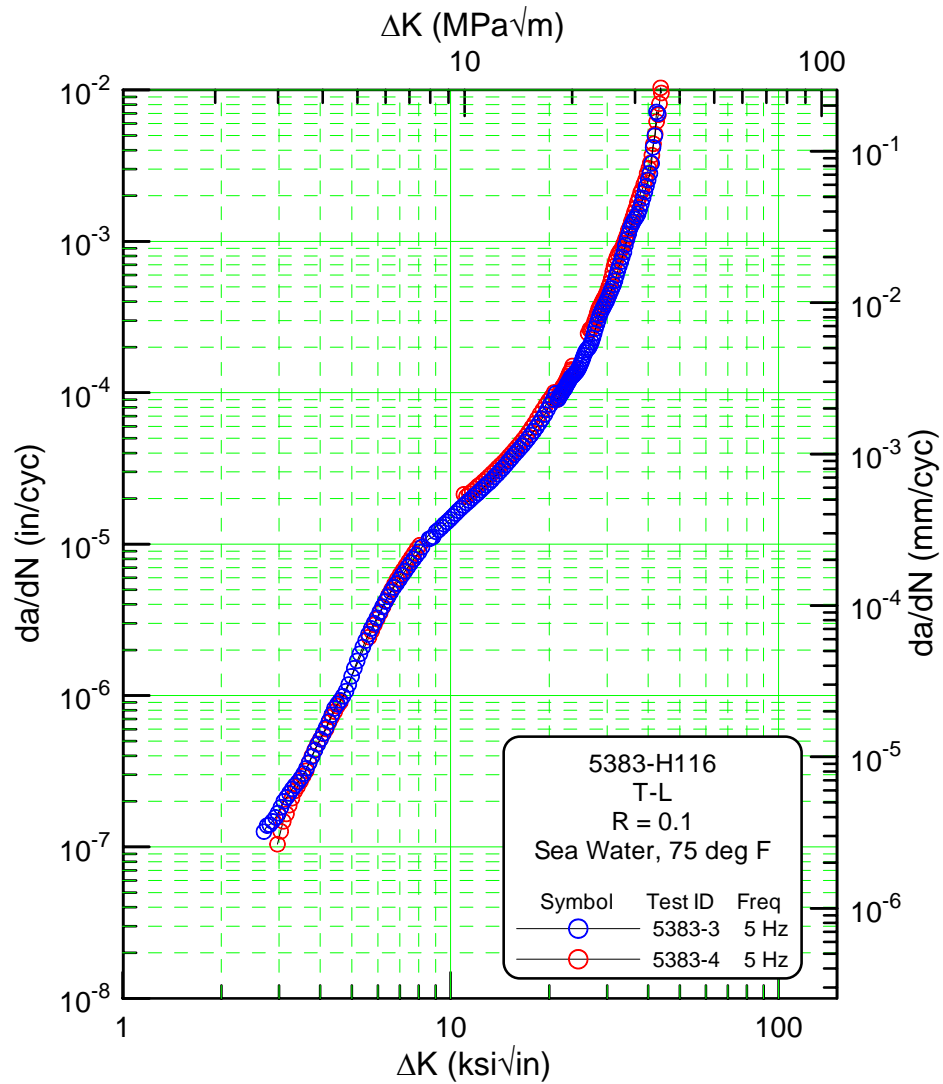


Figure 9. FCGR response comparing duplicate tests for the 5383-H116 alloy in seawater.

2.5.2 Effect of Environment

Figures 10 through 12 show the effect of environment for each grade of material. The impact is greater at lower growth rates. The crack growth rates may be too fast at the higher growth rates for significant environmental effects. It appears that the environmental effect is greater with the 5083-H321 and 5383-H116 alloys.

Fatigue Crack Growth Rate vs. Stress Intensity

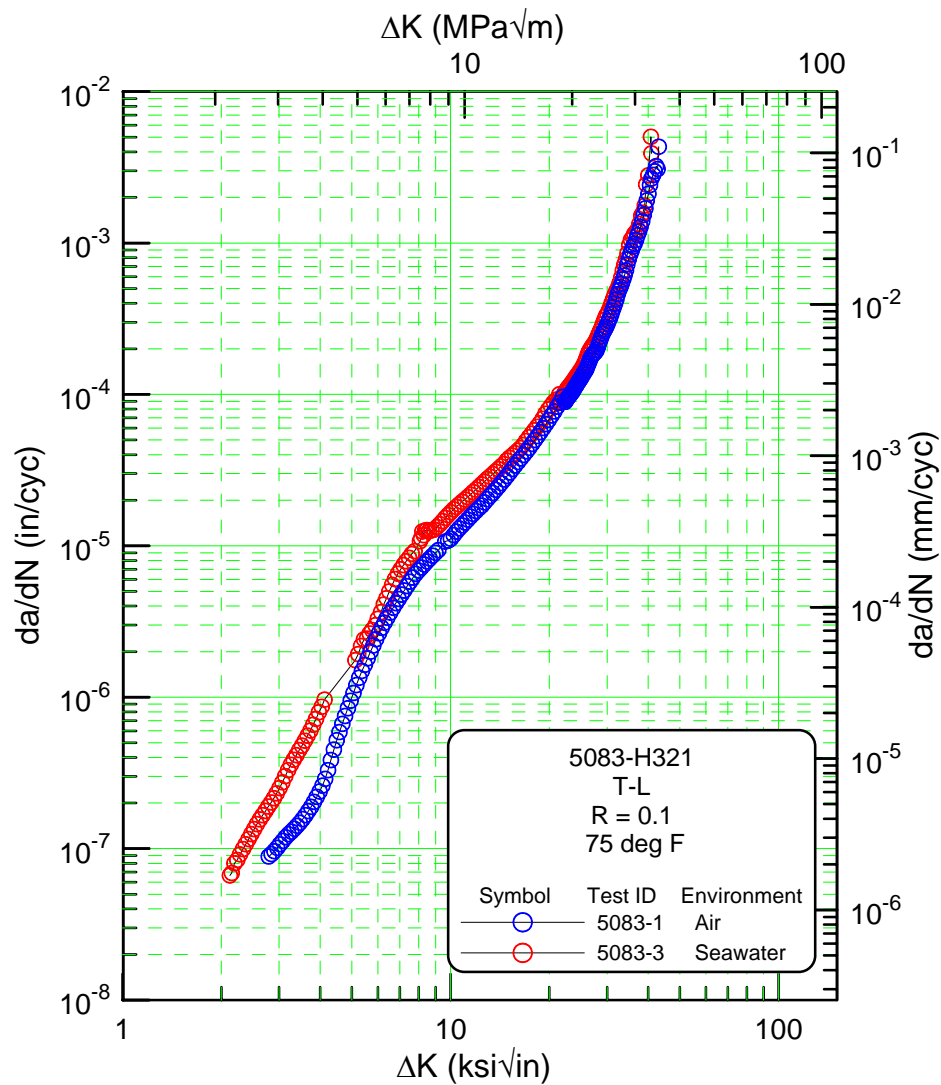


Figure 10. FCGR response showing the effect of environment for the 5083-H321 alloy.

Fatigue Crack Growth Rate vs. Stress Intensity

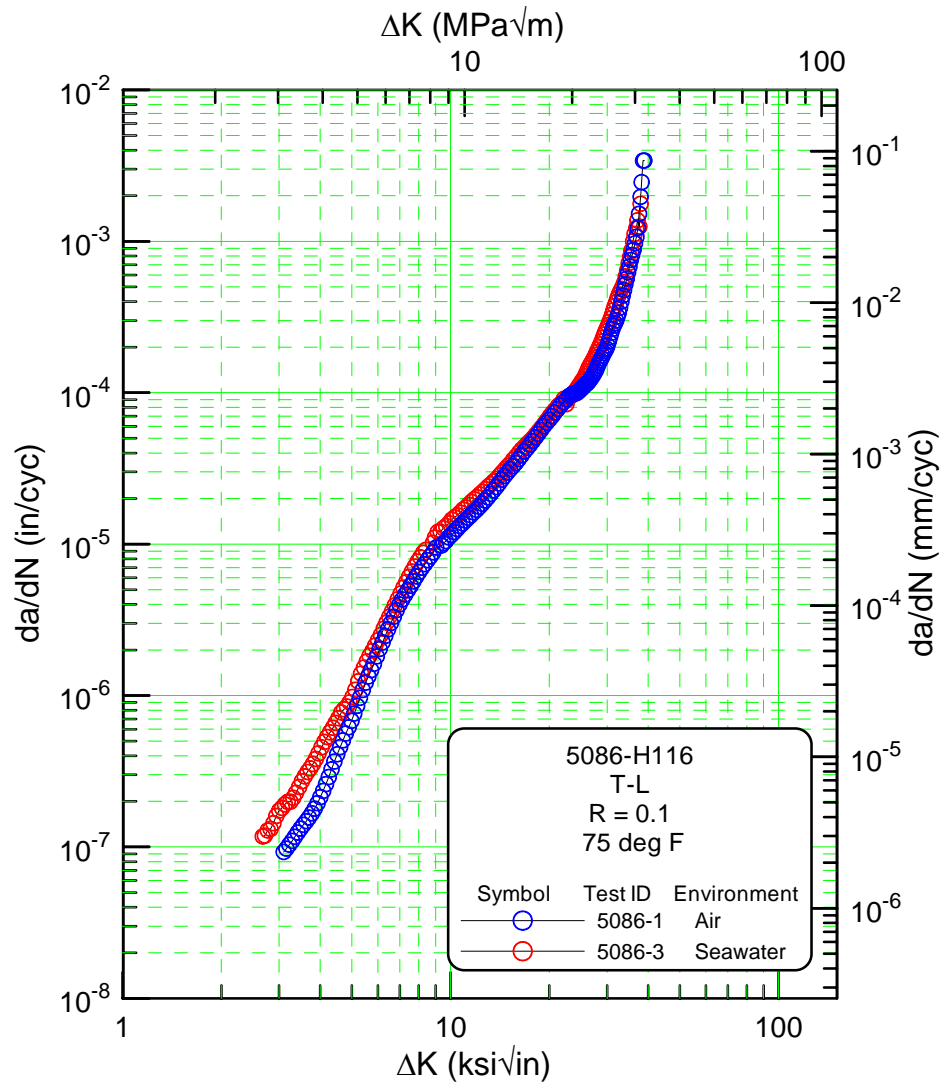


Figure 11. FCGR response showing the effect of environment for the 5086-H116 alloy.

Fatigue Crack Growth Rate vs. Stress Intensity

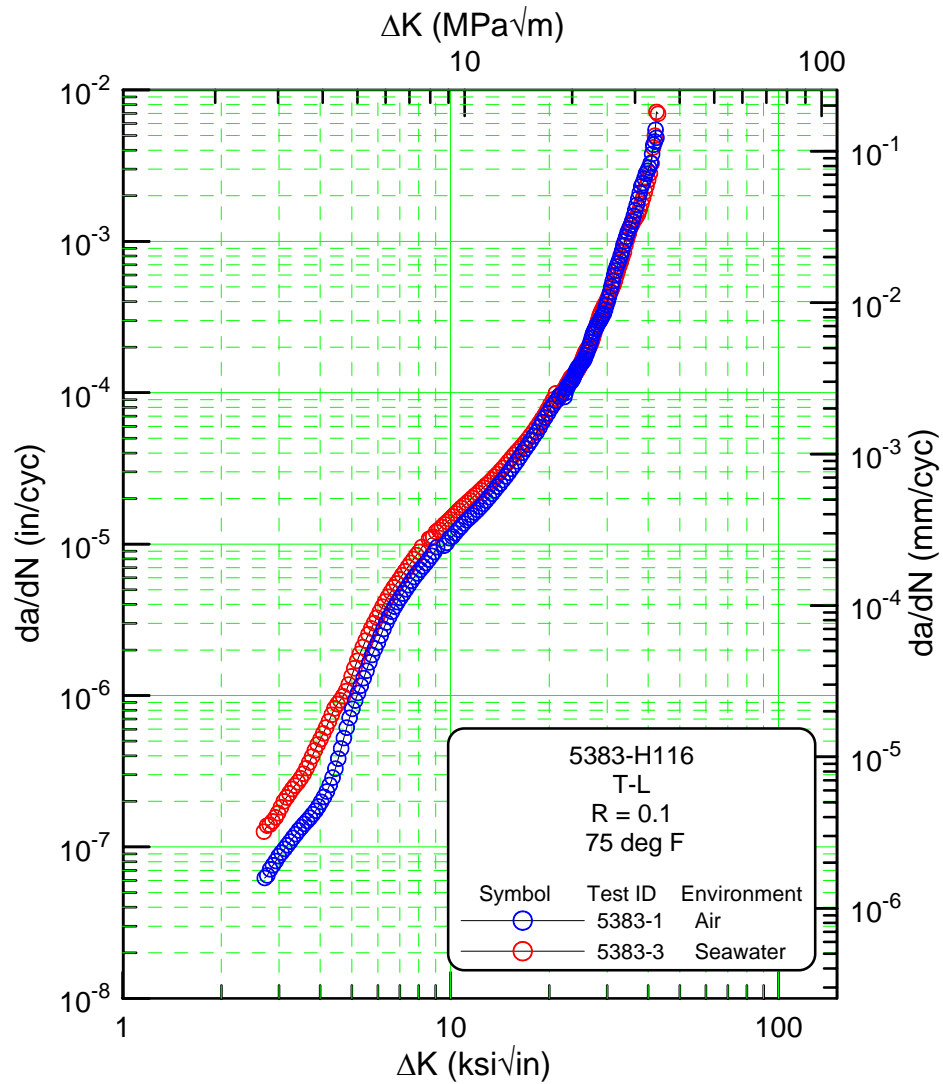


Figure 12. FCGR response showing the effect of environment for the 5383-H116 alloy.

2.5.3 Effect of Material

Figures 13 and 14 show the effect of the grade of material in laboratory air and seawater, respectively. The difference in laboratory air is negligible (Figure 13). Figure 14 shows slightly superior performance with the 5086-H116 alloy.

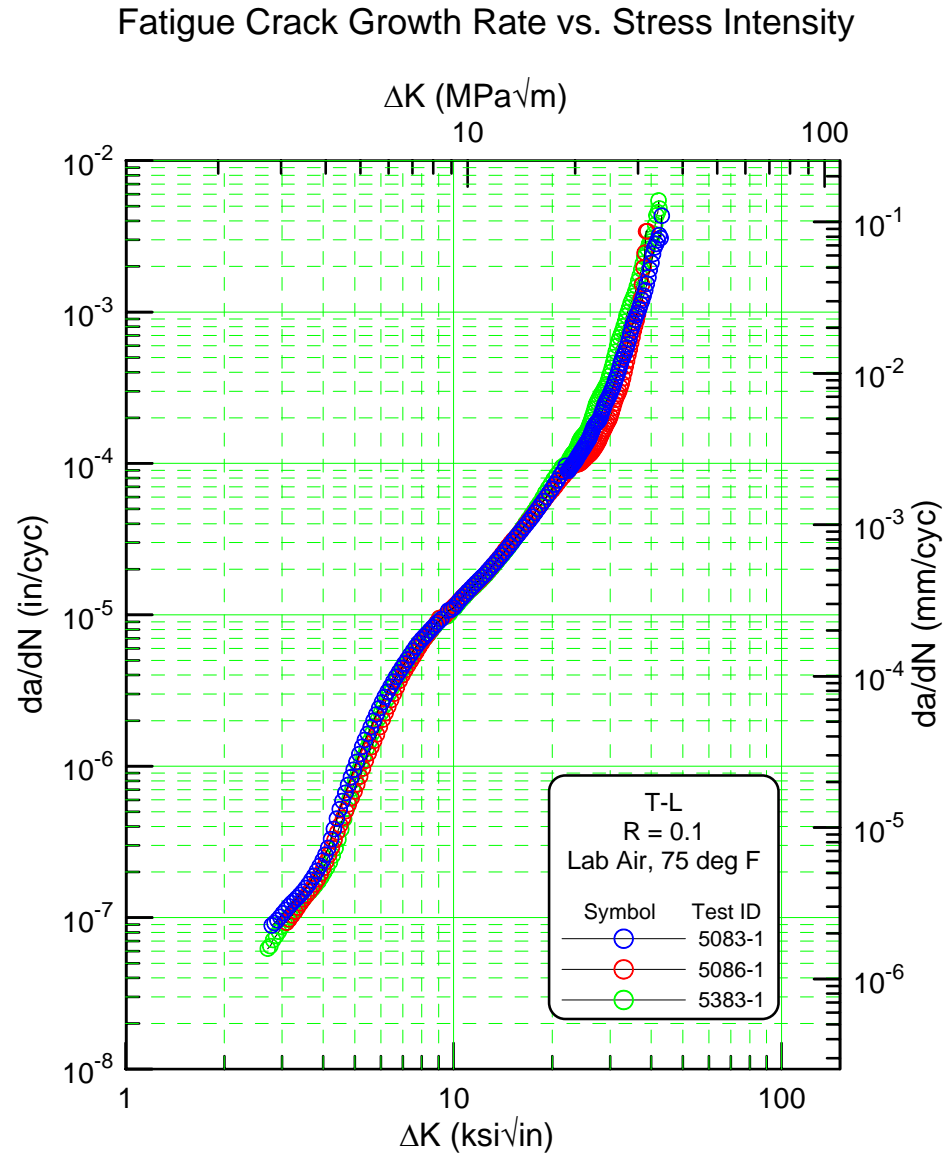


Figure 13. FCGR response showing the effect of the grade of material in laboratory air.

Fatigue Crack Growth Rate vs. Stress Intensity

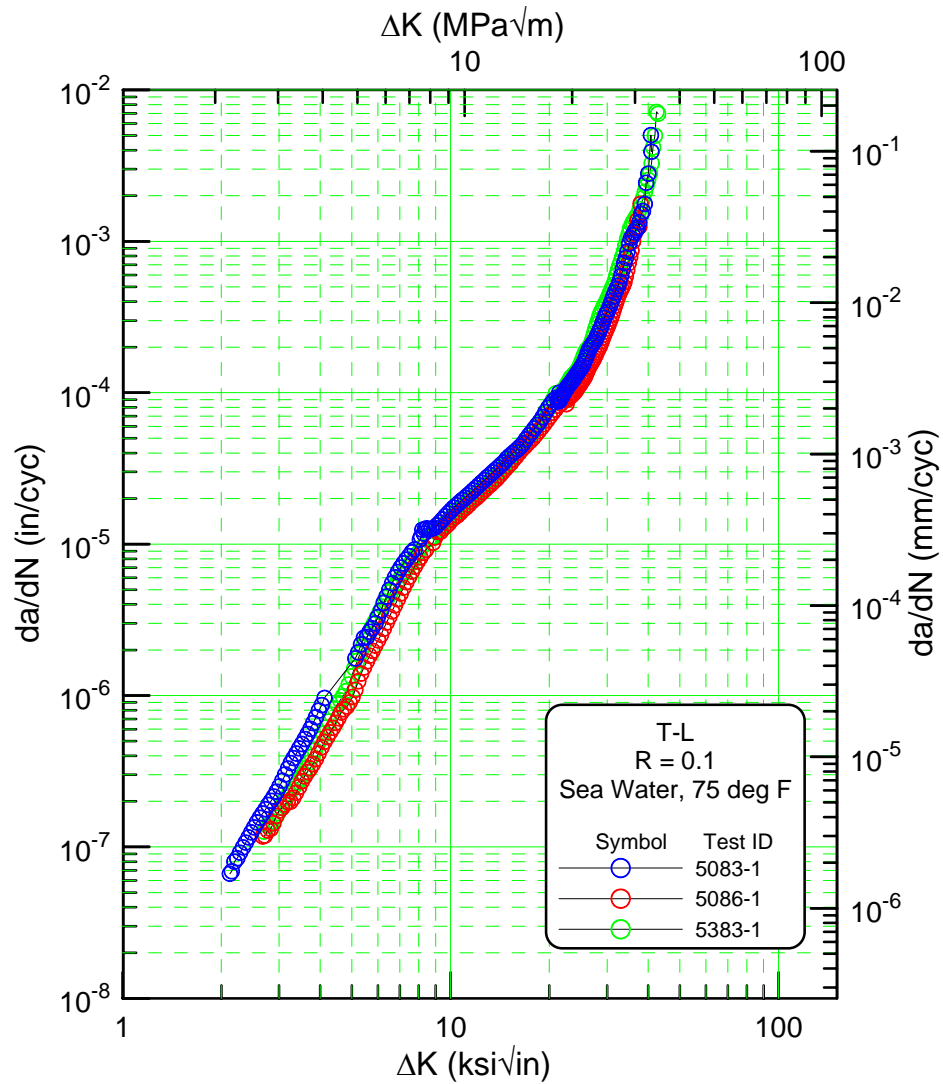


Figure 14. FCGR response showing the effect of the grade of material in seawater.

2.5.4 Effect of Frequency

In order to assess the effect of frequency on the FCGR tests conducted in seawater, one sample of each grade of material was tested at three different frequencies (5.0 Hz, 0.5Hz and 0.05Hz). At a frequency of 0.05 Hz, both a sinusoidal waveform shape and a hold at maximum load were investigated. For the dwell segment, the waveform consisted of an unload in 1 second, a reload in 1 second followed by a hold at maximum load for 18 seconds. Figures 15 through 17 show the effect of the frequency for each grade of material in seawater. The effect of frequency was investigated at crack growth rates of $\sim 1-2 \times 10^{-6}$, $\sim 1-2 \times 10^{-5}$, and $\sim 1-2 \times 10^{-4}$ inch/cycle. Almost no frequency effect was observed despite a change of two orders of magnitude in frequency. In fact, at growth rates of $\sim 1-2 \times 10^{-5}$ the crack growth rates at 0.05 Hz appeared to be slower, not faster, as would be expected. This behavior suggests that these alloys are fairly resistant to corrosion fatigue in seawater.

2.5.5 Threshold Behavior

Figure 18 shows a comparison of the threshold data for each grade of material. Good agreement was noted where the decreasing and increasing K data overlap. The increasing K data are in good agreement with the previous test data in laboratory air. However, the decreasing K threshold data appear higher than would have been expected from the results of the standard increasing K tests. An examination of the threshold fatigue surfaces indicates darker appearance, most likely associated with crack closure contact. The size of the sample and the long crack length are not generally recommended for threshold testing and this may in part explain some of the deviation in behavior just above the knee of the curve. This difference is clearly illustrated in Figures 19 through 21.

2.5.6 Effect of Crack Closure

In order to properly interpret the results of standard fatigue crack growth tests, it is often necessary to incorporate corrective techniques to the ΔK applied data. Since Elber discovered the existence of crack closure, it has become a widely used tool to explain the extrinsic response of fatigue crack growth rate behavior. Crack closure is a crack tip shielding mechanism whereby the crack-tip cyclic strain is partially shielded from damaging stress. The source of this shielding is most commonly caused by crack wake interference due to plasticity, roughness (microstructure), oxide and/or residual stress. The experimental measurement of crack closure has been hampered by widely varying and non-repeatable methods of evaluation.

Furthermore, experimental observations are subject to varying and inconsistent methods of interpretation. In an attempt to improve consistency of measurement, ASTM E647 has an automated offset opening load technique. After two round-robin programs, this method was adopted as an annex to the ASTM E647 standard. However, this method often over corrects the ΔK applied data primarily because the method fails to account for evidence of crack tip cyclic strain below the opening load. This is especially important if the closure mechanism is not necessarily near the crack tip but distributed along the full wake of the crack.

As an alternative approach, the adjusted compliance ratio (ACR) method of determining the effective stress intensity has been useful in accounting for compressive residual stress and other sources of remote closure resulting in an intrinsic FCGR curve that is thought to emulate the small crack behavior. The method uses the same load-displacement records as the opening load method, but it accounts for partial closure effects (effects below the opening load). Further details of this methodology are provided in Annex B.

The data from Figures 10 through 12 have been re-plotted in Figures 22 through 24 using the ACR method to estimate ΔK_{eff} . These plots show that in the absence of remote closure, the seawater environment has an equivalent or possibly even greater impact of the FCGR behavior. Depending on exposure times, crack size and crack growth rates, the extrinsic behavior (based on $\Delta K_{\text{applied}}$) may be different than the intrinsic behavior based on $\Delta K_{\text{effective}}$. This is because the environment can work in two ways. It tends to accelerate crack growth due to environmental influence at the crack tip. At the same time it can lead to suppressed crack growth rates due to corrosion product build-up resulting in crack closure shielding in the crack wake. By analyzing the effective stress intensity, the two opposing mechanisms can be partitioned.

A re-examination of the data from Figure 13 shows that when crack closure is accounted for, there is even less difference in the three grades of material (Figure 25). Similarly, in seawater, (Figure 14) some of the perceived differences in lower region II data may be attributed to crack closure as well (Figure 26). Finally, a re-examination of the near-threshold data from Figure 18 also shows that the intrinsic behavior of all three alloys is nearly identical (Figure 27).

Fatigue Crack Growth Rate vs. Stress Intensity

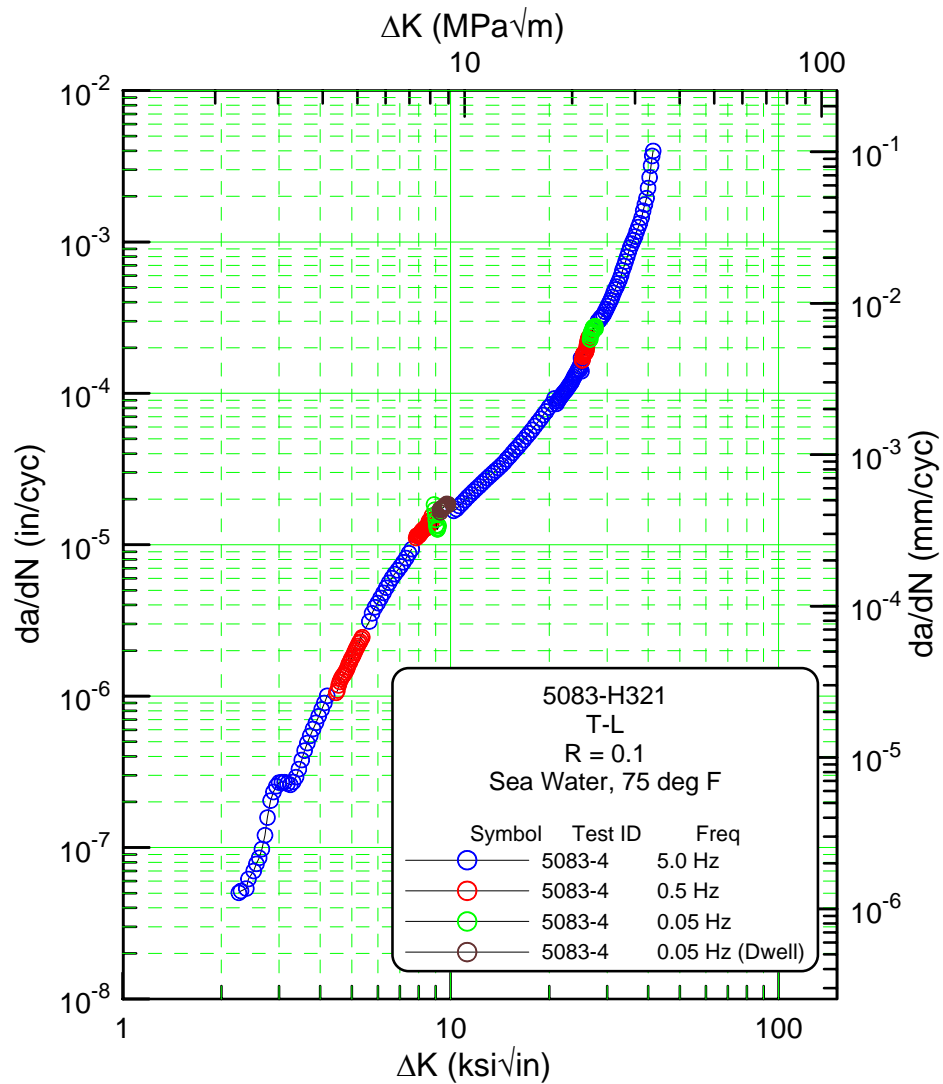


Figure 15. FCGR response showing the effect of frequency for the 5083-H321 alloy in seawater.

Fatigue Crack Growth Rate vs. Stress Intensity

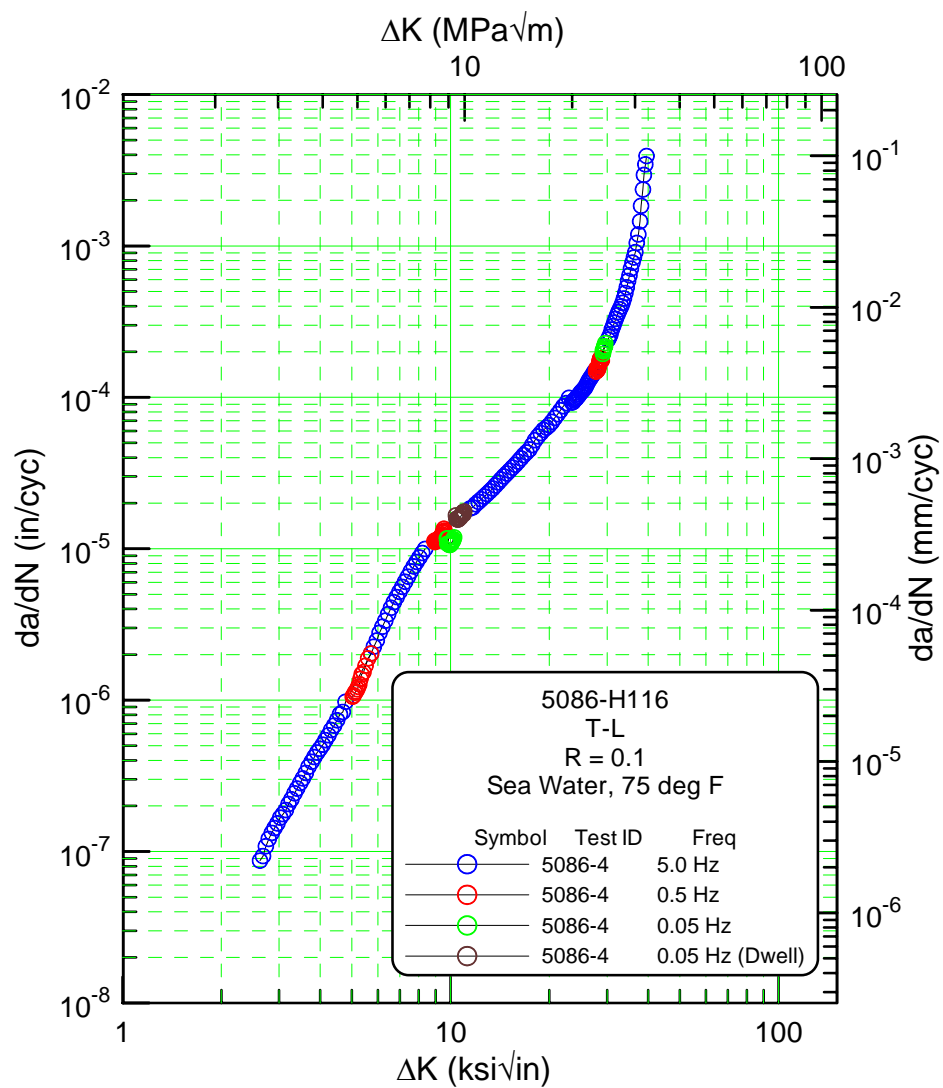


Figure 16. FCGR response showing the effect of frequency for the 5086-H116 alloy in seawater.

Fatigue Crack Growth Rate vs. Stress Intensity

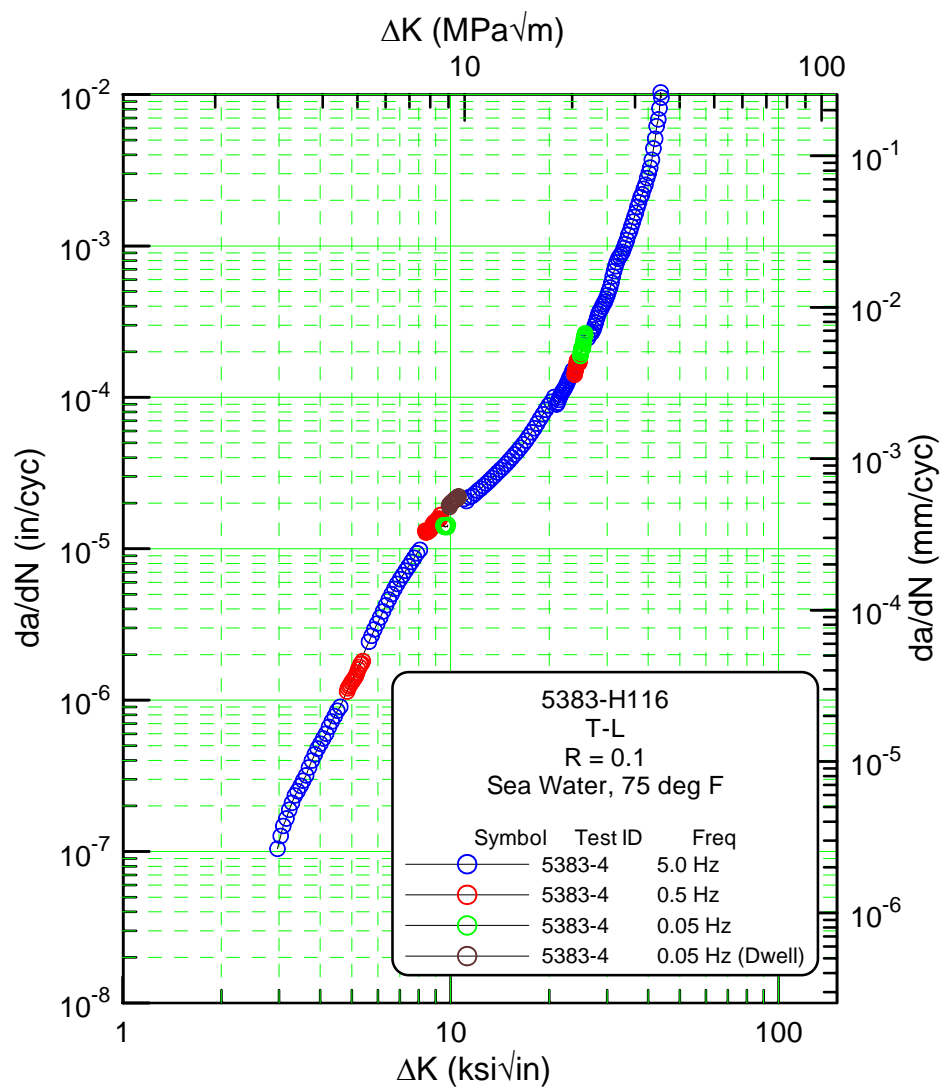


Figure 17. FCGR response showing the effect of frequency for the 5383-H116 alloy in seawater.

Fatigue Crack Growth Rate vs. Stress Intensity

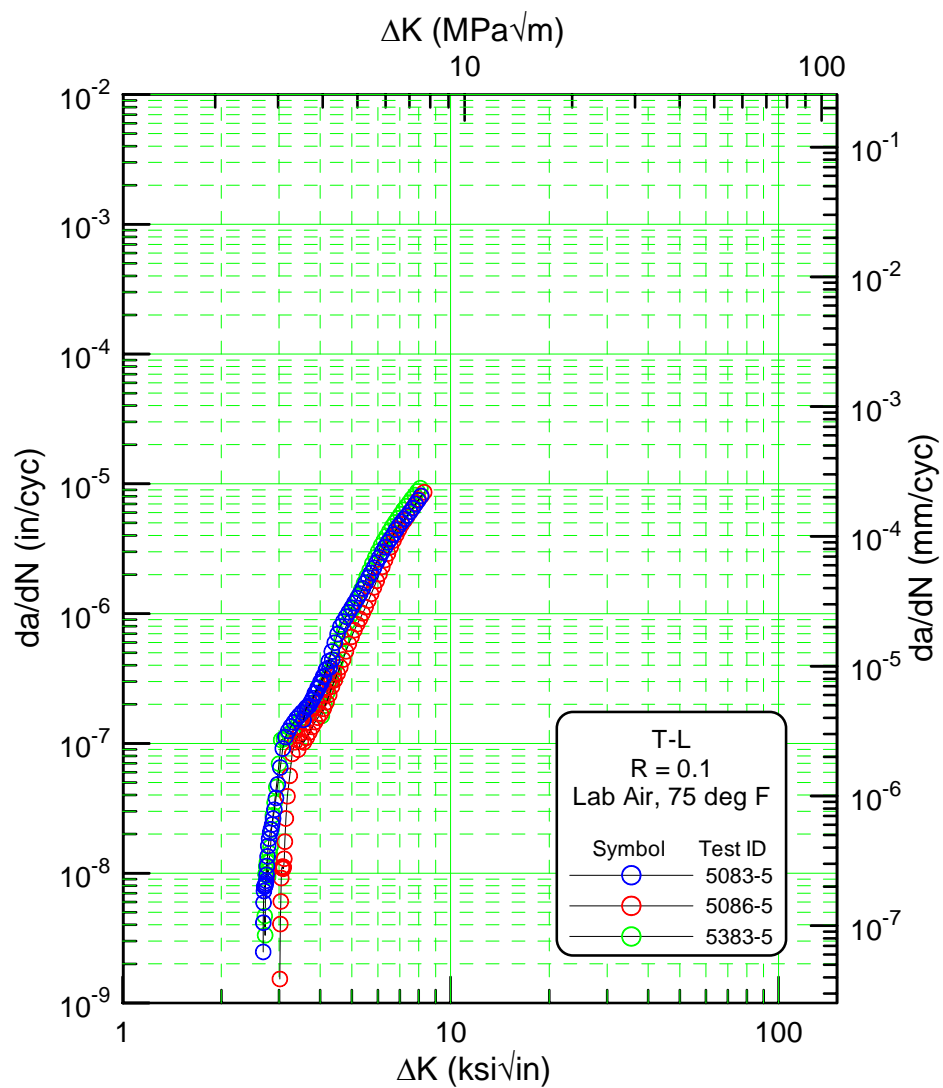


Figure 18. FCGR response showing the effect of the alloy on near-threshold behavior.

Fatigue Crack Growth Rate vs. Stress Intensity

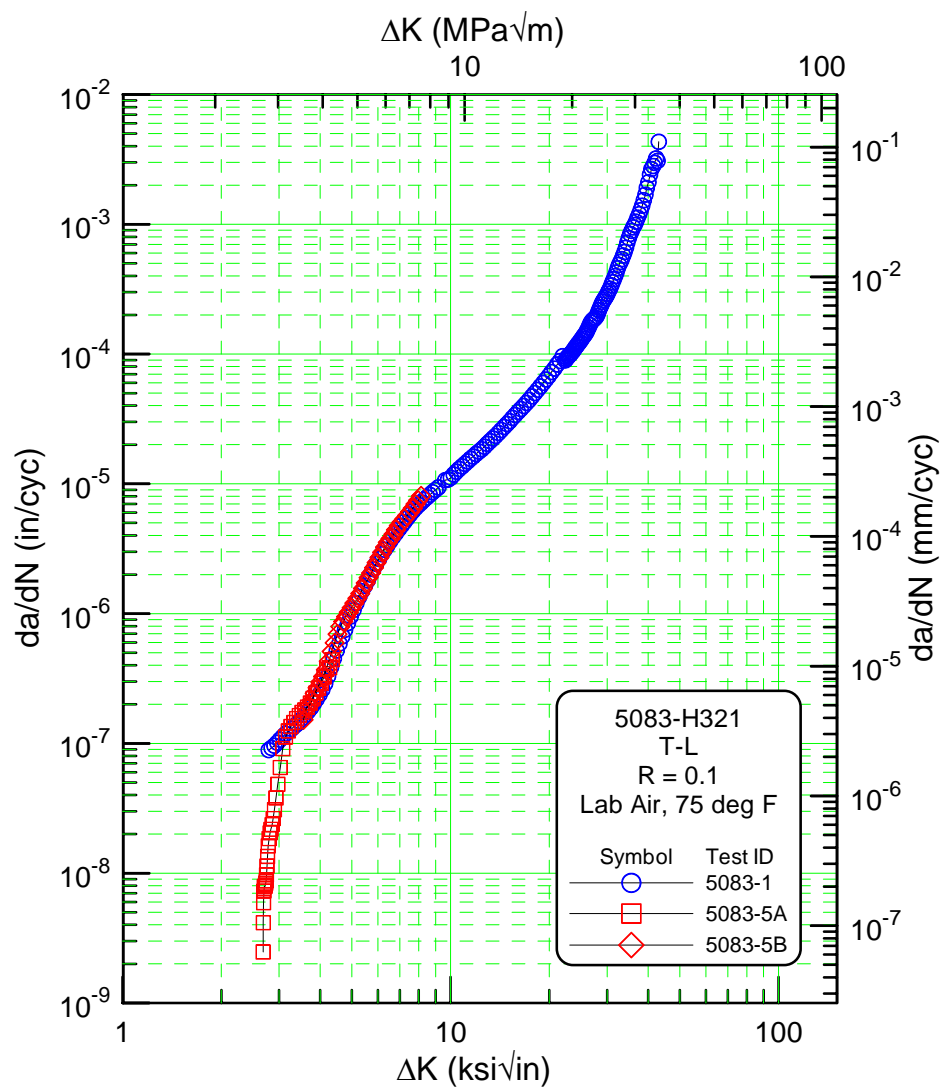


Figure 19. FCGR response comparing near-threshold behavior with previous increasing K data for the 5083-H321 alloy. Note departure in behavior at $\sim 1 \times 10^{-7}$ inch/cycle.

Fatigue Crack Growth Rate vs. Stress Intensity

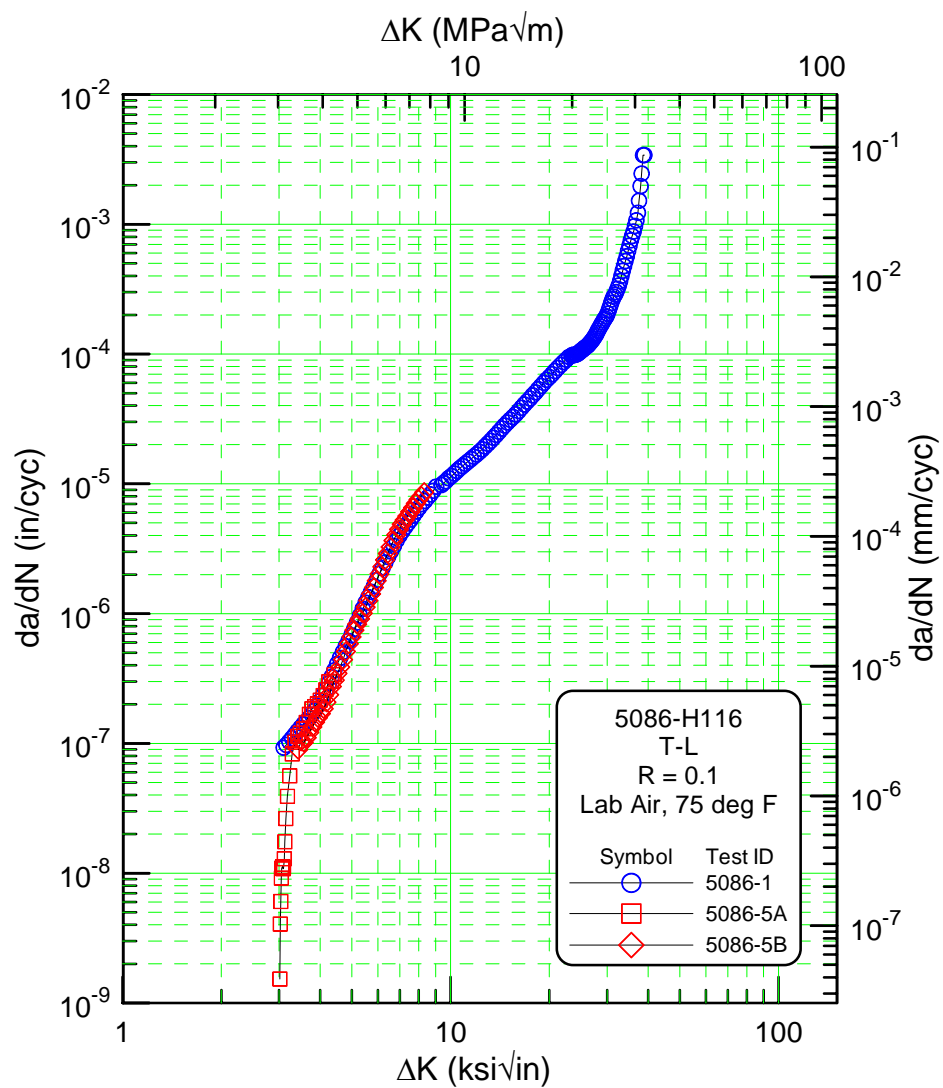


Figure 20. FCGR response comparing near-threshold behavior with previous increasing K data for the 5086-H116 alloy. Note departure in behavior at $\sim 1 \times 10^{-7}$ inch/cycle.

Fatigue Crack Growth Rate vs. Stress Intensity

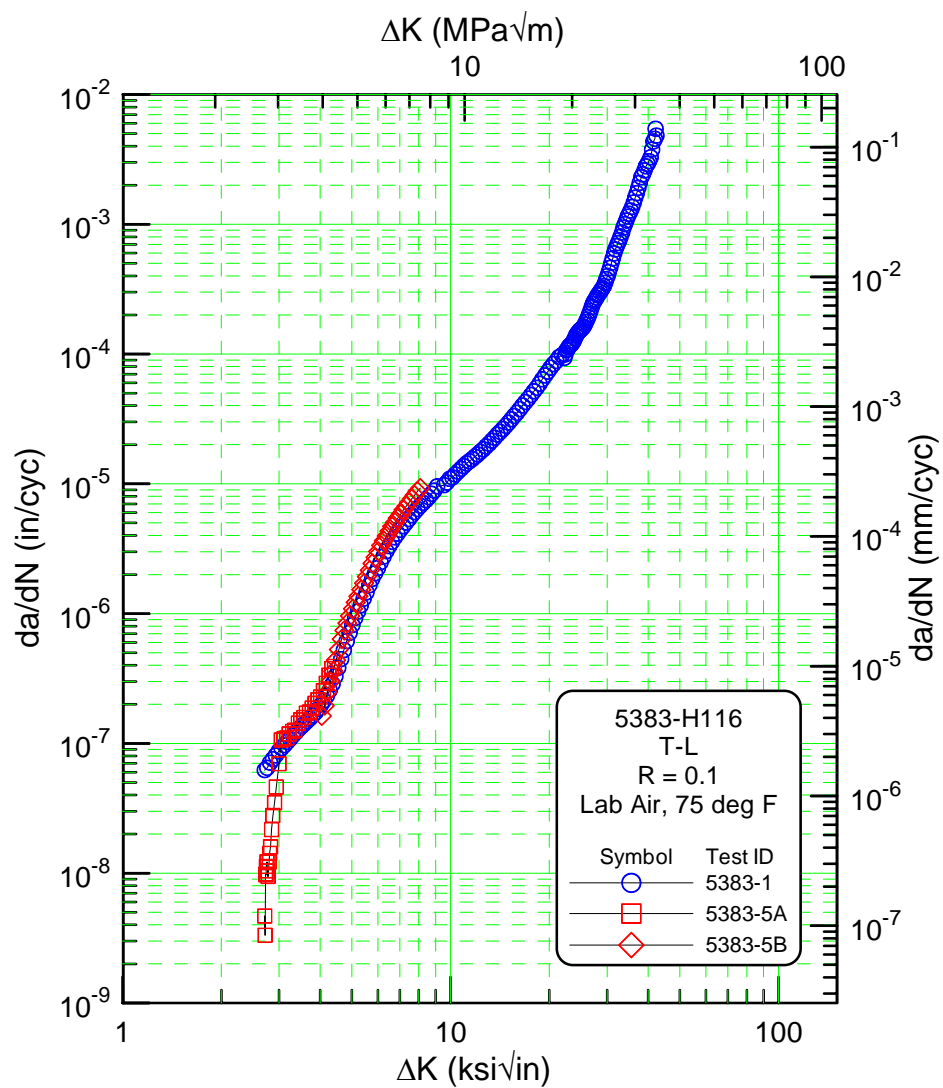


Figure 21. FCGR response comparing near-threshold behavior with previous increasing K data for the 5383-H116 alloy. Note departure in behavior at $\sim 1 \times 10^{-7}$ inch/cycle.

Fatigue Crack Growth Rate vs. Stress Intensity

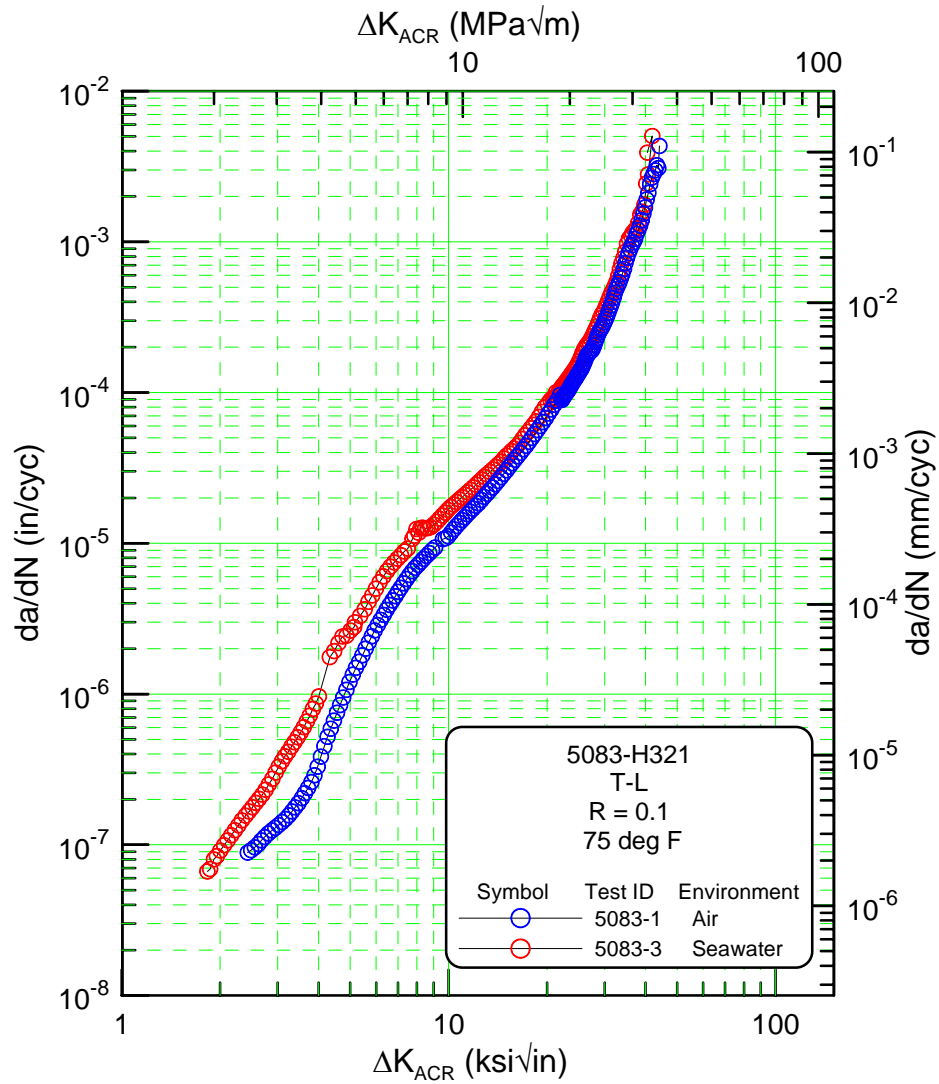


Figure 22. FCGR response showing the effect of environment for the 5083-H321 alloy. Data are corrected for closure using the ACR method.

Fatigue Crack Growth Rate vs. Stress Intensity

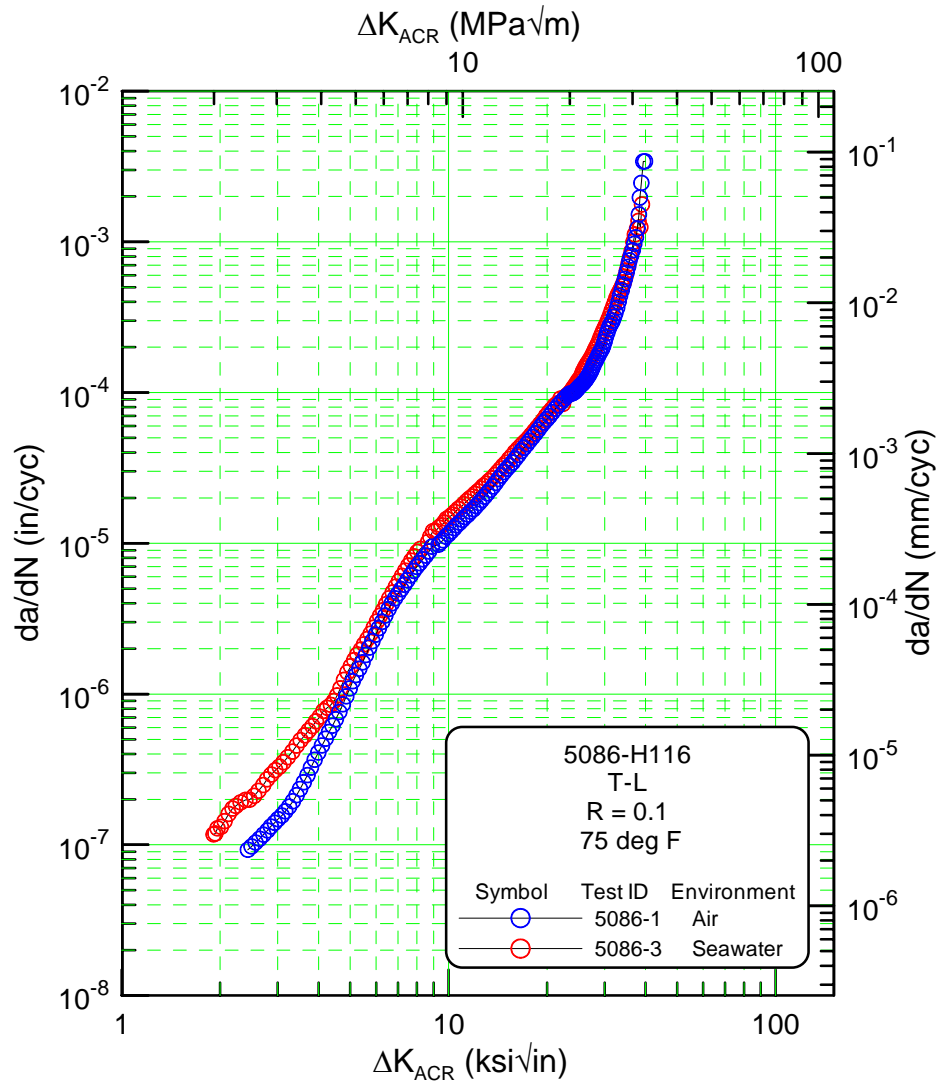


Figure 23. FCGR response showing the effect of environment for the 5086-H116 alloy. Data are corrected for closure using the ACR method.

Fatigue Crack Growth Rate vs. Stress Intensity

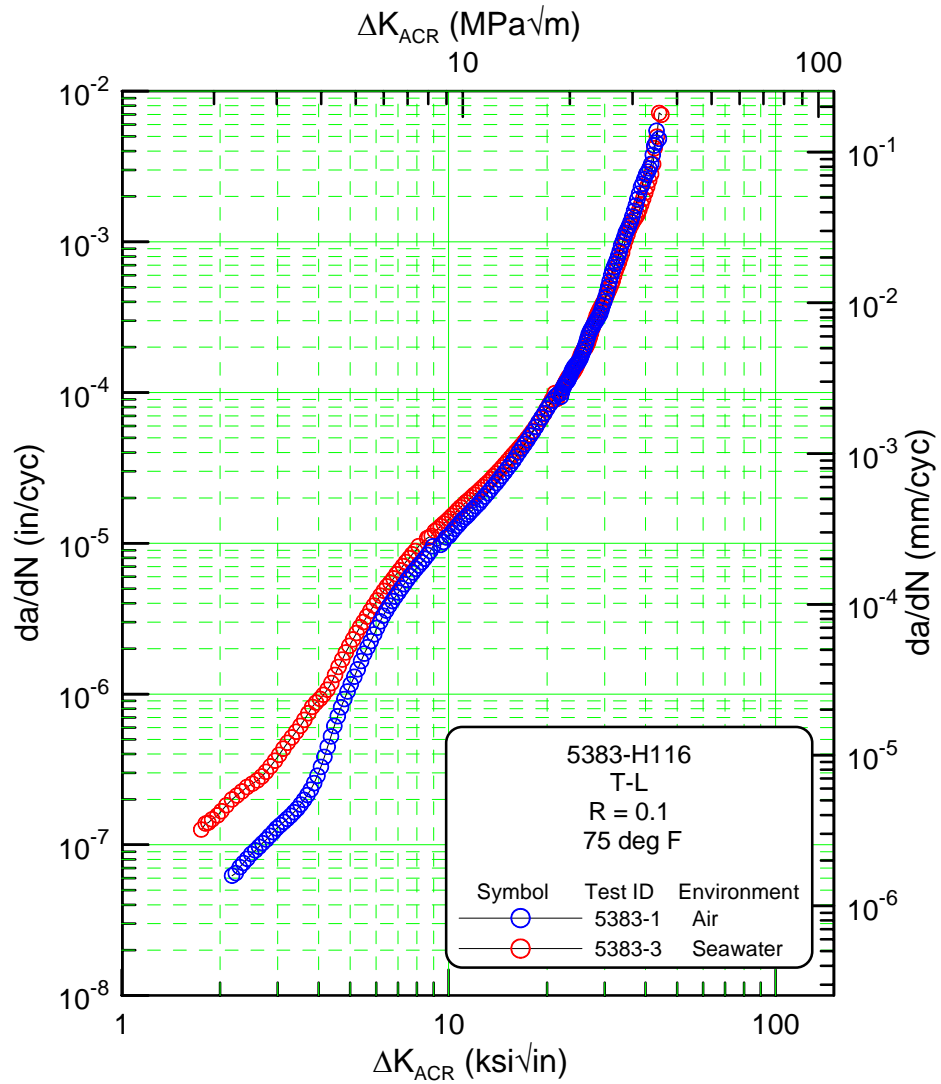


Figure 24. FCGR response showing the effect of environment for the 5383-H116 alloy. Data are corrected for closure using the ACR method.

Fatigue Crack Growth Rate vs. Stress Intensity

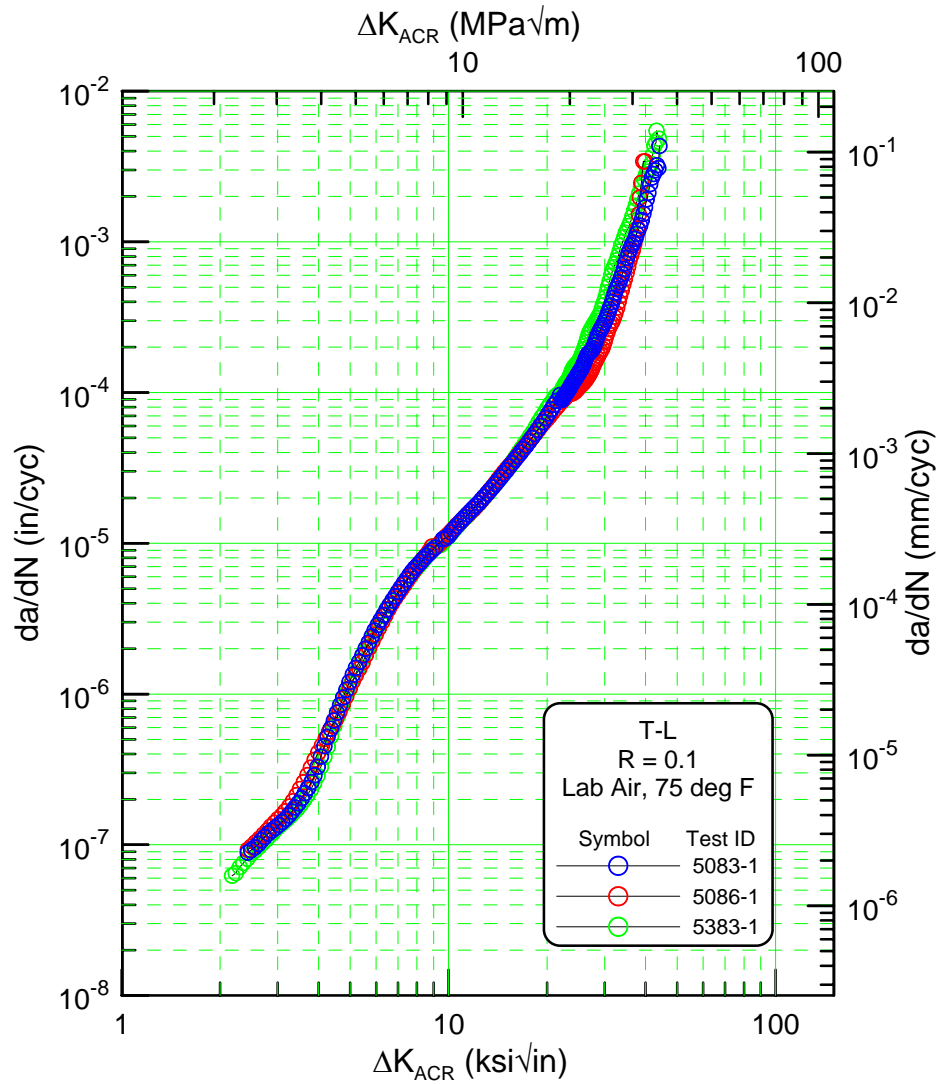


Figure 25. FCGR response showing the effect of the grade of material in laboratory air. Data are corrected for closure using the ACR method.

Fatigue Crack Growth Rate vs. Stress Intensity

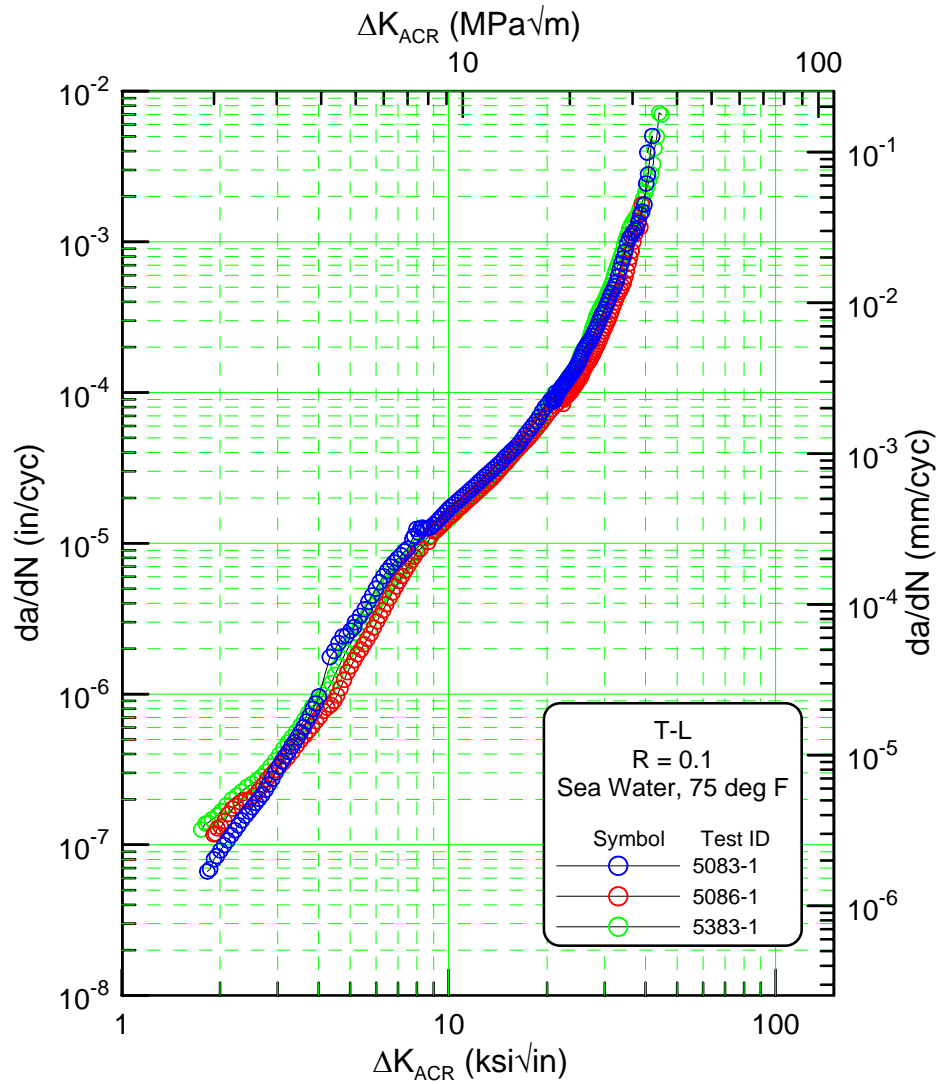


Figure 26. FCGR response showing the effect of the grade of material in seawater. Data are corrected for closure using the ACR method.

Fatigue Crack Growth Rate vs. Stress Intensity

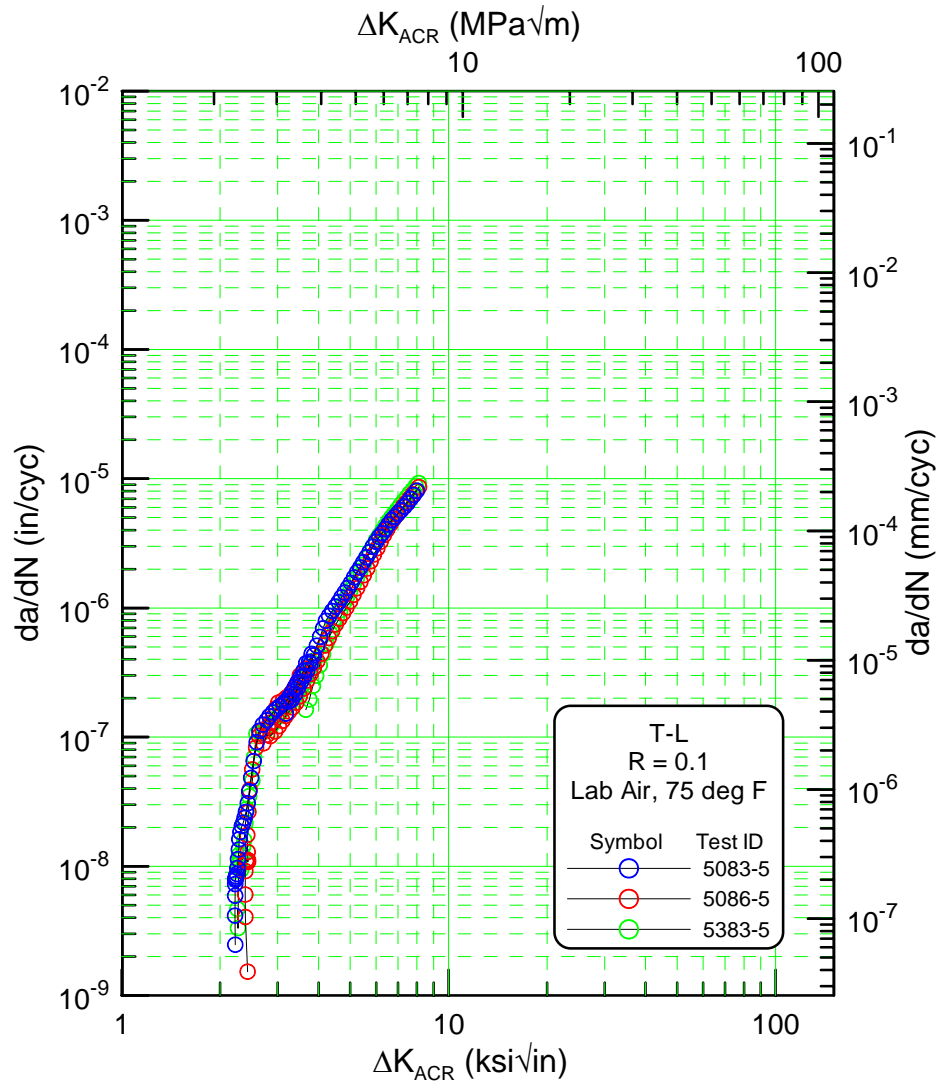


Figure 27. FCGR response showing the effect of the alloy on near-threshold behavior. Data are corrected for closure using the ACR method.

3. Non-Linear Fracture Toughness Characterization

3.1 Introduction

Non-Linear fracture toughness testing (NLFT) testing was conducted on three grades of aluminum alloys designated 5083-H321, 5086-H116 and 5383-H116. A compact tension sample having a width of 2.000 inches and a thickness of 0.500 inches was chosen for the majority of the NLFT testing. In addition, a compact tension sample having a width of 4.000 inches and a thickness of 0.500 inches was used to evaluate size effects. For each grade of material, two replicate tests were conducted using full thickness samples without side grooves. A third set of samples was tested with side-grooves to evaluate constraint effects. All samples were machined in the T-L orientation and all samples were tested laboratory air. Testing was performed in accordance with the ASTM E 1820-01 "Standard Test Method for Measurement of Fracture Toughness. A single specimen unloading compliance technique was used to monitor stable crack extension.

3.2 Test Equipment

The tests were conducted on one MTS load frame equipped with a 5,000 lbf load cell and interfaced to an Adwin-Gold FTA computer system and configured for fracture toughness testing. An MTS model 632.03B-30 (opt 006) clip gage was used for load-line displacement measurement. Compliance measurement accuracy was enhanced by mounting needle bearings in both the clevis holes and the specimen holes to minimize non-linearity in the load-displacement signal due to pin friction. Laboratory temperature and relative humidity were controlled to 75°F ±2°F and 40% ±5% R.H. throughout the entire period of testing.

3.3 Sample Preparation

The test samples were machined according to Figure 28.

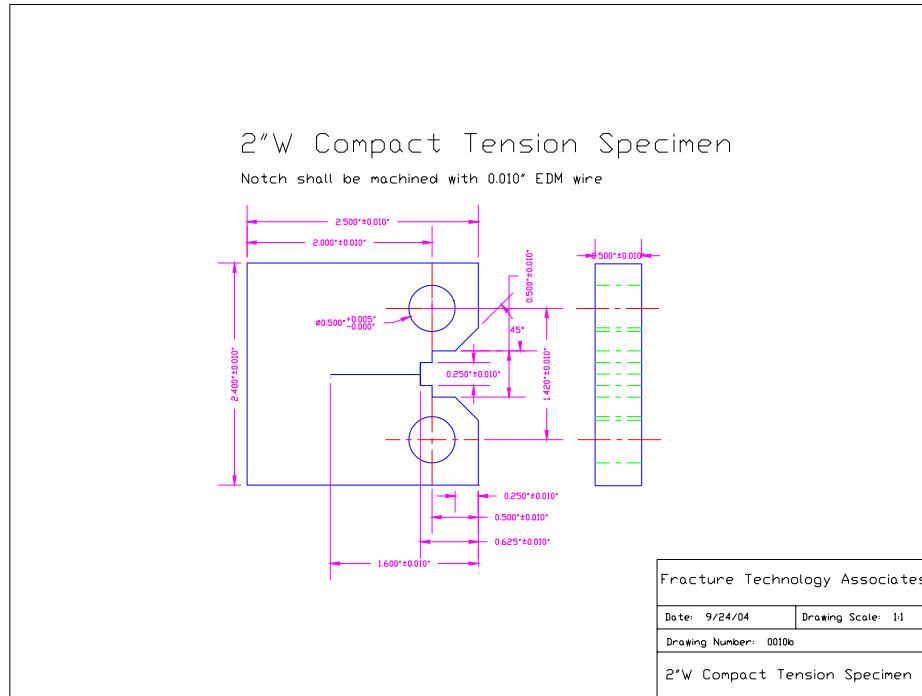


Figure 28. Diagram of C(T) sample for fracture toughness testing (diagram reproduction not to scale).

3.4 Test Procedure

Data storage (.raw file extension) was set to 2 points per second for load displacement data in the ramp up/ramp down mode; 0.2 points per second for load displacement data during the hold mode, and 10 points per second for unloading slope data (.unl file extension). The actuator loading and unloading rate was set to 0.020 inches/minute. Each test was initially ramped to the approximate pre-crack load and several unloading slopes were performed with a loading/unloading data acquisition rate of 10 points/second to ensure the specimens were properly seated. The correlation coefficient of each unloading slope was typically 0.99998. After verification that the unloading slopes were repeatable and that the compliance measured crack length was within 2% of the predicted crack length, actual testing commenced. Load and clip gage displacement were recorded in the analysis file every 0.0010 - 0.0020 inches of clip gage displacement or every 200 lbs. increase in load. In addition, the largest observed load and corresponding displacement were stored.

Each test was terminated after about 0.2 inches of stable crack extension. The sample was then fatigue loaded to mark the final crack extension. A nine point average of the pre-crack as well as the final stable crack extension was recorded and used to verify the compliance calculated crack extension.

3.5 Test Results and Discussion

Table 5 summarizes key test conditions and results. The fracture toughness results are based on the J at initiation (J_{Ic}) according to ASTM E1820-01 as well as an equivalent K at initiation designated K_{IIC} . The toughness values at initiation for the side grooved and non-side grooved samples were almost equivalent. The larger sample size gave slightly higher values of toughness at initiation. Regardless of the size of the sample or the absence or presence of the side grooves, all samples showed the same ranking of toughness with the 5086-H116 showing the highest toughness, followed by the 5083-H321, and the 5383-H116 alloy showing the lowest toughness.

Table 5. Summary of Fracture Toughness Test Conditions and Results (Temperature: 75°F, Orientation: T-L, Environment: Lab Air (RH = 40%)).

| Test ID | Material | Sample Size (W, in) | Side-Groove | J_{Ic} -1820 (in-lb/in ²) | K_{IIC} (ksi \sqrt{in}) | Comments |
|-----------|-----------|---------------------|-------------|---|------------------------------|-----------------------------|
| 5083-FT-1 | 5083-H321 | 2.00 | no | 96.6 | 33.4 | Significant crack tunneling |
| 5083-FT-2 | 5083-H321 | 2.00 | no | 91.8 | 32.6 | Significant crack tunneling |
| 5083-FT-3 | 5083-H321 | 2.00 | yes | 111.4 | 35.9 | Straight crack front |
| 5083-FT-5 | 5083-H321 | 4.00 | no | 146.9 | 41.2 | Significant crack tunneling |
| | | | | | | |
| 5086-FT-1 | 5086-H116 | 2.00 | no | 155.4 | 42.3 | Significant crack tunneling |
| 5086-FT-2 | 5086-H116 | 2.00 | no | 147.6 | 41.3 | Significant crack tunneling |
| 5086-FT-3 | 5086-H116 | 2.00 | yes | 155.2 | 42.3 | Straight crack front |
| 5086-FT-5 | 5086-H116 | 4.00 | no | 201.0 | 48.2 | Significant crack tunneling |
| | | | | | | |
| 5383-FT-1 | 5383-H116 | 2.00 | no | 86.6 | 31.6 | Significant crack tunneling |
| 5383-FT-2 | 5383-H116 | 2.00 | no | 86.1 | 31.5 | Significant crack tunneling |
| 5383-FT-3 | 5383-H116 | 2.00 | yes | 90.3 | 32.3 | Straight crack front |
| 5383-FT-5 | 5383-H116 | 4.00 | no | 99.9 | 34.0 | Significant crack tunneling |
| | | | | | | |

The most significant difference between the side grooved and non-side grooved samples is illustrated in Figure 29. These R-curves show stable crack extension well beyond maximum load. The samples without the side grooves are representative of the fracture toughness characteristics of the 0.5 inches plate whereas the side grooved samples are representative of much thicker material since the side grooves add additional constraint and suppress plane stress behavior. Data beyond crack initiation

should be used with caution since stable crack extension behavior is highly geometry/application dependent (See annexes for details). The ranking of the alloys is also clearly indicated consistent with the previous observations regarding toughness at initiation. The reproducibility of duplicate tests is also clearly indicated.

Fracture Toughness R-Curve

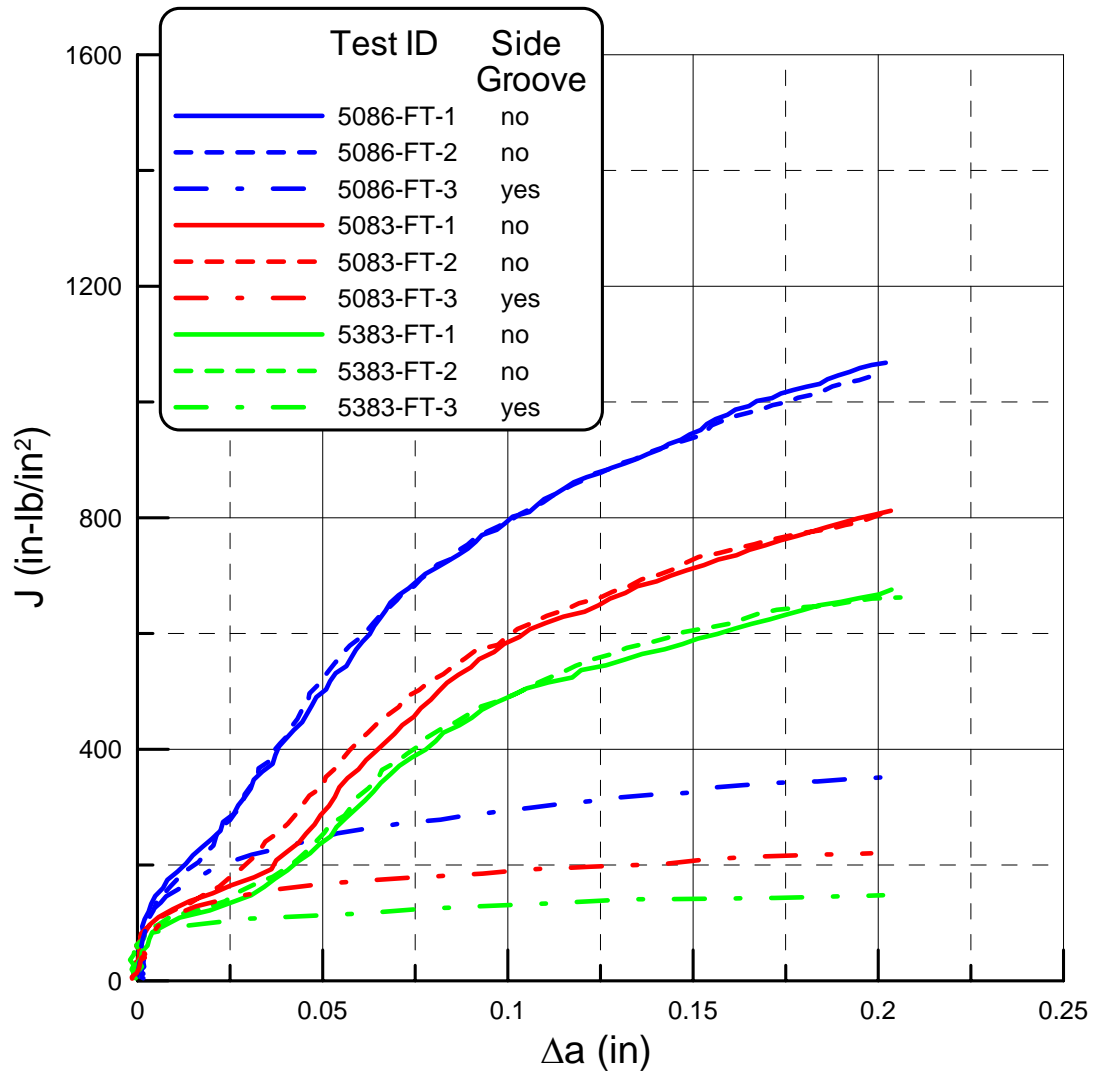


Figure 29. Non-linear fracture toughness showing ranking of alloys as well as duplicate test results and the effect of side grooves.

Figure 30 illustrates the effect of sample size. In all cases, the larger sample size shows slightly higher values of toughness at a given increment of crack extension. Figures 31 and 32 show the same trends but the toughness values have been presented as equivalent values of stress intensity K instead of J .

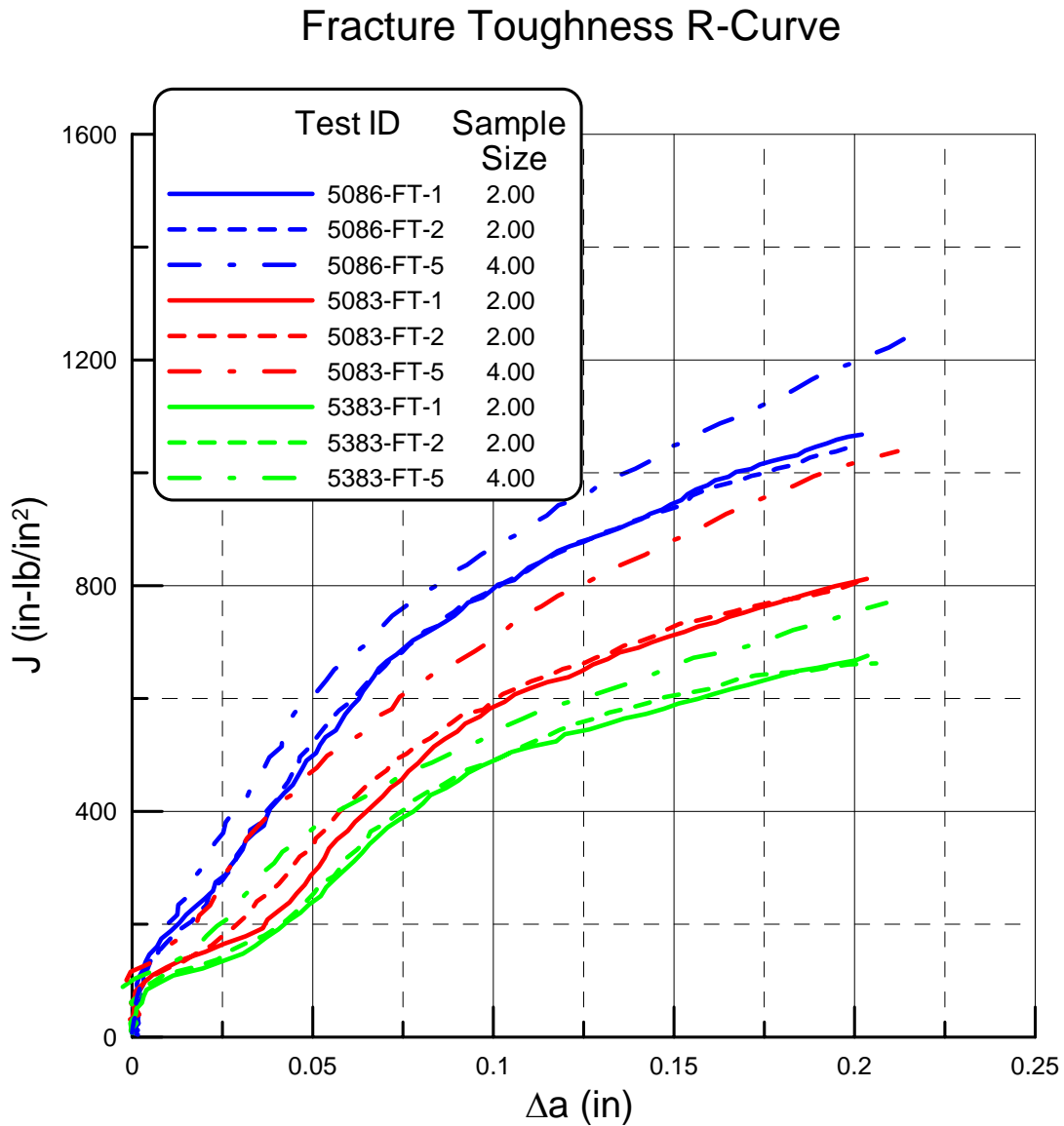


Figure 30. Non-linear fracture toughness showing ranking of alloys as well as duplicate test results and the effect of sample size.

Fracture Toughness R-Curve

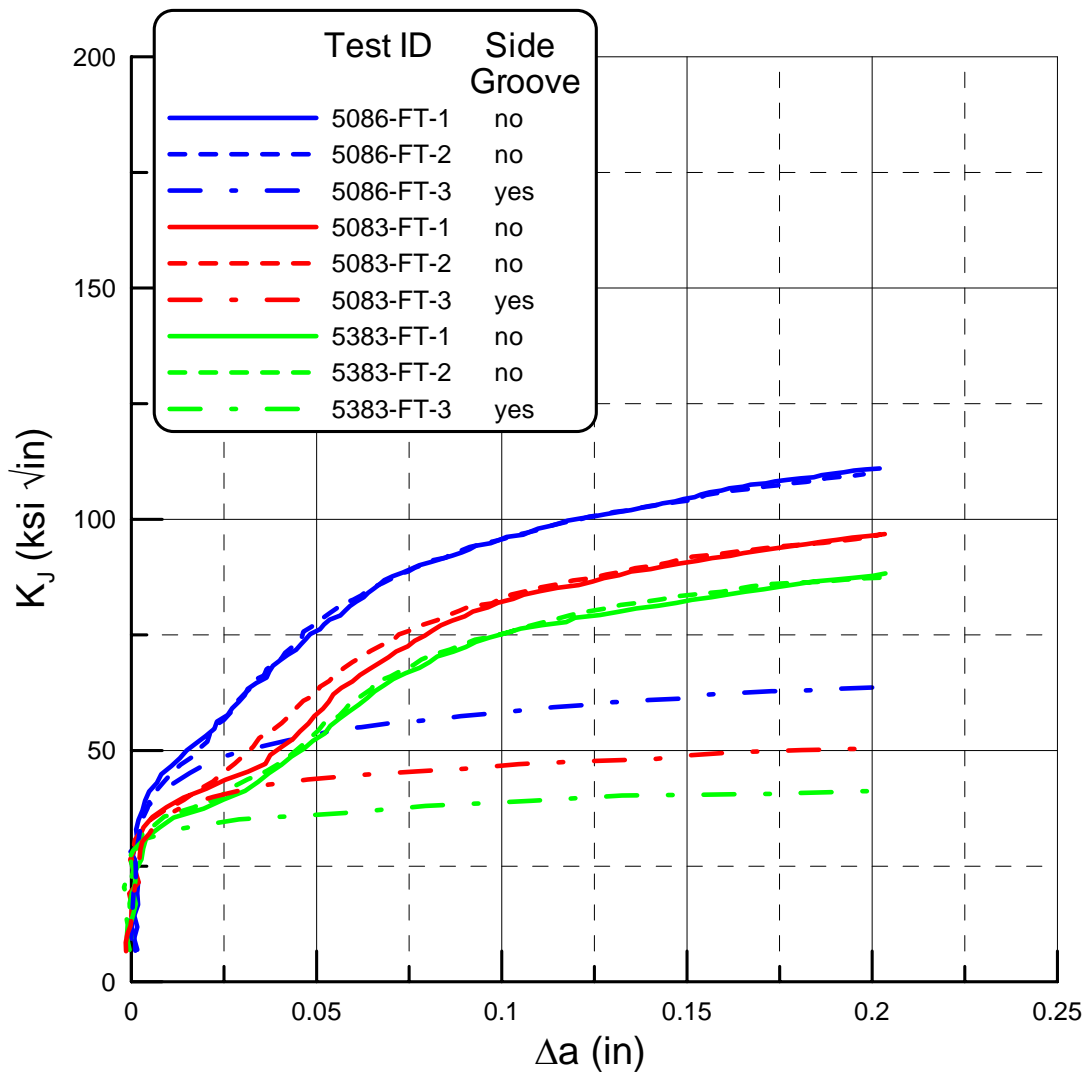


Figure 31. Non-linear fracture toughness showing ranking of alloys as well as duplicate test results and the effect of side grooves. Equivalent K is plotted.

Fracture Toughness R-Curve

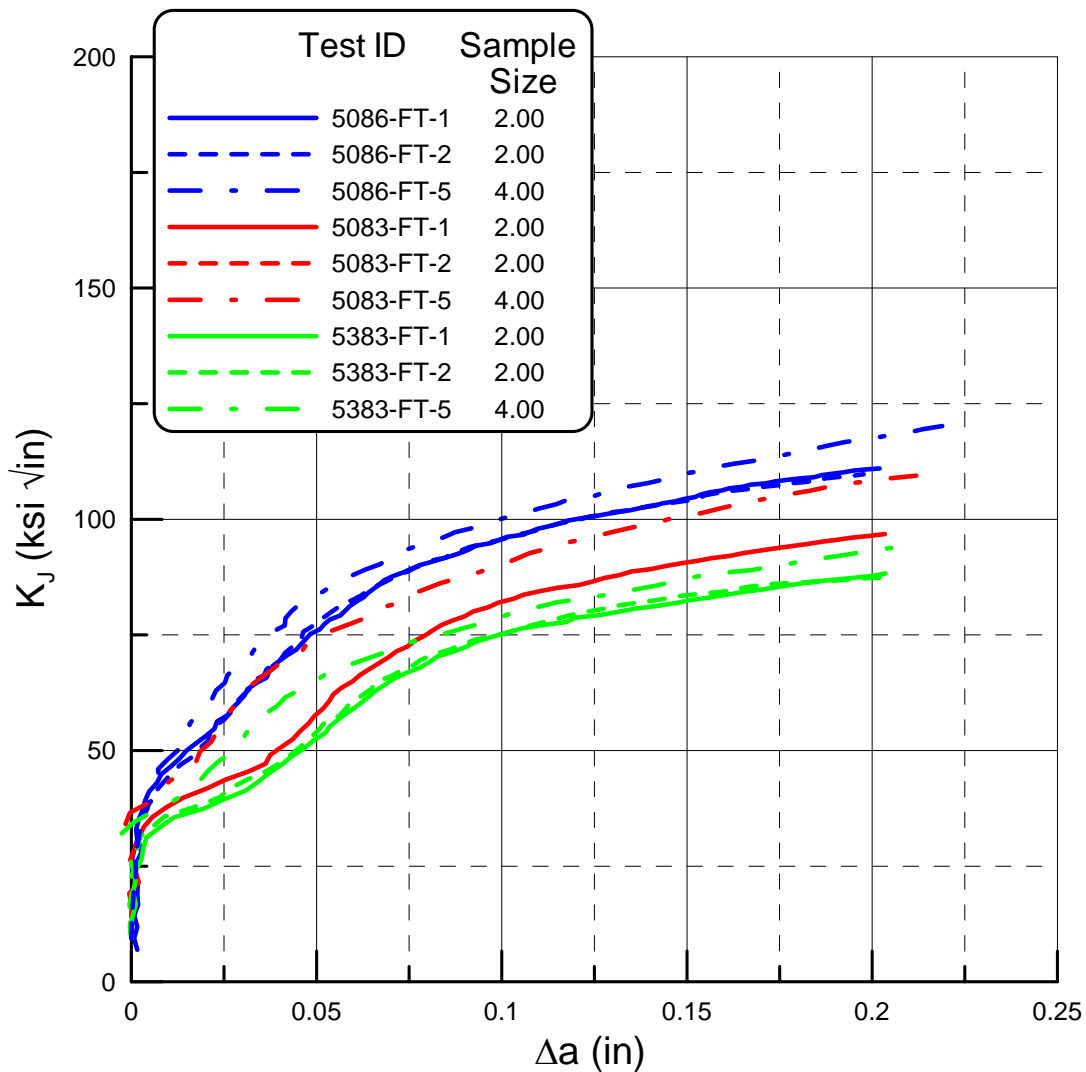


Figure 32. Non-linear fracture toughness showing ranking of alloys as well as duplicate test results and the effect of sample size. Equivalent K is plotted.

The photographs in Annex C clearly show the crack straightness characteristic of each test. Annex F contains individual J vs. Δa plots. Annex G contains load vs. load-line displacement curves. Annex H contains the tabular results of the ASTM 1820 analyses including a summary of validity statements for each test.

Annex A – Procurement and Characterization of Alloys

A1. Summary

The Project Technical Committee selected four alloys – 5083 H321, 5086 H116, 5383 H116, and 5059 H321 – in ½-in-thick plates conforming to ASTM B 928. After much searching, a supplier (warehouse) was found that could supply three of the four selected alloys.

5083 H321 was supplied as 5083 H321 to ASTM B 928 and meets ASTM B 928 for mechanical properties and chemical composition. Metallographic examination showed that this alloy is not sensitized but has considerable grain boundary **Beta** and may have more than 15 mg/cm² mass loss in ASTM G 67.

5086 H116 was supplied as 5086 H32 to ASTM B 209 and met both ASTM B 928 for mechanical properties and chemical composition except for yield strength (27.0 ksi vis-à-vis 28.0 ksi minimum) and ASTM G 66 for exfoliation susceptibility. Metallographic examination showed that this alloy is not sensitized and has the least grain boundary **Beta** of the three alloys examined.

5383 H116 was supplied as 5383/5083 H116 to ASTM B 209 and met both ASTM B 928 for mechanical properties and chemical composition except for Fe and Mn content (respectively, 0.29% vis-à-vis 0.28% maximum and 0.53% vis-à-vis 0.7 - 1.0%) and ASTM G 66 for exfoliation susceptibility. Metallographic examination showed that this alloy has less grain boundary **Beta** than the 5083 H321 alloy examined.

It is interesting to note that the alloy furnished to ASTM B 928 – 5083 H321 – showed more **Beta** phase on the grain boundaries than either alloy – 5086 H32 and 5383 H116 – furnished to ASTM B 209.

No source could furnish grade 5059 in either temper, H116 or H321.

The mechanical properties and chemistries of the three alloys are compared in, respectively, Tables 6 and 7.

Table 6. Summary of Mechanical Properties.

| Alloy | 0.2% Yield Strength, ksi | | Tensile Strength, ksi | | Percent Elongation in 1 inch | | Percent Reduction of Area | |
|-----------|--------------------------|---------|-----------------------|---------|------------------------------|---------|---------------------------|---------|
| | Long. | Transv. | Long. | Transv. | Long. | Transv. | Long. | Transv. |
| 5083 H321 | 37.9 | 34.3 | 52.7 | 51.8 | 14.4 | 19.6 | 21.3 | 36.1 |
| 5086 H32 | 27.0 | 27.0 | 45.8 | 46.0 | 15.1 | 19.4 | 16.8 | 34.2 |
| 5383 H116 | 39.2 | 35.4 | 54.2 | 53.3 | 13.8 | 17.3 | 16.3 | 27.7 |

Table 7. Summary of Chemical Composition.

| Alloy | Weight Percent Maximum | | | | | | | |
|-----------|------------------------|------|------|------|-----|------|------|------|
| | Si | Fe | Cu | Mn | Mg | Cr | Zn | Ti |
| 5083 H321 | 0.15 | 0.31 | 0.06 | 0.50 | 4.8 | 0.08 | 0.09 | 0.03 |
| 5086 H32 | 0.14 | 0.31 | 0.07 | 0.45 | 3.8 | 0.19 | 0.03 | 0.03 |
| 5383 H116 | 0.13 | 0.29 | 0.06 | 0.53 | 4.8 | 0.10 | 0.08 | 0.03 |

A2. Tempers Used in Marine Alloys

The non-heat-treatable 5xxx alloys are solution-strengthened, primarily, by magnesium. The tempers H116 and H321 have been reserved by the Aluminum Association for wrought products in the 5xxx series containing 3% or more Mg. The temper designations are:

- H Strain hardened.
- H1 Strain hardened without thermal treatment. Second digit indicates degree of strain hardening.
- H116 Strain hardened only.
- H3 Strain hardened and stabilized by low temperature thermal treatment. Tensile strength reduced slightly but ductility improved.
- H32 Stabilized by a low-temperature thermal treatment after strain hardening. The second digit 2 indicates the degree of strain hardening, i.e., quarter-hard.

H321 Stabilized by a low-temperature thermal treatment after strain hardening less than the amount required for a controlled H32 temper. The third digit identifies variation from H32.

A3. Alloys Furnished to the Project

The PTC of the subject project selected four alloys – 5083 H321, 5086 H321, 5383 H321, and 5059 H321 – in ½-in-thick plates conforming to ASTM B 928^[1] for fracture mechanics characterization.

Contacts with both domestic and European aluminum manufacturers and builders of aluminum vessels were unsuccessful. However, a supplier (warehouse) was found that could supply three of the four selected alloys, Table 8. Each alloy was furnished as a ½x24x24-in plate.

No source could furnish grade 5059 in either temper, H 116 or H321.

Table 8. Plates Furnished by Suppliers.

| Alloy Ordered to B 928 | Supplier | | | | | |
|------------------------------|-------------------------|----------------------|----------|--------------------------|-----------|----------|
| | Pierce, Warminster, Pa. | | | Pierce, New Orleans, La. | | |
| | Alloy | ASTM Std. | Mfgr. | Alloy | ASTM Std. | Mfgr. |
| 5083 H321 | 5083 H321 | B 928 | Pechiney | | | |
| 5086 H116 | 5086 H32 | B 209 ^[2] | Capral | | | |
| 5383 H116 | | | | 5383/5083 H116 | B 209 | Pechiney |

A3.1 Laboratories

Dirats Laboratories, Westfield, Massachusetts, performed the tensile tests and chemical analysis on the three furnished alloys.

The *tension specimens* were cylindrical with a test-section diameter of 0.25 in and a gage-length of 1 in. Data for each alloy are presented in the following sections. Note that *Elongation* is measured over a gage length of 4 times the diameter of the tension test specimen, i.e., 1 in. Three specimens were taken in both the longitudinal and

¹ ASTM B928/B 928M-04a *Standard Specification for High Magnesium Aluminum-Alloy Sheet and Plate for Marine Service and Similar Environments.*

² ASTM B 209-02a *Standard Specification for Aluminum-Alloy Sheet and Plate.*

transverse directions (with respect to rolling direction) from each of the three 0.5 in thick alloys.

The results of the tensile tests and chemical analyses are listed below for each of the three alloys.

Dr Catherine Wong, Materials Engineer, NAVSEA, performed metallography on 2x2x0.5-in samples of each of the three acquired alloys. The primary purpose of this investigation was to determine the extent of the **Beta** phase (i.e., magnesium-rich precipitate) precipitation on the grain boundaries.

Her findings and metallographs are presented below for each of the three alloys.

A3.2 *Beta* Phase

In the 5xxx series alloys, magnesium can precipitate out of solution and solidify on the grain boundaries. This magnesium-rich precipitate is known as the **Beta** phase. Sensitivity of high magnesium aluminum plates to exfoliation and intergranular corrosion increases with the amount of **Beta** phase on the grain boundaries.

Solid lines of **Beta** phase are sensitive to intergranular corrosion whilst **Beta** phase as spheres at intermittent locations on the grain boundaries is resistant to intergranular corrosion.

The form and amount of Beta phase on the grain boundaries depend on

- Thermal-mechanical rolling practices, i.e., the number of passes, reduction in thickness per pass, total reduction, and metal temperature in each pass.
- Product thickness. E.g., The problem that led to the development of ASTM B 928 was confined to relatively thin 5083 H321 sheets and plates, i.e., 3/8-in thick and below.

A3.3 *Alloy 5083 H321*

For 5083 H321, Pierce, Warminster, Pa., supplied 5083 H321 to ASTM B 928 by Pechiney (France).

The alloy supplied met ASTM B 928 for mechanical properties and chemical composition, respectively, Tables 9 and 10.

Table 9. Mechanical Properties – 5083 H321.

| Source | | 0.2% Yield Strength, ksi | | Tensile Strength, ksi | | % Elongation |
|---|---------|--------------------------|------|-----------------------|------|--------------|
| | | min | max | min | max | min |
| B 928 | | 31.0 | 43.0 | 44.0 | 56.0 | 12 |
| Pierce | | 35.2 — 39.6 | | 52.2 — 53.9 | | 14 — 16 |
| Dirats | Long. | 37.9 | | 52.7 | | 14.4 |
| | Transv. | 34.3 | | 51.8 | | 19.6 |
| * <i>Dirats Reduction of Area: Long., 21.3%, Transv., 36.1%</i> | | | | | | |

Table 10. Chemical Composition – 5083 H321.

| Source | Weight Percent Maximum unless shown as Range | | | | | | | |
|--------|--|------|------|------------|-----------|-------------|------|------|
| | Si | Fe | Cu | Mn | Mg | Cr | Zn | Ti |
| B 928 | 0.40 | 0.40 | 0.10 | 0.40 - 1.0 | 4.0 - 4.9 | 0.05 - 0.25 | 0.25 | 0.15 |
| Pierce | 0.11 | 0.29 | 0.06 | 0.52 | 4.8 | 0.09 | 0.09 | 0.03 |
| Dirats | 0.15 | 0.31 | 0.06 | 0.50 | 4.8 | 0.08 | 0.09 | 0.03 |

A3.3.1 Metallography

This alloy is not sensitized but has considerable grain boundary **Beta** and may have more than 15 mg/cm² mass loss in ASTM G 67^[3]. Metallographs are shown in Figures 33 and 34 for, respectively, longitudinal and transverse sections.

³ ASTM G 67 Test Method for Determining the Susceptibility to Intergranular Corrosion of 5xxx Series Aluminum Alloys by Mass Loss after Exposure to Nitric Acid

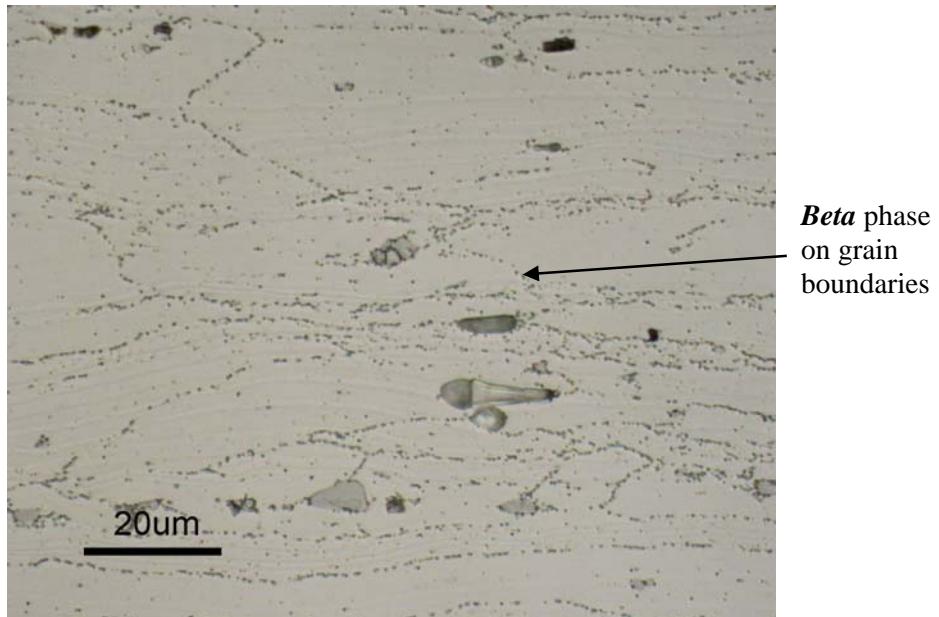


Figure 33. 5083 H321 – Longitudinal.

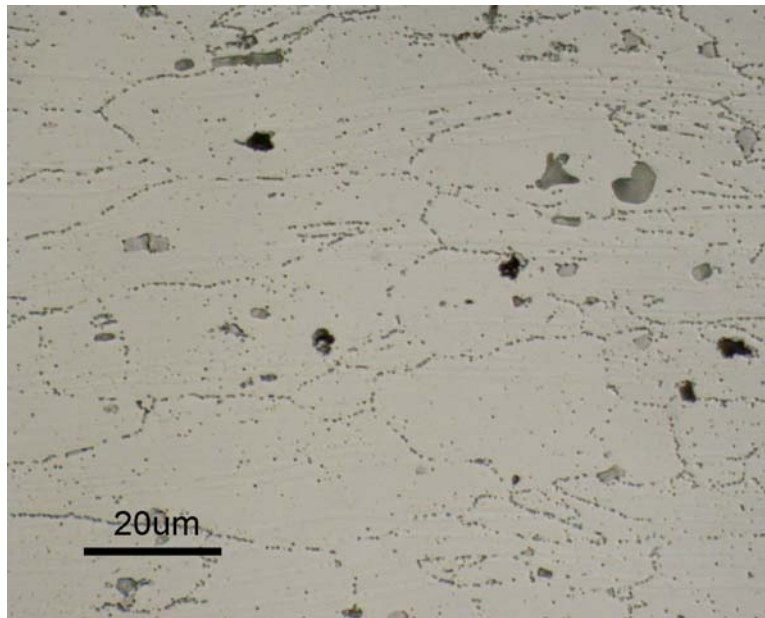


Figure 34. 5083 H321 – Transverse.

A3.4 Alloy 5086 H32

For 5086 H116, Pierce, Warminster, Pa, supplied 5086 H32 to ASTM B 209 manufactured by Capral (Australia).

The alloy supplied met ASTM B 928 for mechanical properties and chemical composition, respectively, Tables 11 and 12, with the exception of yield strength.

The alloy met ASTM G 66^[4] for exfoliation susceptibility. ASTM G 67 was not required in ASTM B 209 to which the alloy was supplied.

Table 11. Mechanical Properties – 5086 H32.

| Source | | 0.2% Yield Strength, ksi | | Tensile Strength, ksi | | % Elongation |
|--|---------|--------------------------|-----|-----------------------|-----|--------------|
| | | min | max | min | max | min |
| B 928 | | 28.0 | — | 40.0 | — | 10 |
| Pierce | | 34.8 | | 46.3 | | 18 |
| Dirats | Long. | 27.0* | | 45.8 | | 15.1 |
| | Transv. | 27.0 | | 46.0 | | 19.4 |
| Dirats Reduction of Area: Long., 16.8%, Transv., 34.2% | | | | | | |
| * Outside specification limits | | | | | | |

Table 12. Chemical Composition – 5086 H32.

| Source | Weight Percent Maximum unless shown as Range | | | | | | | |
|--------|--|------|------|------------|-----------|-----------|------|------|
| | Si | Fe | Cu | Mn | Mg | Cr | Zn | Ti |
| B 928 | 0.40 | 0.50 | 0.10 | 0.20 - 0.7 | 3.5 - 4.5 | 0.05—0.25 | 0.25 | 0.15 |
| Pierce | 0.17 | 0.27 | 0.03 | 0.38 | 3.8 | 0.07 | 0.02 | 0.01 |
| Dirats | 0.14 | 0.31 | 0.07 | 0.45 | 3.79 | 0.19 | 0.03 | 0.03 |

A3.4.1 Metallography

This alloy is not sensitized and has the least grain boundary **Beta** of the three alloys examined. Metallographs are shown in Figures 35 and 36 for, respectively, longitudinal and transverse sections.

⁴ ASTM G 66-95 *Test Method for Visual Assessment of Exfoliation Corrosion Susceptibility of 5xxx Aluminum Alloys*.

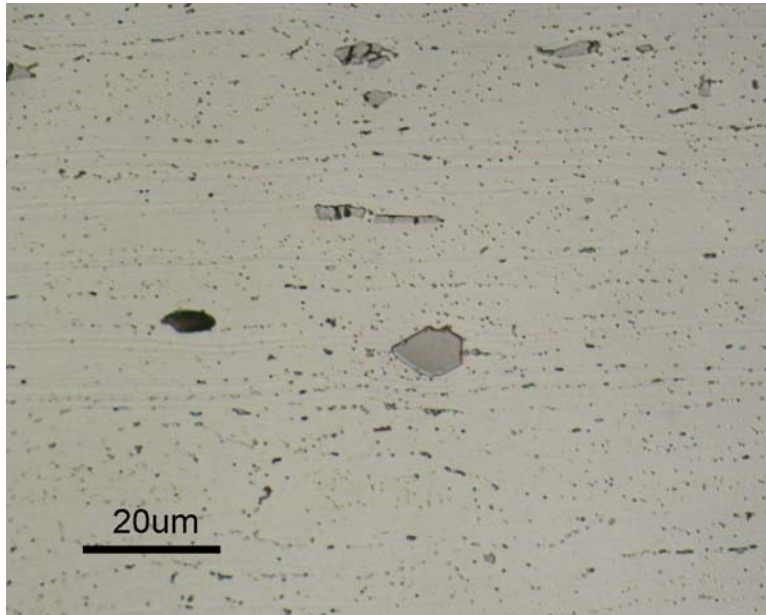


Figure 35. 5086 H32 – Longitudinal.

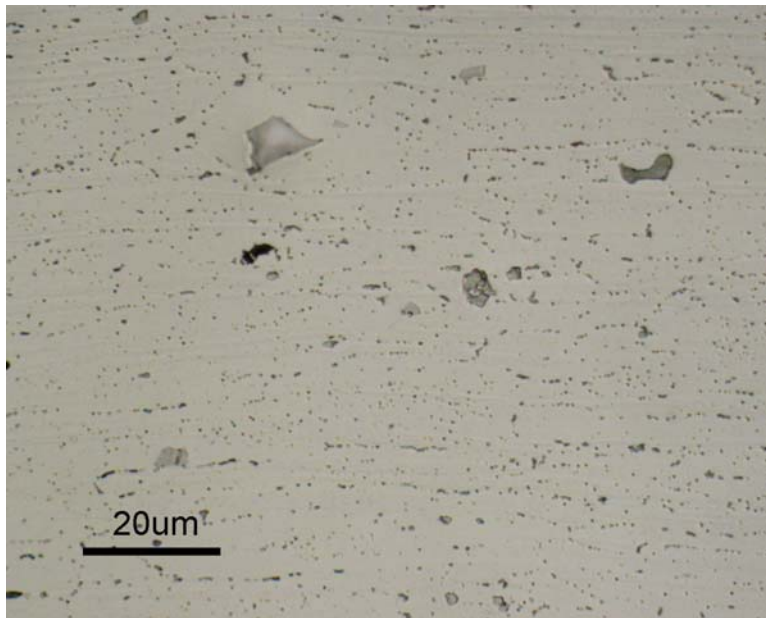


Figure 36. 5086 H32 – Transverse.

A3.5 Alloy 5383 H3116

For 5383 H116, Pierce, New Orleans, La, supplied 5383/5083 H116 to ASTM B 209 manufactured by Pechiney (France).

The alloy supplied met ASTM B 928 for mechanical properties and chemical composition, respectively, Tables 8 and 9.

The alloy met ASTM G 66 for exfoliation susceptibility. ASTM G 67 is not required in ASTM B 209 to which the alloy was supplied.

Table 13. Mechanical Properties – 5383 H116.

| Source | | 0.2% Yield Strength, ksi | | Tensile Strength, ksi | | % Elongation |
|--|---------|--------------------------|-----|-----------------------|-----|--------------|
| | | min | max | min | max | min |
| B 928 | | 33.0 | — | 48.0 | — | 10 |
| Pierce Certificate | | 36.3 — 40.7 | | 50.9 — 53.4 | | 16 — 17 |
| Dirats | Long. | 39.2 | | 54.2 | | 13.8 |
| | Transv. | 35.4 | | 53.3 | | 17.3 |
| Dirats Reduction of Area: Long., 16.3%, Transv., 27.7% | | | | | | |

Table 14. Chemical Composition – 5383 H116.

| Source | Weight Percent Maximum unless shown as Range | | | | | | | |
|--|--|--------------|------|--------------|-----------|------|------|------|
| | Si | Fe | Cu | Mn | Mg | Cr | Zn | Ti |
| B 928 | 0.25 | 0.25 | 0.20 | 0.7 - 1.0 | 4.0 - 5.2 | 0.25 | 0.40 | 0.15 |
| Pierce | 0.10 | 0.28* | 0.06 | 0.56* | 4.73 | 0.11 | 0.08 | 0.03 |
| Dirats | 0.13 | 0.29* | 0.06 | 0.53* | 4.76 | 0.10 | 0.08 | 0.03 |
| <i>Zr: ASTM B 928, 0.20% max., Pierce, 29 ppm, Dirats, 0.01%</i> | | | | | | | | |
| <i>* Outside specification limits</i> | | | | | | | | |

A3.5.1 Metallography

This alloy is not sensitized and has less grain boundary Beta than the 5083 H321 alloy examined. Metallographs are shown in Figure 37 and 38 for, respectively, longitudinal and transverse sections.

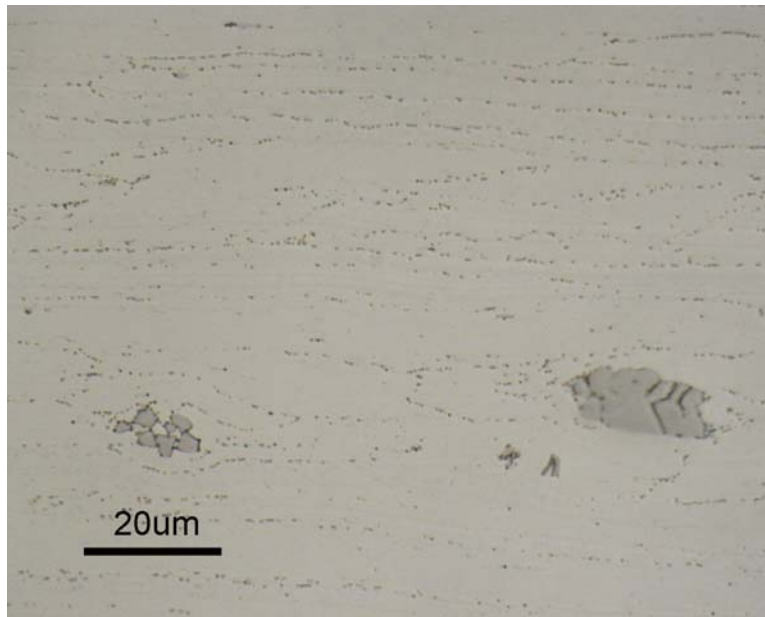


Figure 37. 5383 H116 – Longitudinal.

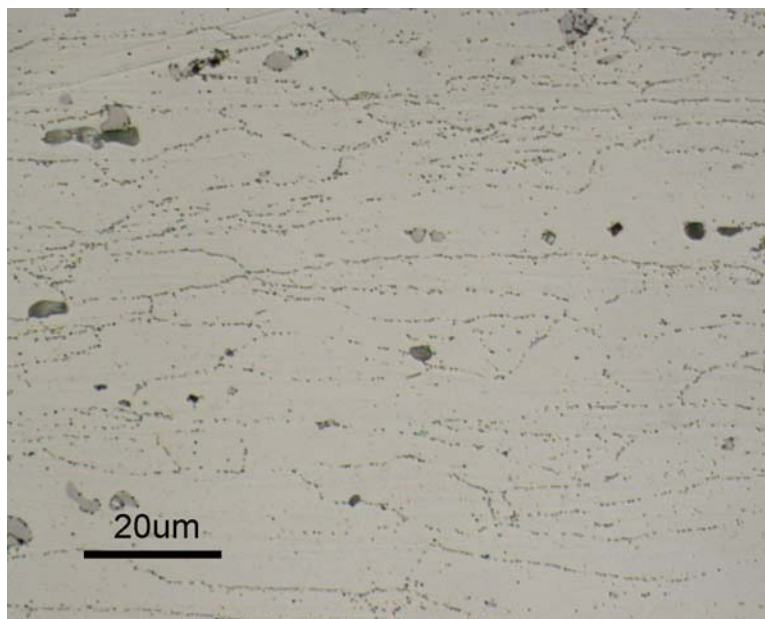


Figure 38. 5383 H116 – Transverse.

A3.6 Stress-Strain Curves

Dirats Laboratories, Westfield, Massachusetts, performed additional tensile tests on the three alloys to determine the engineering and true stress-strain curves.

The *tension specimens* were cylindrical with a test-section diameter of 0.25 in and a gage-length of 1 in and were taken in the transverse direction (with respect to rolling direction) from each of the three 0.5 in thick alloys. The engineering and true stress-strain properties are listed in, respectively, Tables 15 and 16.

Table 15. Transverse Engineering Mechanical Properties.

| Alloy | 0.2% Yield Strength, ksi | Tensile Strength, ksi | Percent Elongation in 1 inch | Percent Reduction of Area |
|-----------|--------------------------|-----------------------|------------------------------|---------------------------|
| | Transv. | Transv. | Transv. | Transv. |
| 5083 H321 | 34.4 | 51.9 | 19.4 | 37.9 |
| 5086 H32 | 27.0 | 46.1 | 24.0 | 34.7 |
| 5383 H116 | 35.0 | 53.3 | 22.6 | 28.1 |

Table 16. Transverse True Mechanical Properties.

| Alloy | 0.2% Yield Strain, ϵ_{YS} , in/in | Young's Modulus, E, ksi | Strain-hardening Exponent, n | Strength Coefficient, k, ksi |
|-----------|--|-------------------------|------------------------------|------------------------------|
| | Transv. | Transv. | Transv. | Transv. |
| 5083 H321 | 0.00505 | 11,300 | 0.155 | 79.2 |
| 5086 H32 | 0.00422 | 12,200 | 0.202 | 77.4 |
| 5383 H116 | 0.00505 | 11,500 | 0.158 | 81.9 |

The strain-hardening exponent n and the strength coefficient k are the parameters of the Ramberg-Osgood model of the true stress-strain curve

$$\epsilon = \frac{\sigma}{E} + \left(\frac{\sigma}{k} \right)^{1/n} \quad (A-1)$$

where

- ϵ true strain = $\ln(1 + e)$
- σ true stress = $s(1 + e)$
- e engineering strain
- s engineering stress
- E Young's Modulus.

The stress-strain curves are shown for 5083 H321, 5086 H32 and 5383 H116 in, respectively, Figures 39, 40 and 41.

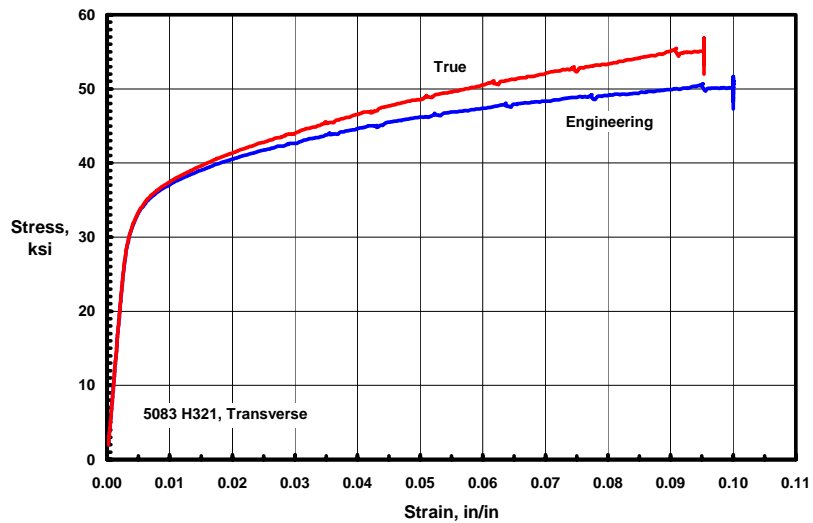


Figure 39. 5083 H321 – Transverse Stress-Strain Curves.

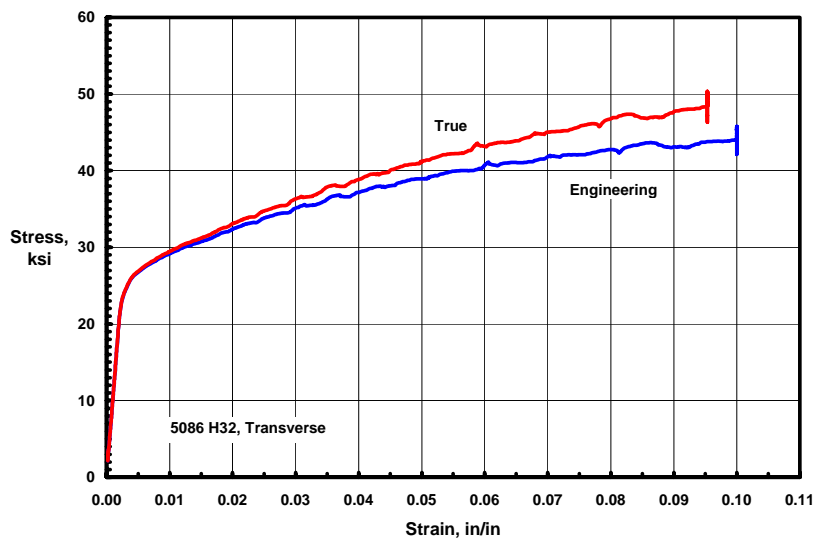


Figure 40. 5086 H32 – Transverse Stress-Strain Curves.

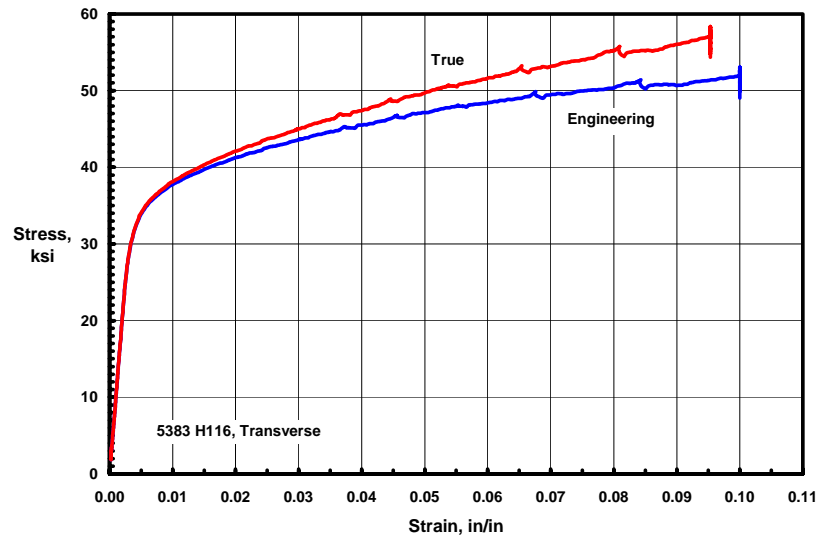


Figure 41. 5383 H116 – Transverse Stress-Strain Curves.

Annex B – FCGR Methodology

AN INTEGRATED METHODOLOGY FOR SEPARATING CLOSURE AND RESIDUAL STRESS EFFECTS FROM FATIGUE CRACK GROWTH RATE DATA

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Abstract—To properly interpret the results of standard fatigue crack growth tests it is often necessary to incorporate corrective techniques to the ΔK applied data. This is especially true in the near-threshold regime where long crack data need to be closure corrected to predict small crack behavior. It is also an issue in the presence of residual stress. A methodology to separate the influence of sample size, geometry, crack length, and residual stress from the standard crack growth test data to obtain a true material response is presented. Stress ratio and residual stress contributions from known combinations of assumed crack size, applied stress, and residual stress are also addressed and incorporated in the fatigue crack growth behavior.

NOMENCLATURE

| | |
|----------------------|--|
| a | = crack length |
| a_i | = notch length before crack initiation |
| a_n, a_{n+1} | = current crack lengths measured at two successive steps n and $n+1$ |
| da | = change in crack length |
| ACR | = adjusted compliance ratio |
| C_o | = $\Delta\delta_{app}/\Delta P$, compliance above the opening load |
| C_s | = $\Delta\delta_{eff}/\Delta P$, secant compliance |
| C_i | = $\Delta\delta_i/\Delta P$, compliance of the notch before crack initiation |
| E | = modulus of elasticity |
| n | = K_{max} sensitivity exponent |
| P_{max} | = maximum load |
| P_{min} | = minimum load |
| P_{op} | = opening load |
| P_0 | = zero load |
| R | = ratio of minimum to maximum load or stress |
| $Z(a)$ | = influence function |
| $d\delta$ | = change in displacement due to change in crack length |
| $d\delta_{max}$ | = change in displacement at maximum load due to change in crack length |
| $d\delta_{res}$ | = change in displacement due to residual stress and change in crack length |
| $\Delta\delta_{max}$ | = change in displacement at maximum load due crack advance from notch |
| $\Delta\delta_{app}$ | = closure free displacement range |
| $\Delta\delta_{eff}$ | = actual measured displacement range |
| $\Delta\delta_i$ | = measured displacement range before crack initiation |
| $\Delta\delta_{cl}$ | = $\Delta\delta_{app} - \Delta\delta_{eff}$, displacement difference due to closure |
| K | = stress intensity factor |
| K_{res} | = stress intensity due to residual stress |
| K_{max} | = maximum stress intensity |
| K_{ocmn} | = normalized stress intensity |
| ΔK | = stress intensity range |
| ΔK_{app} | = applied stress intensity range |
| ΔK_{eff} | = effective stress intensity range |
| ΔK_{cl} | = $\Delta K_{app} - \Delta K_{eff}$, stress intensity reduction due to closure |

Fatigue & Fracture of Engineering Materials – Special Issue Contribution (in press)

INTRODUCTION

Steady-state fatigue crack growth data generated for long cracks (corresponding to fatigue crack growth testing conducted on compact tension C(T), middle tension M(T), etc. specimens) can be altered by various external effects and often do not represent the true behavior of the material investigated. Such effects have various origins. One is related to the existence of closure mechanisms, active behind the crack tip, which create differences between long crack growth data (ΔK_{app}) and naturally initiated or small crack growth data (ΔK_{eff}) and can lead to non-conservative estimations of fatigue life. Another source of errors when incorporating long crack growth data in design is associated with the presence of externally induced (or global) compression or tension residual stresses [1,2,3]. In this case, sample size and/or geometry can produce variability in the data generated on virtually identical materials, and crack length can also play an important role. Numerous attempts to resolve these issues and normalize data generated under various specimen/testing conditions have been made in the past, but no comprehensive method able to appropriately handle all these effects has yet been proposed. Thus, in this study, a methodology able to successively handle these effects is proposed.

PROPOSED METHODOLOGY

The methodology correlates fatigue crack growth rate (FCGR) data from samples with either tensile, compressive or no residual stress using a combination of compliance measurement techniques, K-control, adjusted compliance ratio (ACR) crack closure measurement techniques, on-line crack-compliance K residual calculations and K_{max} sensitivity concepts. The resulting FCGR curve is a material property response that has been de-coupled from the confounding effects of crack length, test coupon geometry and residual stress. As opposed to the traditional life prediction models, this methodology uses normalized data representative of a zero stress ratio ($R = 0$) with no remote closure (small crack behavior). Stress ratio effects can be further incorporated in fatigue crack growth data by back calculating ΔK_{eff} from the normalized K. Although it is believed that this approach gives the most reliable life prediction methodology, it is difficult to compare this process to more traditional methods since evaluations of residual stress and remote closure are generally not obtained during standard crack growth rate tests.

There are two fundamental reasons why data from large samples with long cracks may not be representative of the crack growth behavior of small cracks:

- 1) In the presence of global residual stress (for example, caused by quenching as part of heat treatment), the larger the sample size relative to the original component, the greater the degree of residual stress captured in the machined sample. Also, edge crack samples and center crack samples generally exhibit different behavior if extracted from the same location within the original component.
- 2) The larger the sample and crack size, the smaller the applied stress for a given stress intensity. This point serves to amplify both the effects of remote closure and residual stress compared to test coupons with smaller crack sizes and higher stresses.

It is proposed that for common long crack test samples, a proper analytical evaluation of the fatigue crack growth rate data involves the following steps:

1. Generate da/dN data using compliance measurement techniques and K-control.
2. Determine the effective stress intensity using the ACR method.
3. If possible, adjust for residual stress using the on-line crack-compliance method.

4. Use K_{max} sensitivity concepts to incorporate residual stress effects into the normalized (or master) crack growth rate curve.
5. Reintroduce stress ratio effects into the master curve from the knowledge of crack size, applied stress and residual stress in the structure.

Each of these steps will be detailed below:

1. Compliance measurement and K -control

K -control methodology offers advantages for fatigue crack growth data generation and uses a constant value of the expression $(1/K) \cdot (dK/da)$ to control the K profile. A negative value of this expression is used for decreasing K (near-threshold) and a positive value for increasing K (mid to upper Region II and Region III). This effectively results in a greater ΔK range over the same increment of crack extension. The details on the K -control procedure suggested in ASTM E647 were first performed in the 1970's (see Ref. [4]). Experience has shown this procedure substantially reduces the test time and cost necessary to generate fatigue crack growth data with no adverse impact on the test result.

When practical, the compliance method of monitoring crack length is used. The method has the advantage of higher resolution than either visual methods or the indirect potential drop method (foil gages) because the method averages the through-the-thickness crack length instead of the somewhat more discontinuous growth of the crack on the surface. When sample type and test temperature permit, the compliance method is generally preferred because of the added advantage that crack closure can be evaluated. Both the ASTM 2% offset opening load method [5] and the adjusted compliance ratio (ACR) method [6] are based on compliance data. The non-visual crack length measurement methods should be complemented by periodic visual measurements of the crack, both for validity purposes and for post-test analysis corrections to the original raw data.

Besides the commonly recognized closure mechanisms, macro residual stress-crack closure may significantly influence fatigue crack growth rate data. Therefore, in addition to measuring crack closure (using compliance measurements), notch closing or opening measurements are recommended on compact tension, C(T), samples before and after machining the notch as a means of evaluating/separating the individual influence of residual stress on/from the crack growth rate behavior. The significance of this statement including the impact of these observations on fatigue crack growth rates can be found elsewhere [7].

2. Adjusted Compliance Ratio (ACR) method

Since Elber introduced the concept of crack closure, it has become a widely used tool to explain the extrinsic response of fatigue crack growth rate behavior. Crack closure is a crack tip shielding mechanism whereby the crack-tip cyclic strain is partially shielded from damaging stress. The source of this shielding is most commonly caused by crack wake interference due to roughness (microstructure), oxides, plasticity, and/or residual stress. The experimental measurement of crack closure has been hampered by widely varying and non-repeatable methods of evaluation. Furthermore, experimental observations are subject to varying and inconsistent methods of interpretation. In an attempt to improve consistency of measurement, ASTM E647 has introduced an automated offset opening load technique. After two round-robin programs, this method was adopted as an annex to the ASTM E647 standard. However, this method often overcorrects the ΔK applied data primarily because the method fails to account for evidence of crack tip cyclic strain below the opening load [6]. This is especially important if the closure mechanism is not necessarily near the crack tip but distributed along the full wake of the crack or near the notch.

The ACR method of determining the effective stress intensity has been useful in accounting for compressive residual stress and other sources of remote closure resulting in an intrinsic FCGR curve that is thought to emulate small crack growth behavior. The method uses the same load-displacement records as the opening load method, but it accounts for partial closure effects (effects below the opening load). The assumption of crack tip activity below the opening load is most relevant at opening loads that are a large fraction of the applied load, such as the near-threshold regime. The ACR technique attempts to account for strain fields at the crack tip, below K_{op} , caused by interaction of the mating broken faces along the crack wake. Below K_{op} , the interference strains induce an additional K at the crack tip, which is added to the K_{min} , thus reducing the ΔK_{eff} , while above K_{op} only the applied force contributes directly to K_{app} .

This method estimates ΔK_{eff} using the ratio of the actual displacement range ($\Delta\delta_{eff}$) to the displacement range that would have occurred in the absence of closure ($\Delta\delta_{app}$) (Figure 1). This method uses remote (front face) displacement measurements because the local crack tip strain is impractical or impossible to obtain. The displacements are a “quantitative” measure of the “qualitative” strain activity of the broken surfaces in the crack wake. Displacement measurements are evaluated relative to the original displacement of the notch at the beginning of the test, and therefore the adjusted compliance ratio is calculated by subtracting the initial notch displacement from both displacements in the presence and the absence of closure:

$$ACR = (\Delta\delta_{eff} - \Delta\delta_i) / (\Delta\delta_{app} - \Delta\delta_i) \quad (1)$$

Converting to compliance, the expression for ACR becomes:

$$ACR = (C_i - C_i) / (C_o - C_i) \quad (2)$$

where

$C_i = \Delta\delta_{eff}/\Delta P$ is the secant compliance

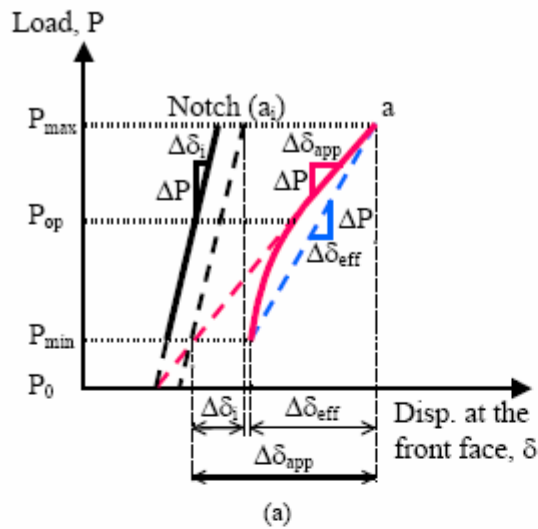
$C_o = \Delta\delta_{app}/\Delta P$ is the compliance above the opening load

$C_i = \Delta\delta_i/\Delta P$ is the compliance of the notch before crack initiation

Once ACR is determined, ΔK_{eff} can be calculated as:

$$\Delta K_{eff} = ACR \cdot \Delta K_{app} = \frac{\Delta\delta_{eff} - \Delta\delta_i}{\Delta\delta_{app} - \Delta\delta_i} \cdot \Delta K_{app} = \frac{C_i - C_i}{C_o - C_i} \cdot \Delta K_{app} \quad (3)$$

Experimental evidence shows that when the initial un-cracked compliance, C_i , is subtracted from both the numerator and denominator of the compliance ratio, the resulting ACR is measurement-location insensitive [6]. The similarity between the ACR method and the on-line crack compliance method (see Ref. 8 and Section 4) is shown in Figures 1 and 2. Either method gives an identical result for the calculation of ΔK_{eff} . In the first case, Figure 1, ΔK_{eff} is calculated directly from the ratio of compliances. In the second case, Figure 2, ΔK_{ci} is calculated directly and then subtracted from ΔK_{app} to determine ΔK_{eff} .



$$\Delta K_{eff} = ACR \cdot \Delta K_{app}$$

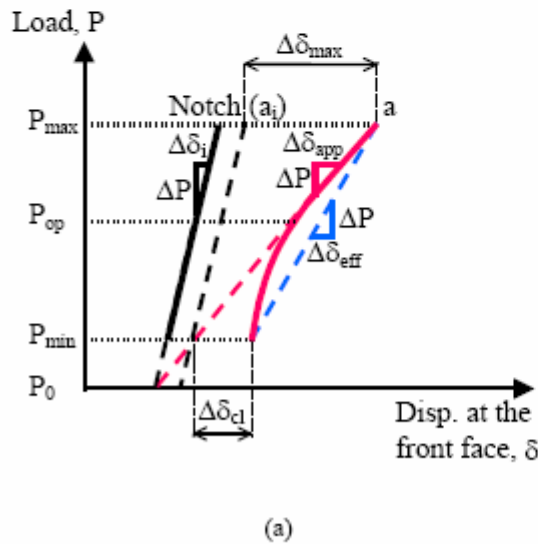
where

$$ACR = \frac{\Delta \delta_{eff} - \Delta \delta_i}{\Delta \delta_{app} - \Delta \delta_i}$$

or

$$ACR = \frac{C_s - C_i}{C_o - C_i}$$

Fig. 1. (a) Load-displacement records showing the critical parameters in the ACR method [6,10];
(b) equations used in the ACR method.



$$\Delta K_{eff} = \Delta K_{app} - \Delta K_{cl}$$

where

$$\Delta K_{cl} = \Delta K_{app} \cdot \frac{\Delta \delta_{cl}}{\Delta \delta_{max}}$$

$$\frac{\Delta K_{cl}}{\Delta K_{app}} = 1 - ACR = 1 - \frac{\Delta K_{eff}}{\Delta K_{app}}$$

Fig. 2. (a) Load-displacement records showing the parameters used in the on-line crack-compliance technique for global closure correction; (b) equations used in the on-line crack-compliance technique for global closure correction.

Recently, a fracture mechanics based analysis providing mathematical foundation for residual stress and crack closure correction methodologies has been developed [8], and good agreement between this analysis and the ACR method was observed. It should be noted that the complexity and the unknown distribution of forces in the crack wake combined with the increasingly larger increments of crack extension used for calculating the ACR make the solution a good approximation rather than an exact solution. The effectiveness of the ACR method has been demonstrated in two recent publications [9,10], which show good correlations between small crack growth data and ACR corrected long crack growth data. The data from reference [9] uses an open-hole corner crack sample whereas the data from reference [10] employs axially loaded corner-crack specimen geometry. Figure 3 [from Ref. 10] shows that the small crack data (triangles) closely matches the ACR corrected data from the long crack sample (stars). This figure also shows the lack of correlation between small crack behavior and the ASTM 2% offset opening load method (squares).

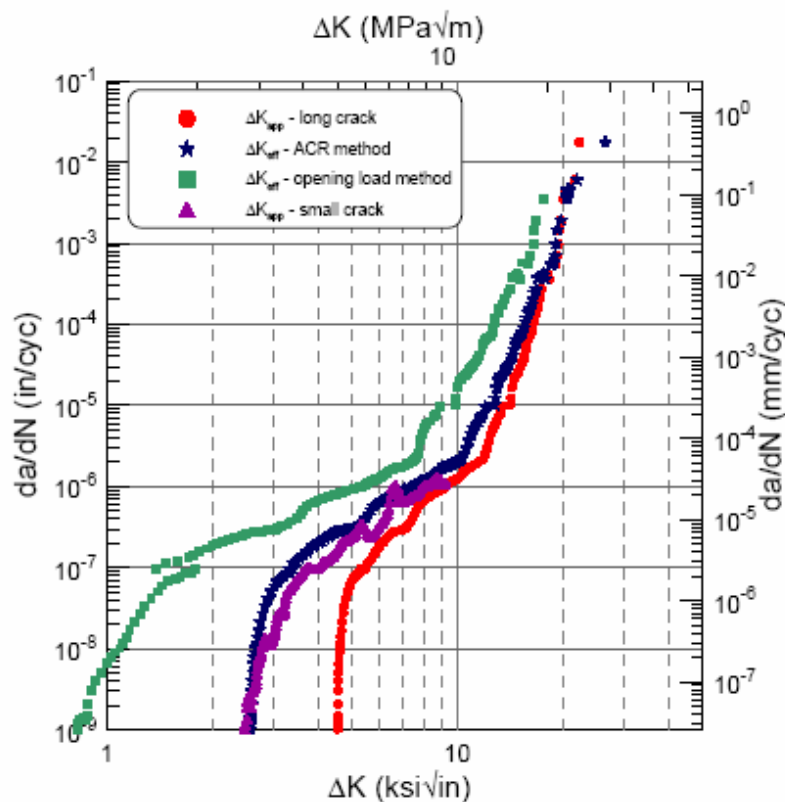


Fig 3. Comparison of long crack data, small crack data, and closure corrected data ($R=0.1$) for an Al-7%Si-0.45%Mg cast alloy [10] (circles = uncorrected long crack growth data; triangles = small crack growth data; stars = ACR corrected long crack growth data; squares = opening load corrected long crack growth data).

3. Real-time determination of K_{res} using on-line crack-compliance method

Recent advances in fracture mechanics derivations for closure corrections [8] have remarkably improved the understanding of the ACR closure concept with notable similarities between this concept and the cut-compliance method [7,11,12] for determining K_{res} . The on-line crack-compliance method of determining K_{res} during a crack growth test [8] is also similar to the cut-compliance method [7,11], but it can be applied during testing and without using influence functions. This is the result of the advances in the understanding of the ACR methodology and experimental evidence that both the on-line crack-compliance method and the ACR method are indeed measurement location insensitive.

The cut-compliance method of computing the stress intensity due to residual stress, K_{res} , was developed by Schindler [11] and is based on Castigliano's theorem. However, new influence functions have been developed [7,8] using front-face displacements instead of back-face strains:

$$K_{res} = \frac{E}{Z(a)} \cdot \frac{d\delta}{da} \quad (4)$$

The new on-line crack-compliance technique can be applied by extrapolating the slope of the load-displacement curve down to a displacement corresponding to zero load and paying careful attention to signal stability and load-displacement linearity. As the crack advances, a decrease in displacement at zero load indicates a compressive (negative) K_{res} , whereas an increase signifies tensile (positive) K_{res} . Tensile residual stress determination is straightforward since the tendency of the crack to open minimizes crack closure effects (Figure 4(a)). Compressive residual stress can also be measured as long as the slope of the load-displacement curve is determined above the closure level (Figure 4(b)). K_{res} can be determined by measuring the change in displacement (or strain) at maximum load for a given increment of crack extension and comparing this to the corresponding change in displacement (or strain) at zero load over the same increment of crack extension. The ratio of the displacement change at zero load ($d\delta_{res}$) to the displacement change at maximum load ($d\delta_{max}$) multiplied by K_{max} provides the K_{res} as shown below [8]:

$$K_{res} = K_{max} \cdot \frac{d\delta_{res}}{d\delta_{max}} \quad (5)$$

As mentioned earlier, the on-line crack-compliance technique can be applied without the need to calculate influence functions, $Z(a)$. It needs to be noted that both this approach and the ACR method are based on ratios of displacements and they are convenient to use due to their simplicity. Since a ratio of displacements is used to calculate K_{res} , the displacements need not be measured at the load-line. The practical application of this methodology requires sufficient signal stability and linearity to determine K_{res} . Furthermore, predominately elastic behavior is assumed since the influence of the crack tip plastic zone would contribute to erroneous calculations of K_{res} .

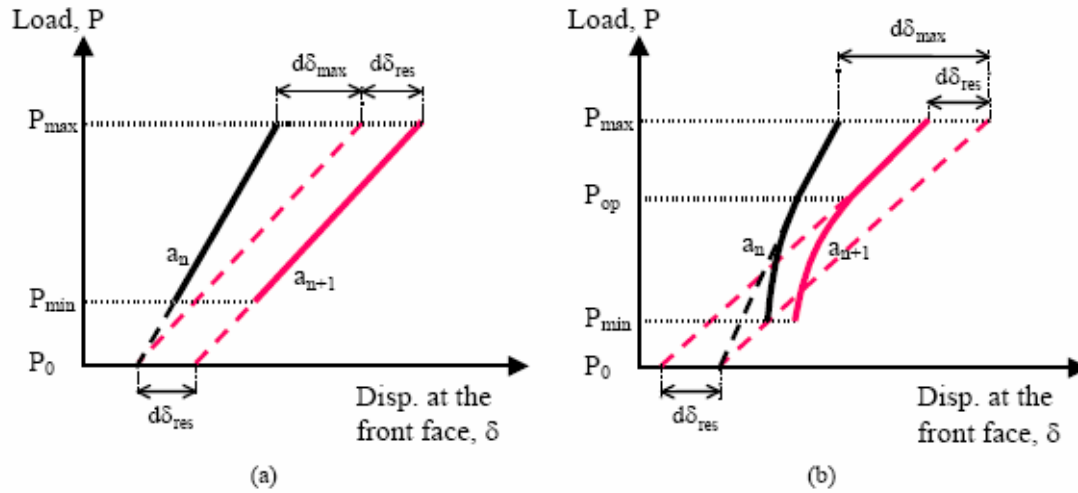


Fig. 4. Load-displacement records showing the critical parameters in the on-line crack-compliance residual measurement technique [8]: (a) tensile residual stress and (b) compressive residual stress; the dashed lines parallel with the a_{n-1} load-displacement (or tangent to the load-displacement) records represent residual stress free conditions.

4. K_{max} sensitivity

Compressive residual stress has a direct impact on the crack tip driving force, ΔK , especially at low stress ratios and at near-threshold crack growth rates. Tensile residual stress may only affect K_{max} since the crack can remain fully open even at the minimum load. Regardless of whether or not compressive or tensile residual stresses are present, correlating stress ratio effects using the ACR method often results in the observation that the FCGR response is determined not only by ΔK_{eff} but it also depends on K_{max} . It was also observed that this K_{max} dependence takes the form of a power law with the magnitude of the exponent being a measure of K_{max} sensitivity [13].

An earlier investigation of 2000, 6000, and 7000 series wrought aluminum alloys [14] has revealed a second order K_{max} effect that covers a wide range of crack growth rate data and stress ratios, Figure 5(a). In a similar manner to that proposed by Walker [15], a unique intrinsic FCGR curve can be obtained by normalizing the stress intensity according to the equation:

$$K_{norm} = \Delta K^{1-n} \cdot K_{max}^n \quad (6)$$

An empirically derived K_{max} sensitivity exponent $n = 0.25$ was shown to “collapse” the data, Figure 5(b) (see Ref. [10]). In order to correctly incorporate this K_{max} sensitivity concept, it is necessary to first determine the effective stress intensity using the ACR method. Then K_{res} needs to be added to K_{max} applied to give the total K in the K normalization process. Equation (6) then becomes:

$$K_{norm} = \Delta K_{eff}^{1-n} \cdot K_{max+residual}^n \quad (7)$$

The K_{max} sensitivity concept is intended to compensate for the interaction between ΔK and K_{max} under predominately elastic conditions and does not apply to Region III behavior. A methodology to correct Region III FCGR data for plasticity can be found elsewhere [16]. The magnitude of the K_{max} sensitivity exponent may vary according to material and environmental conditions. The correlation illustrated in this example may not apply as accurately to all combinations of growth rates and stress ratios for other material-environment systems.

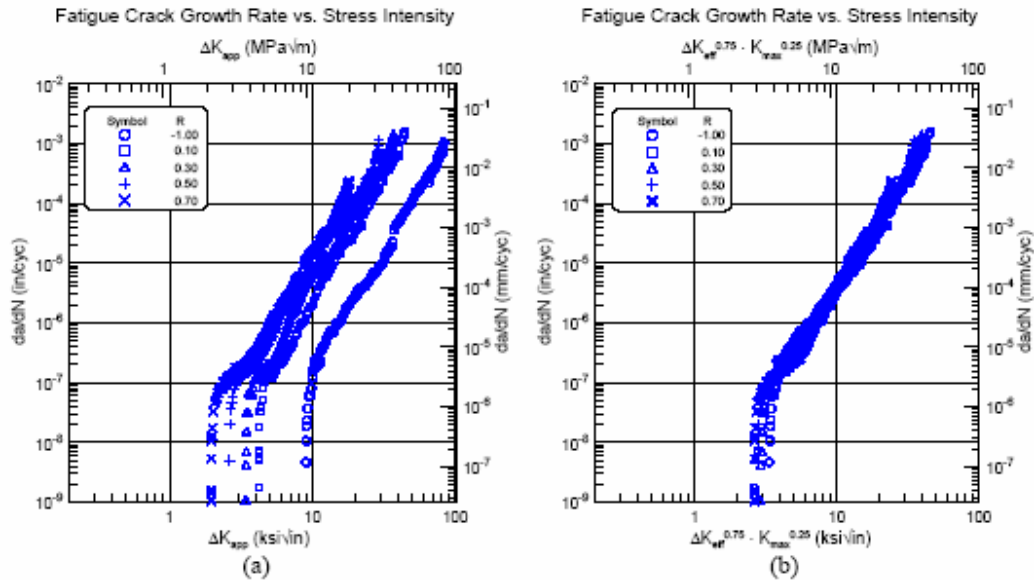


Fig. 5. Fatigue crack growth data of 2324-T39 Al showing: (a) ΔK_{app} and (b) K_{norm} after ACR correction.

5. Re-introducing stress ratio effects

The normalization process masks the effect of stress ratio, residual stress, and remote closure. Since remote closure is also affected by a combination of sample size and geometry, the resulting FCGR response is expected to be a good indicator of the material property for a physically small crack as long as the elastic K analysis is still valid. The physically small crack is larger than the mechanically small crack (where K is no longer valid) and the micro-structurally small crack (where behavior is governed by micro-structural constituents on the order of the crack size). The normalization process is not expected to mask out material property details such as orientation, environment or toughness-related behavior associated with upper Region II and Region III behavior. Thus, the normalization process allows a direct comparison between the responses of different materials and different environments.

In order to apply the normalized curve into a life prediction process, it is necessary to reintroduce the stress ratio effect and solve for ΔK . Recognizing that:

$$K_{max} = \frac{\Delta K}{(1 - R)} \quad (8)$$

Equation (7) can be rearranged to solve for ΔK_{eff} as shown in equation (9):

$$\Delta K_{eff} = K_{nom} \cdot (1 - R)^2 \quad (9)$$

Equation (9) re-evaluates a curve for each stress ratio of interest from the single normalized curve. Figure 6(a) shows the effect of stress ratio ($R = 0.1, 0.3, 0.5, \text{ and } 0.7$) after correcting for closure using the ACR method. In Figure 6(b), the stress ratio effect has been re-introduced using equation (9) for the normalized curve tested at a stress ratio $R=0.1$. After re-processing, Figure 6(b), data initially corresponding to one stress ratio closely match the data provided by the tests done under four different stress ratios (Figure 6(a)). Determining the proper stress ratio also requires knowledge of the applied stress and the residual stress for the structure.

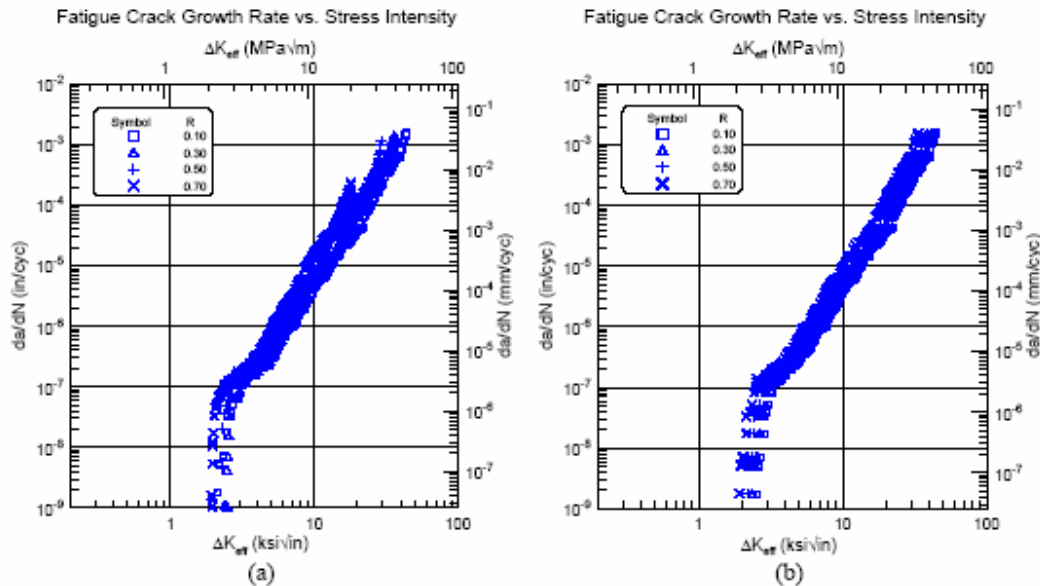


Fig 6. Fatigue crack growth curves showing: (a) original ΔK_{eff} data (using ACR method) and (b) ΔK_{eff} data from single normalized curve after re-introducing stress ratio effect.

SUMMARY

A methodology has been presented to assist in providing a unique intrinsic FCGR curve that is thought to emulate small crack growth behavior of a material. The proposed methodology should be considered a guideline since for several applications some of the presented techniques may be impractical (for example, compliance measurement on samples with small cracks or aggressive environments is often impractical). The ACR methodology is presented as a useful and easy to implement tool to compensate for closure contributions and to determine the small crack growth behavior. On-line K_{res} measurements are considered appropriate means to account for residual stress contributions as long as a high level of instrumentation precision, stability, and linearity can be achieved. K_{max} sensitivity corrections are introduced to broaden the usefulness of the methodology for life prediction since the FCGR curve (excluding Region III) can be normalized and expressed as a unique curve regardless of the stress ratio. A procedure to re-introduce stress ratio effects is also presented to allow the use of normalized data for life prediction.

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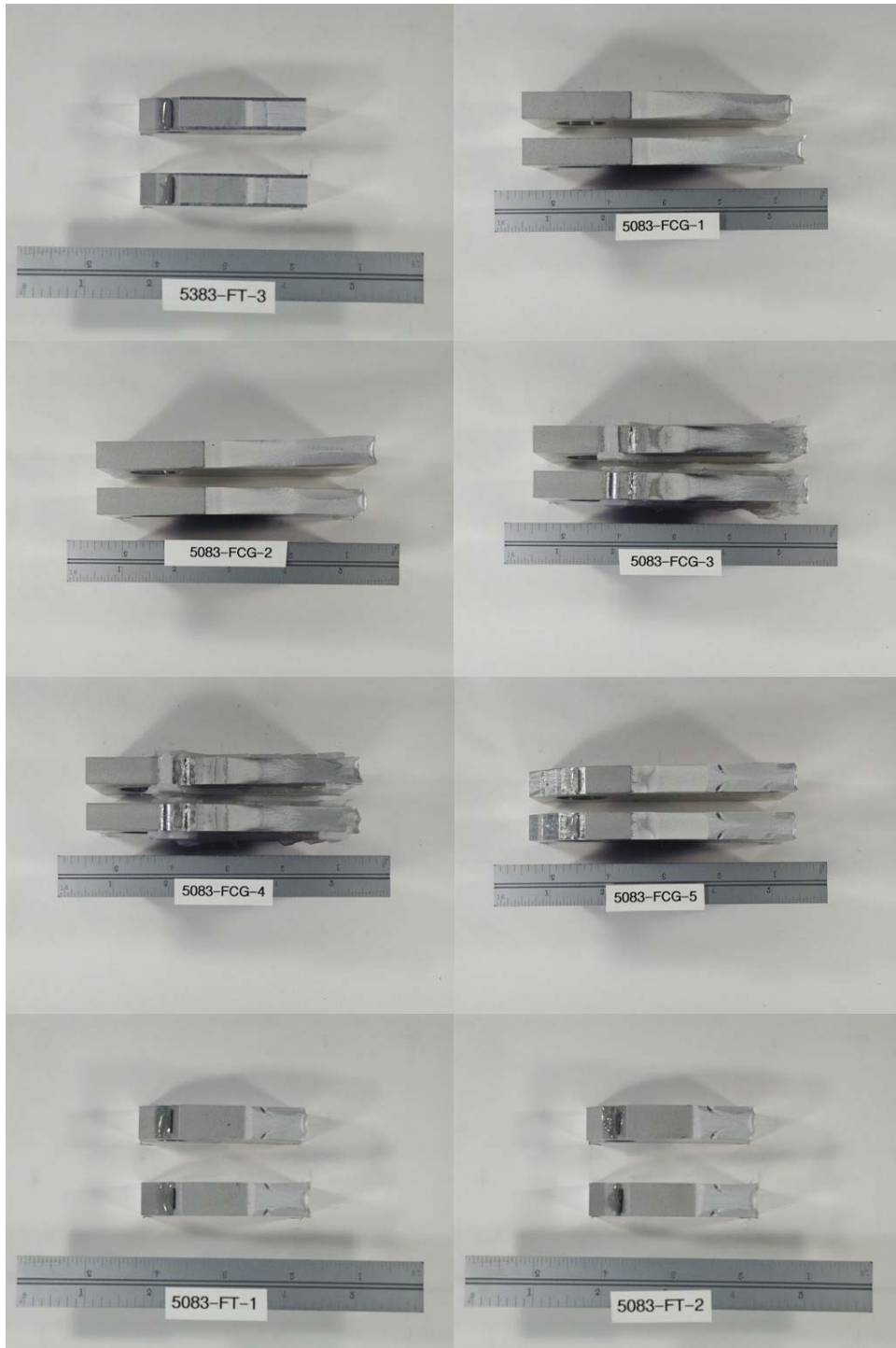
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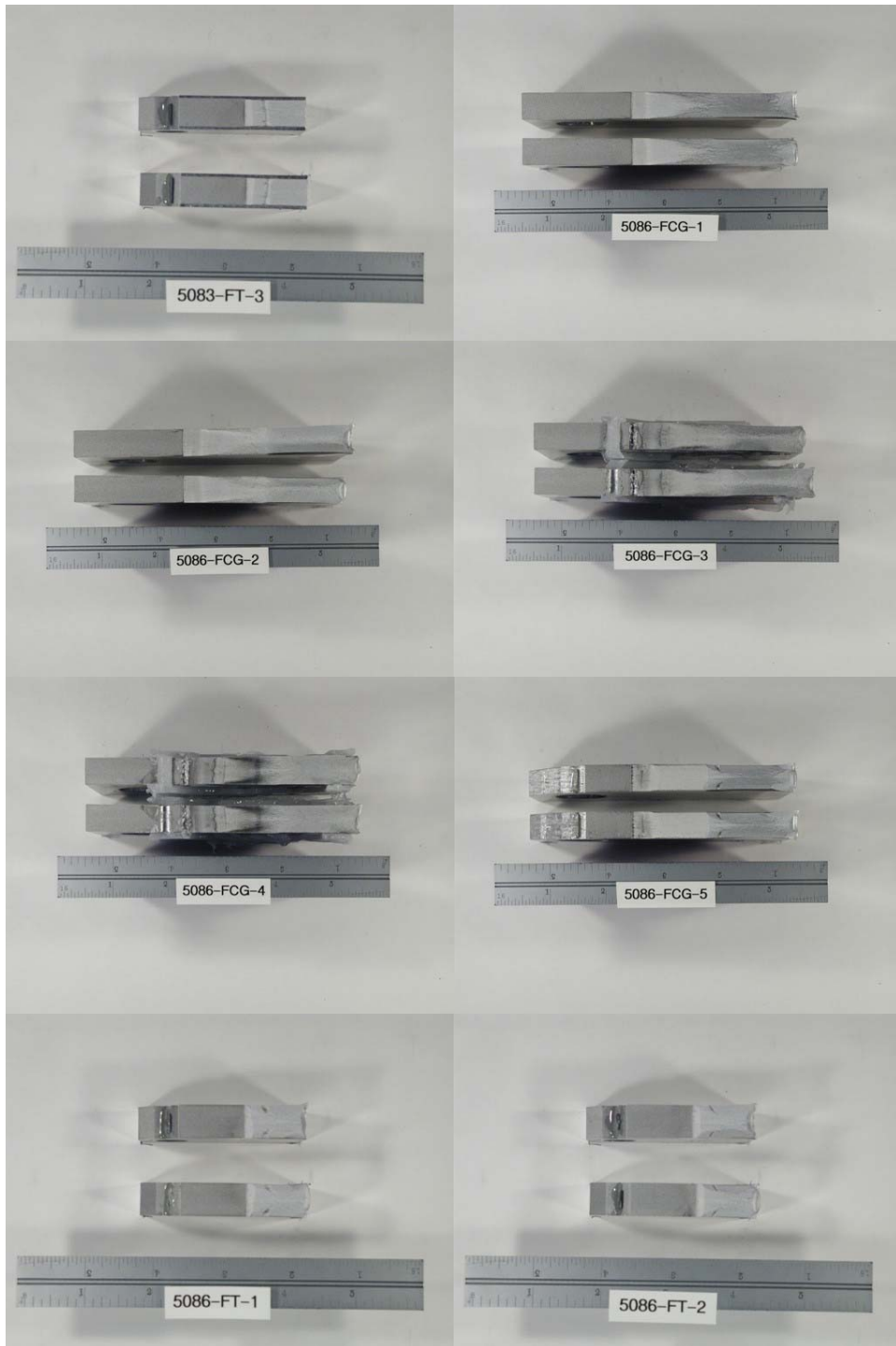
Annex C – Photographs of Test Samples

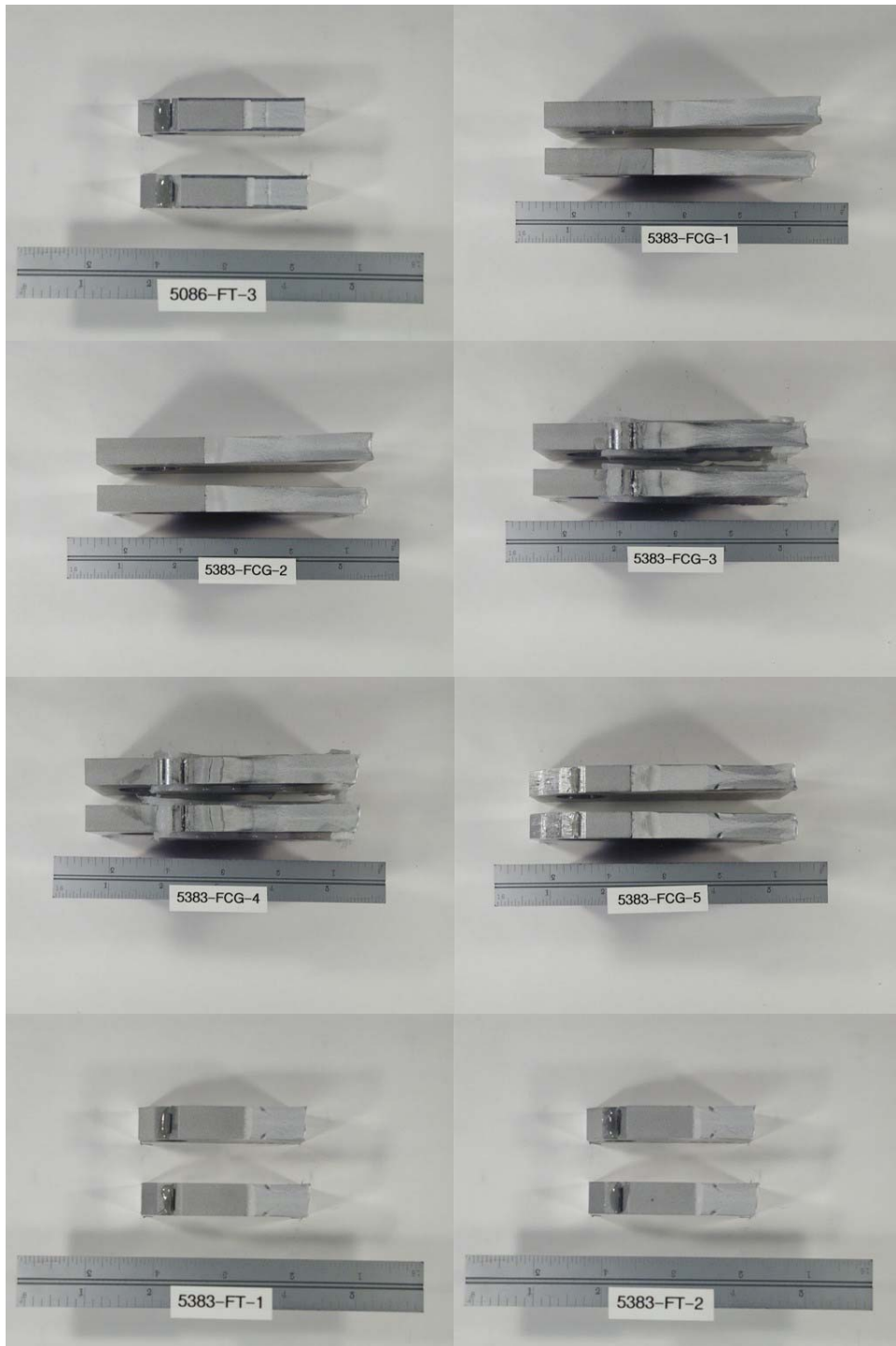






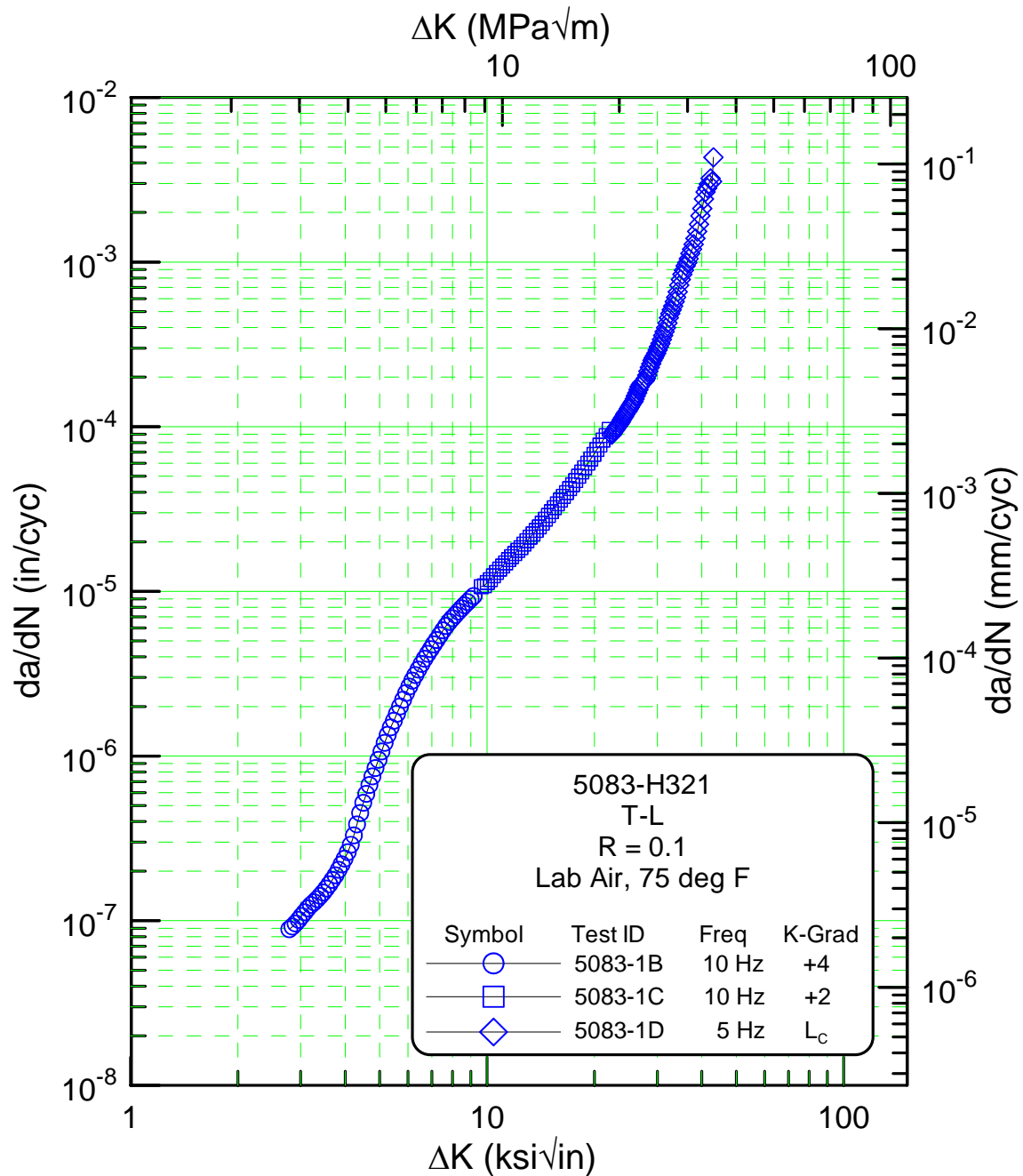




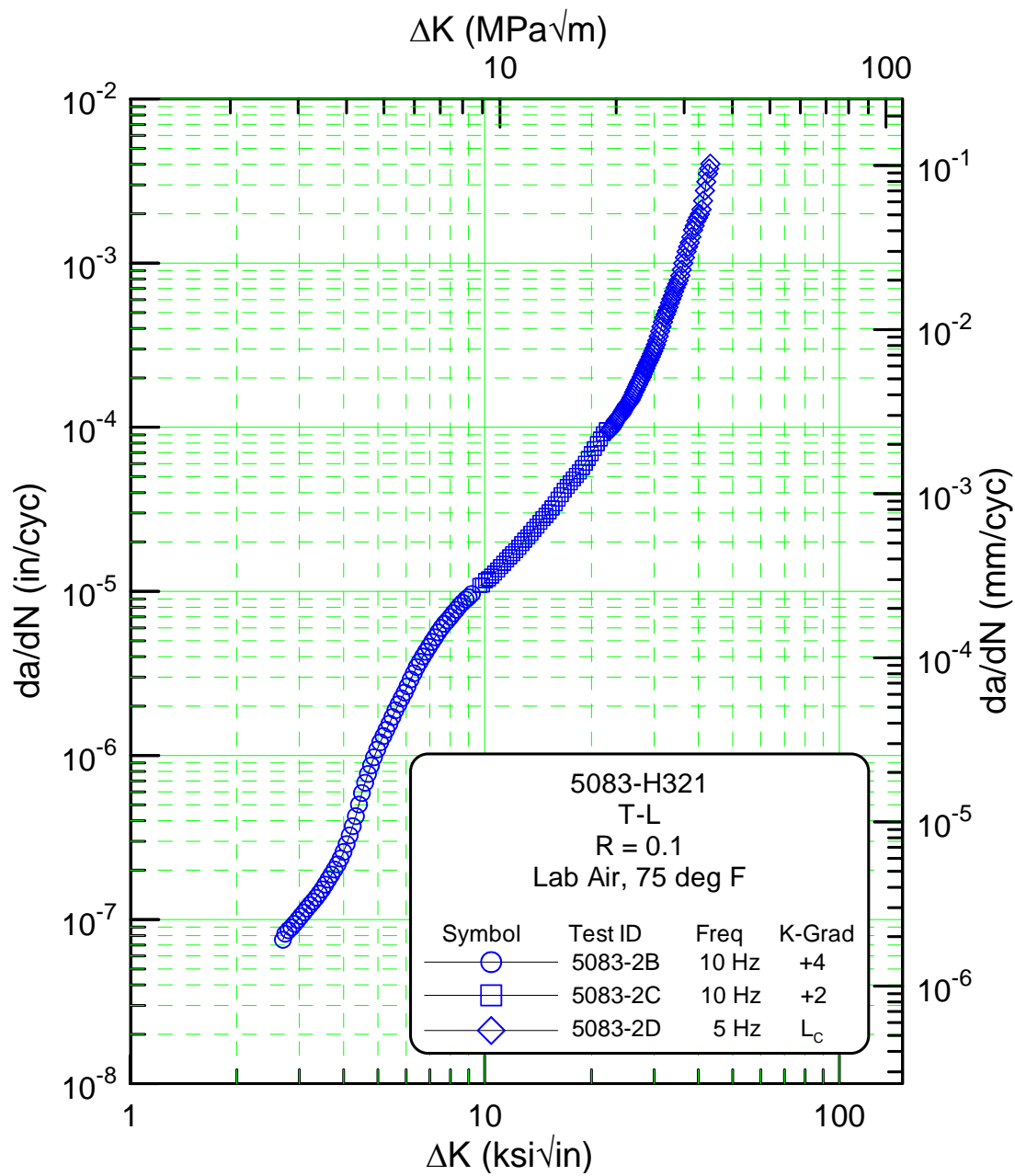


Annex D – Individual FCGR Curves

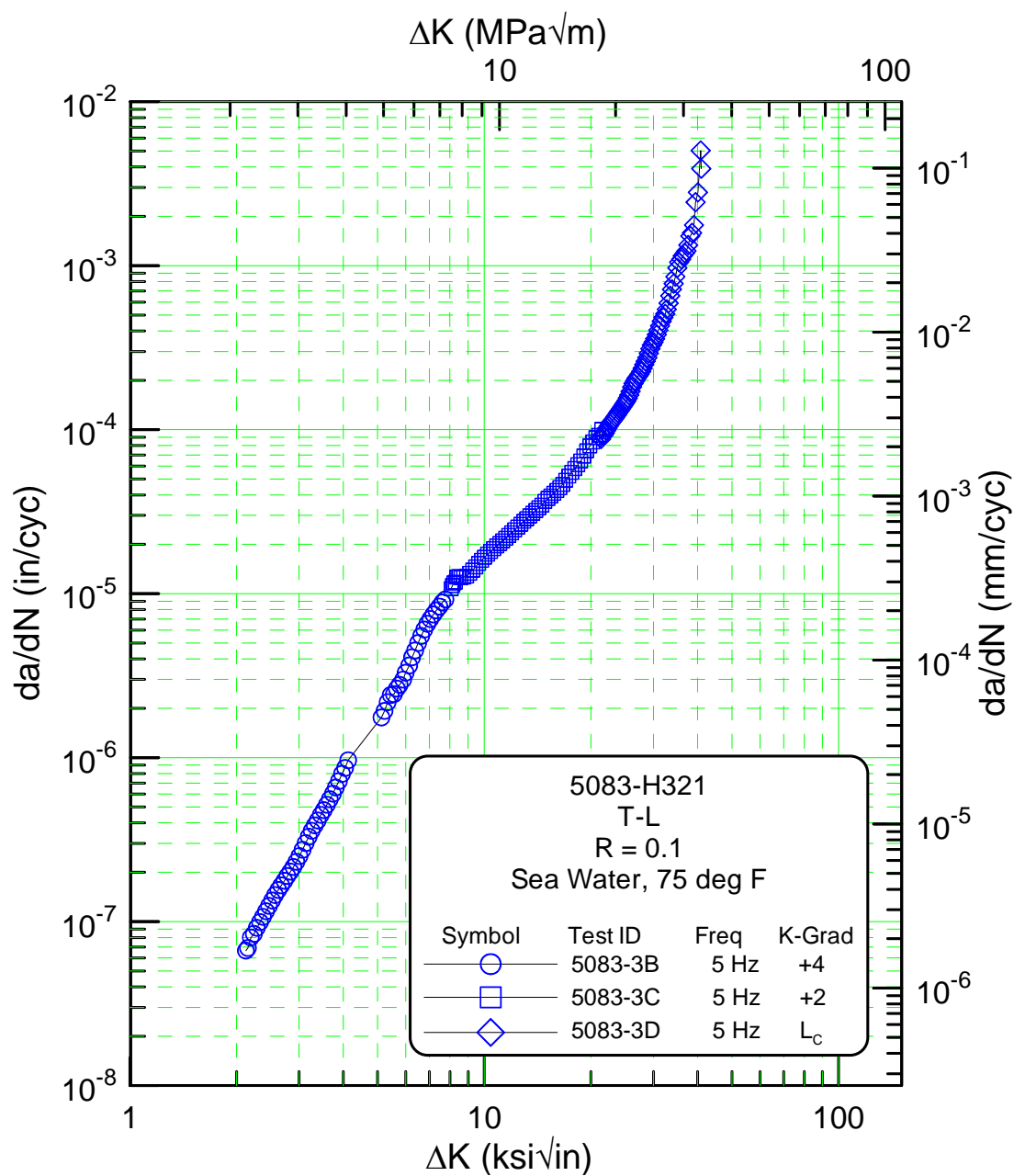
Fatigue Crack Growth Rate vs. Stress Intensity



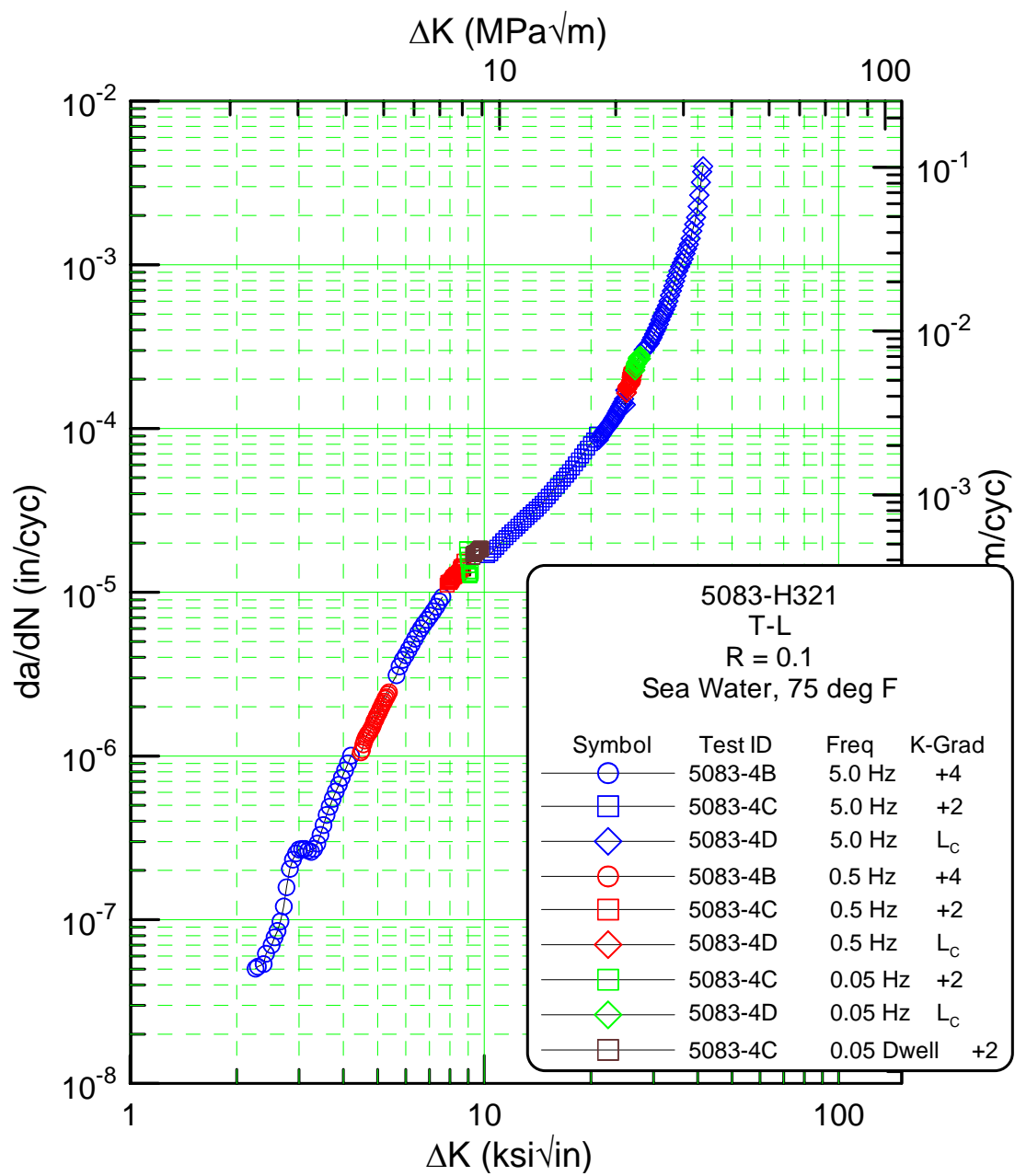
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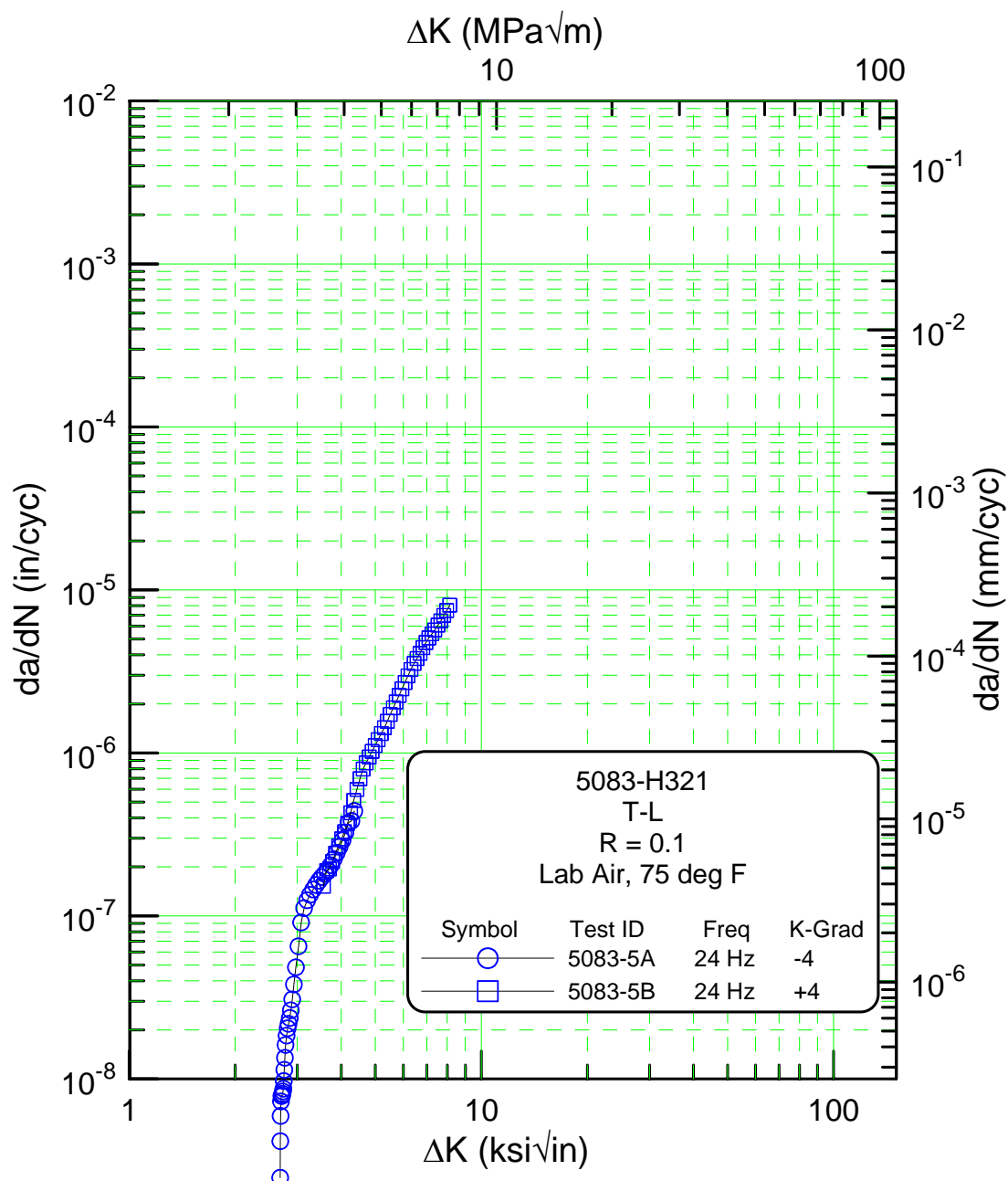
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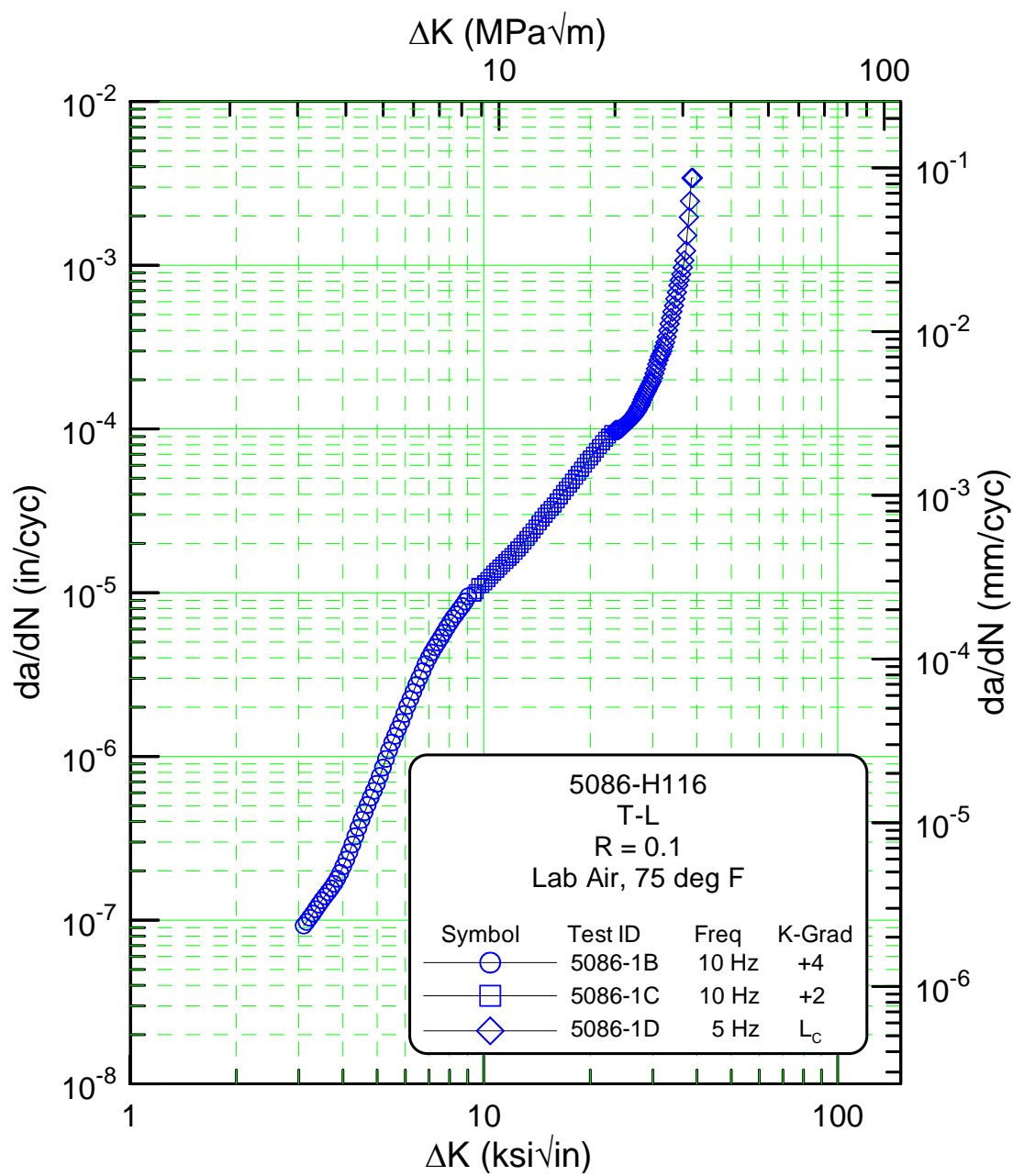
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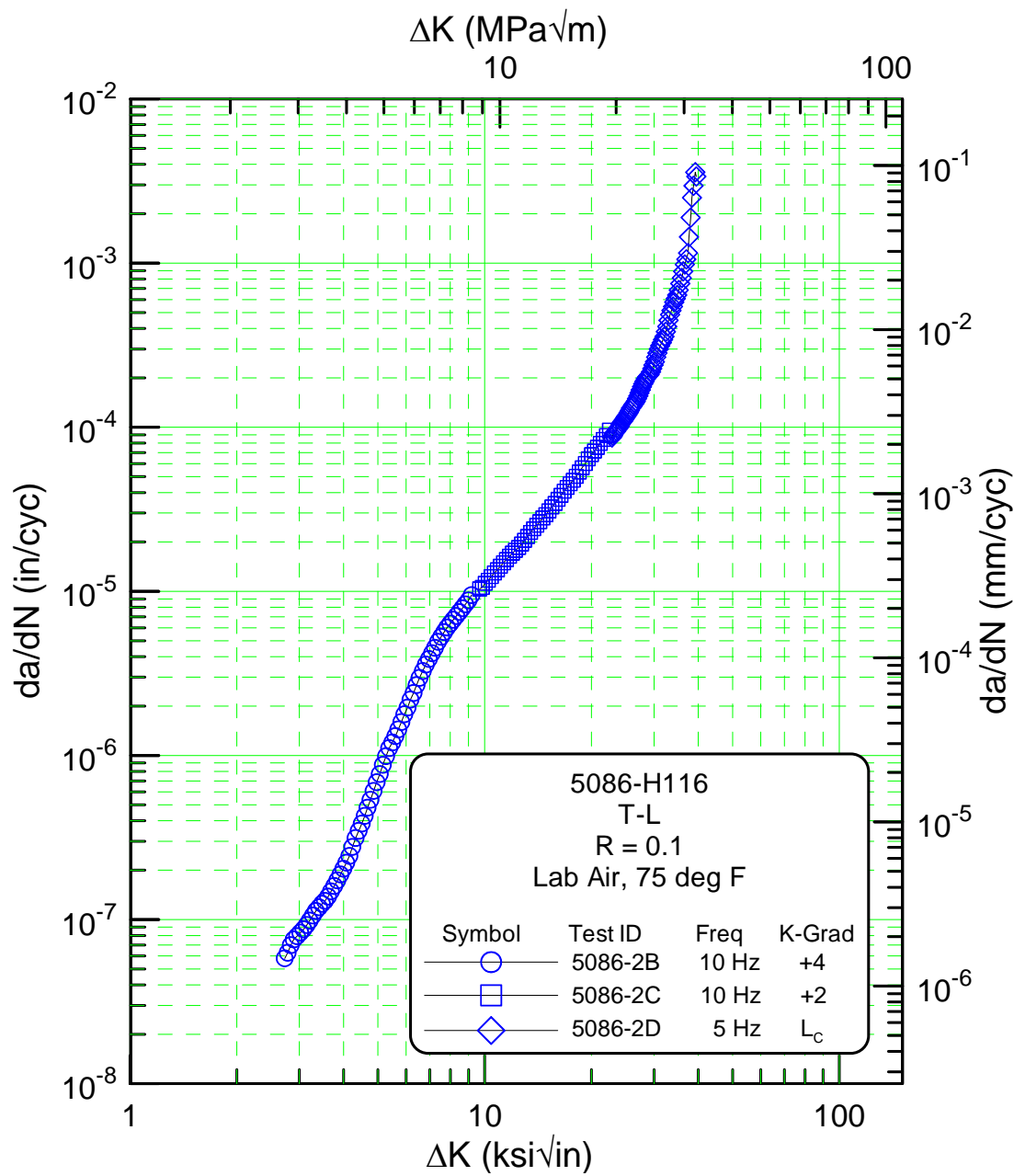
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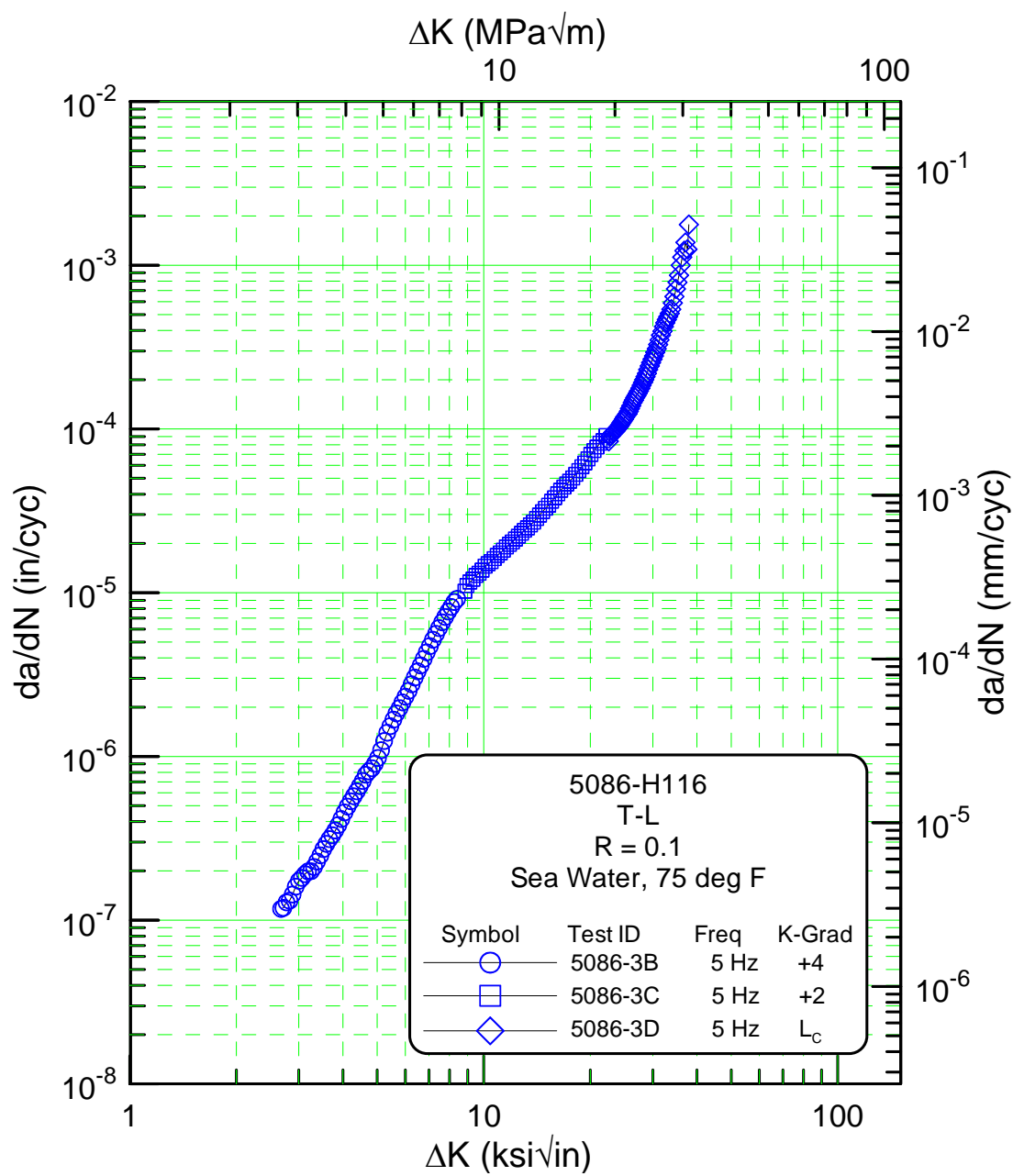
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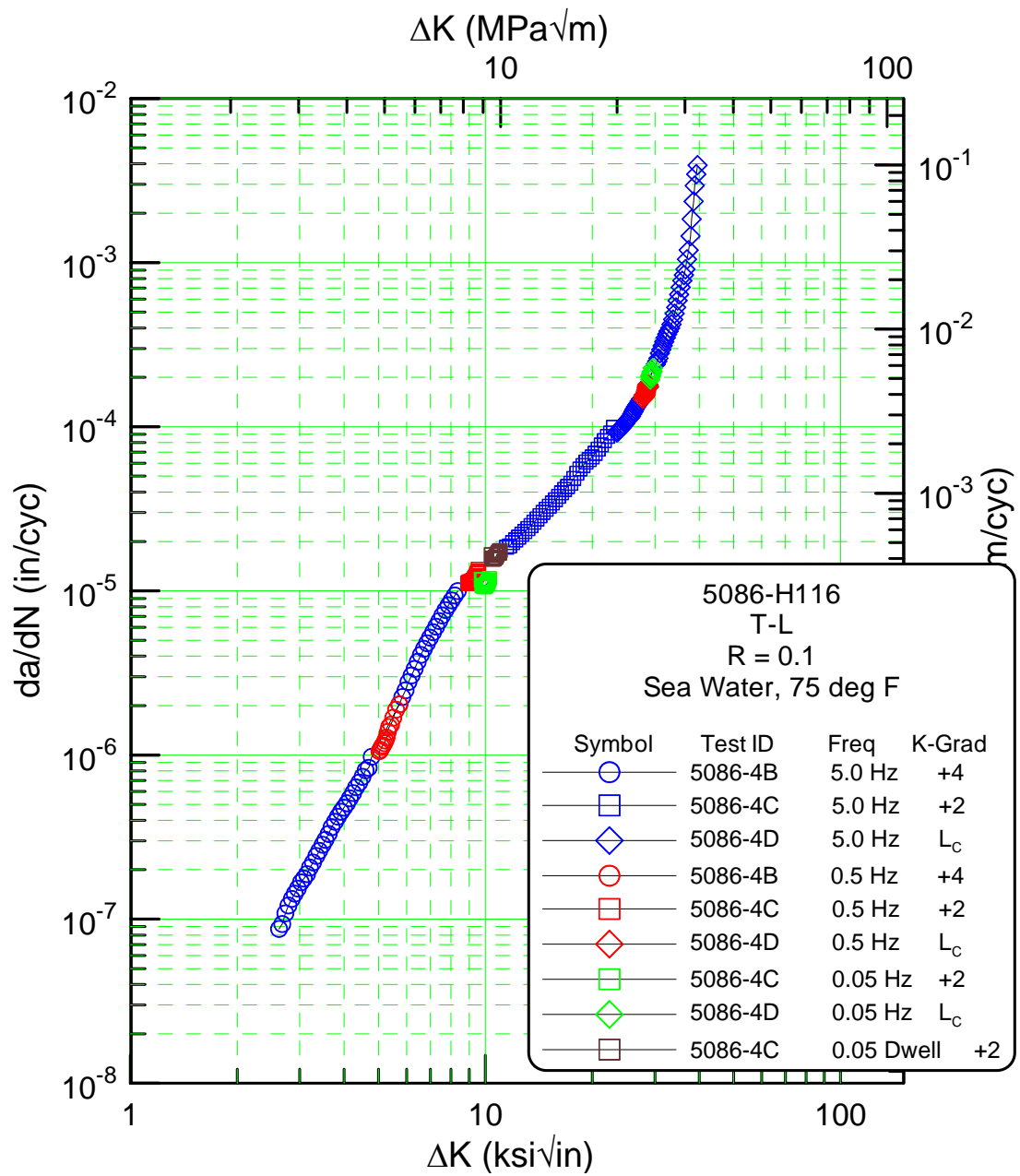
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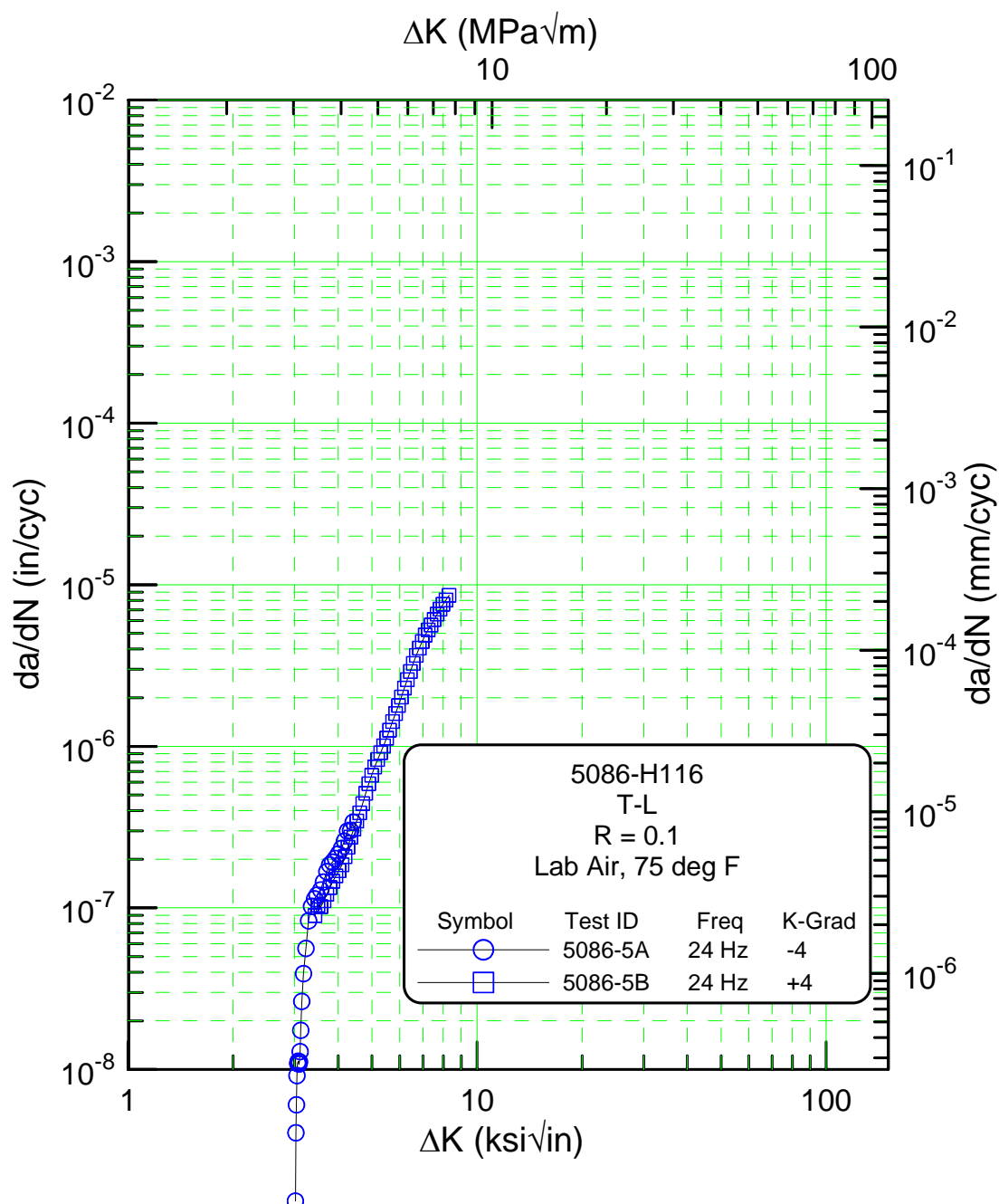
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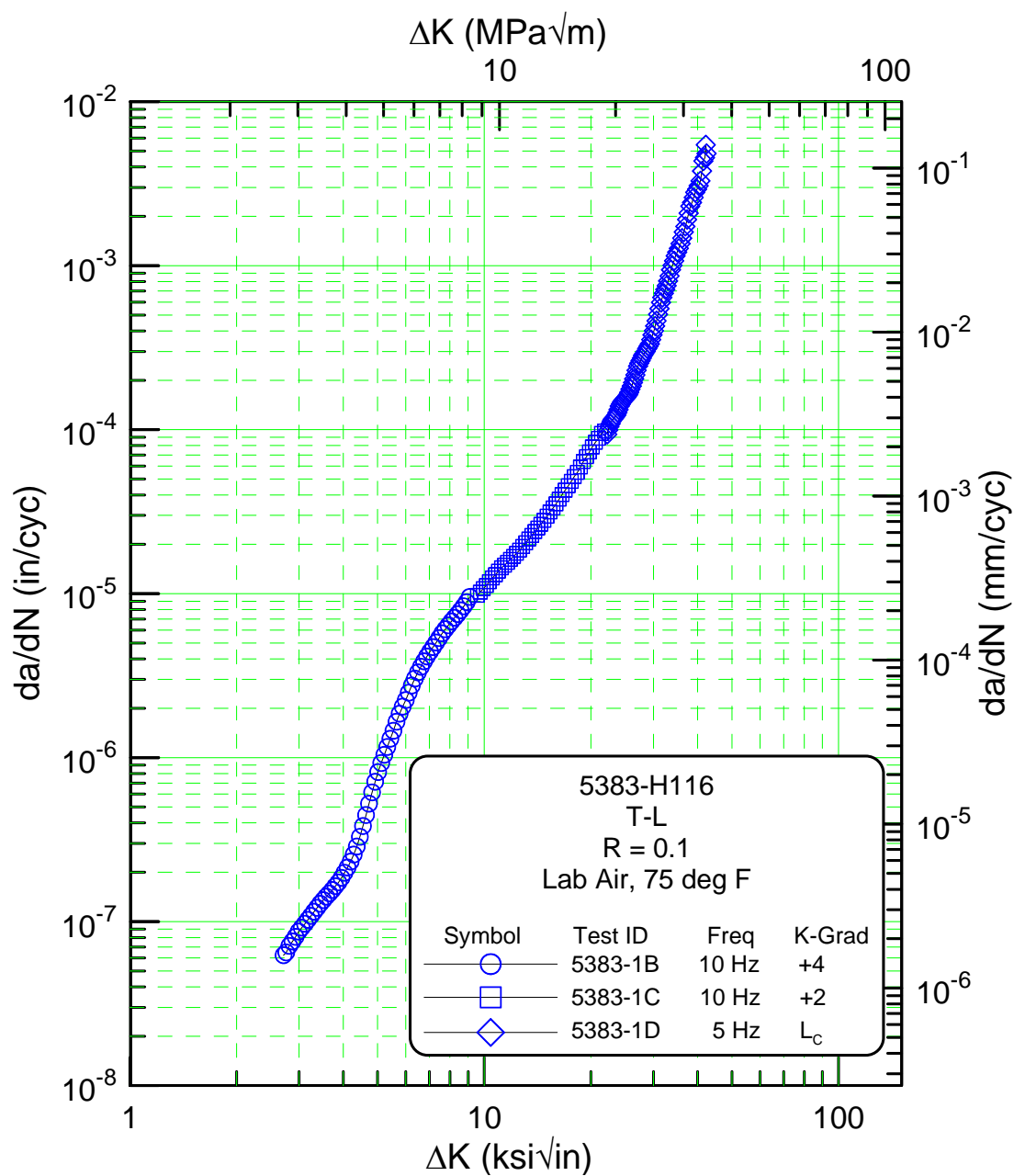
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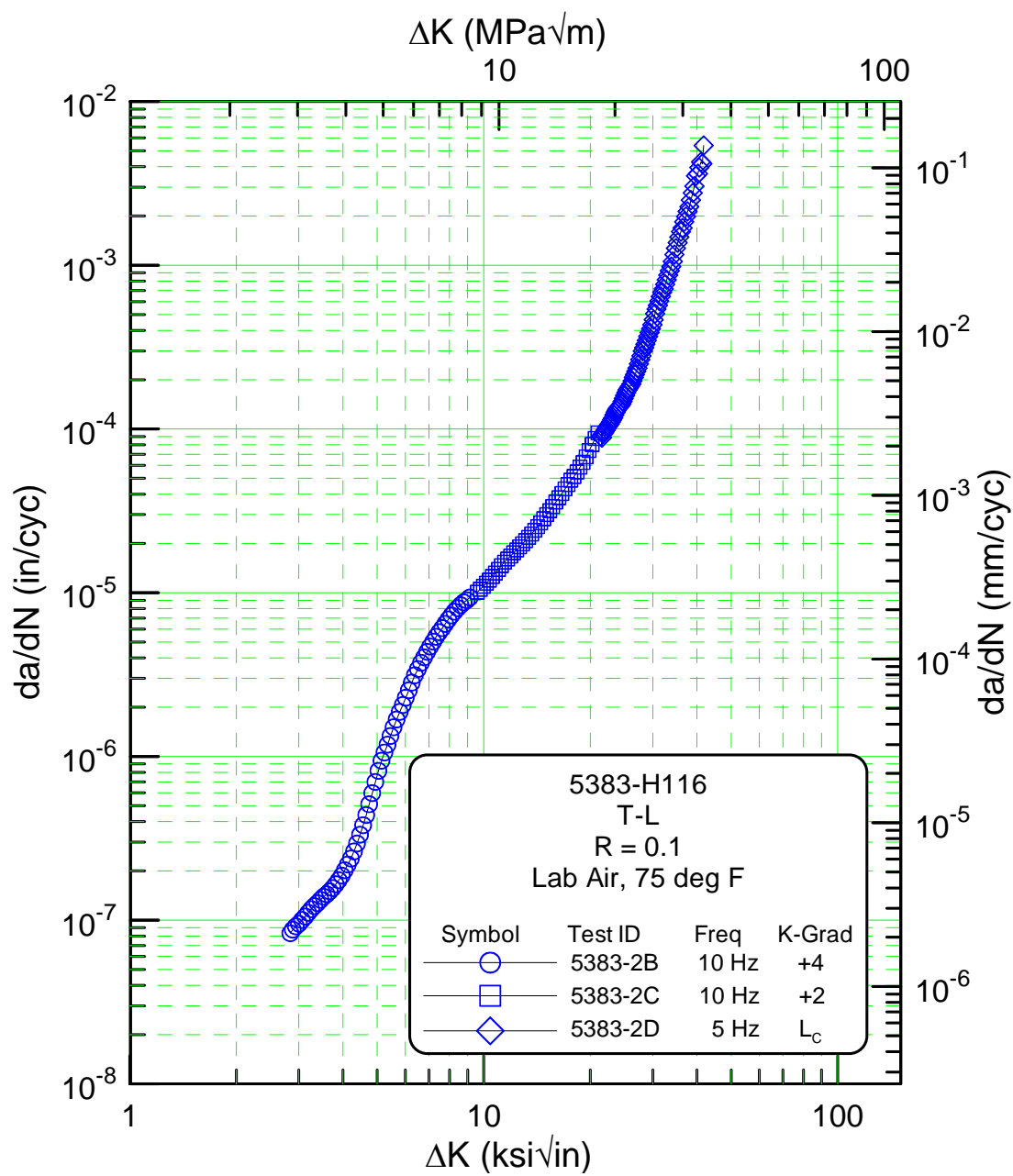
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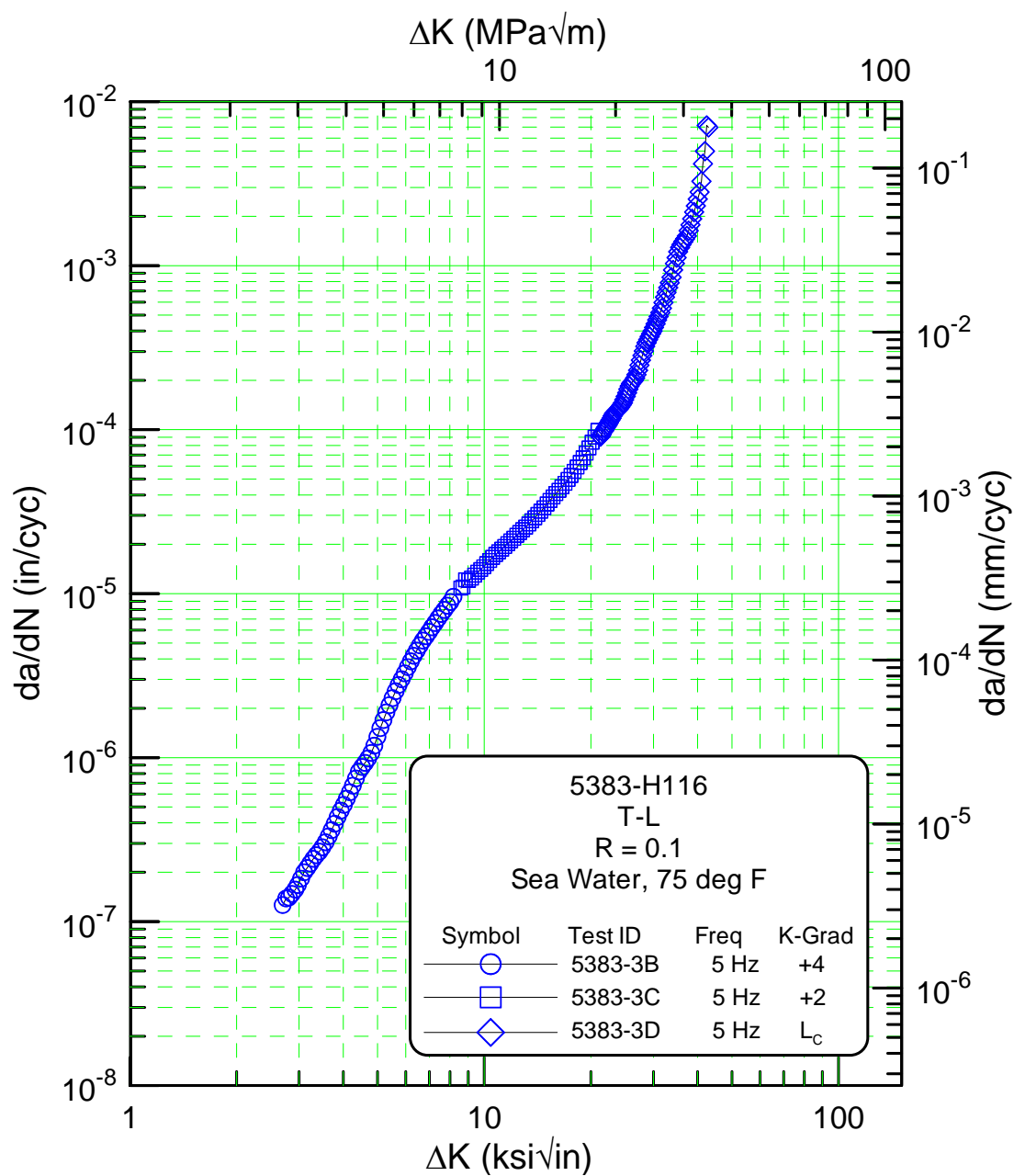
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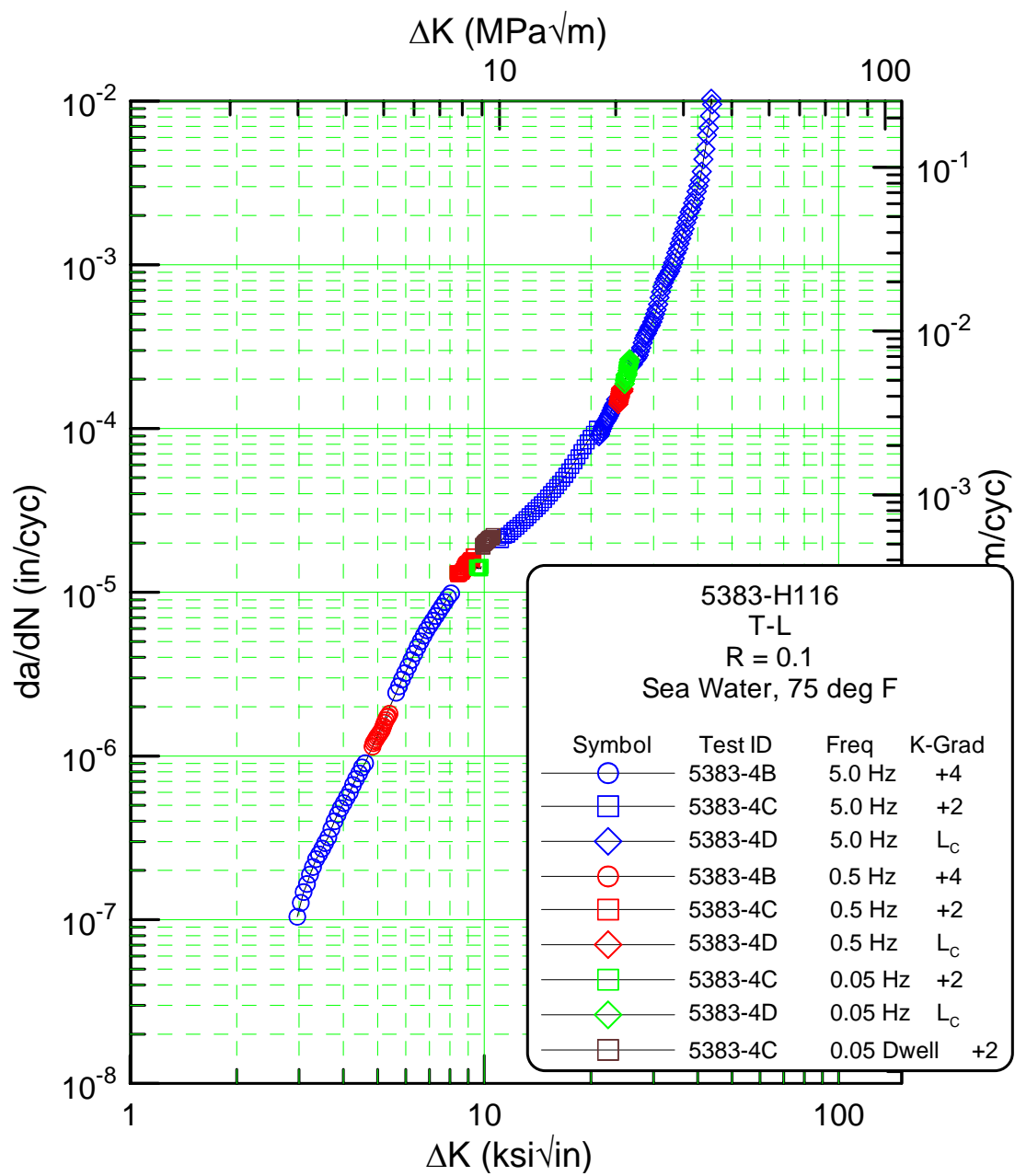
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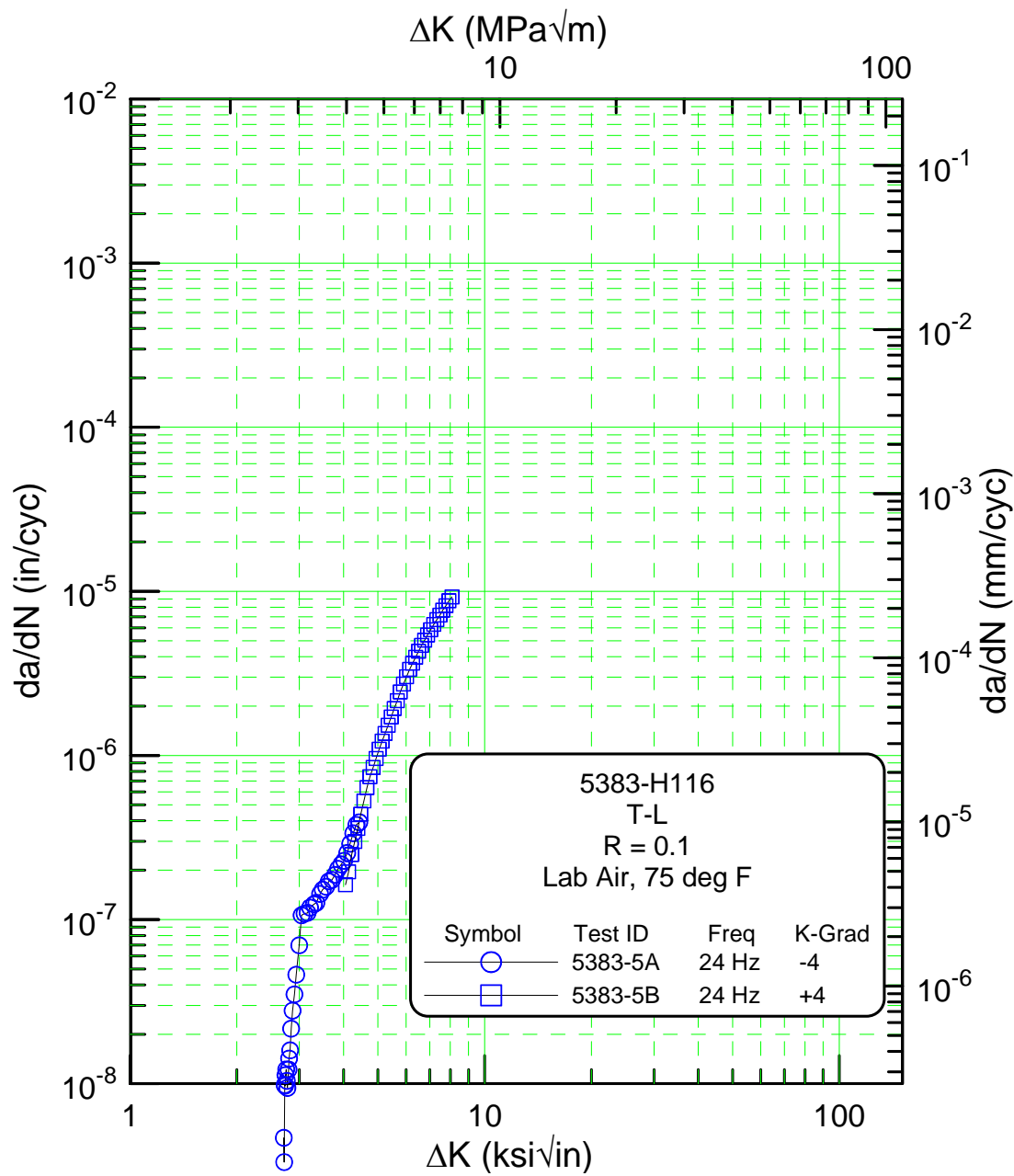
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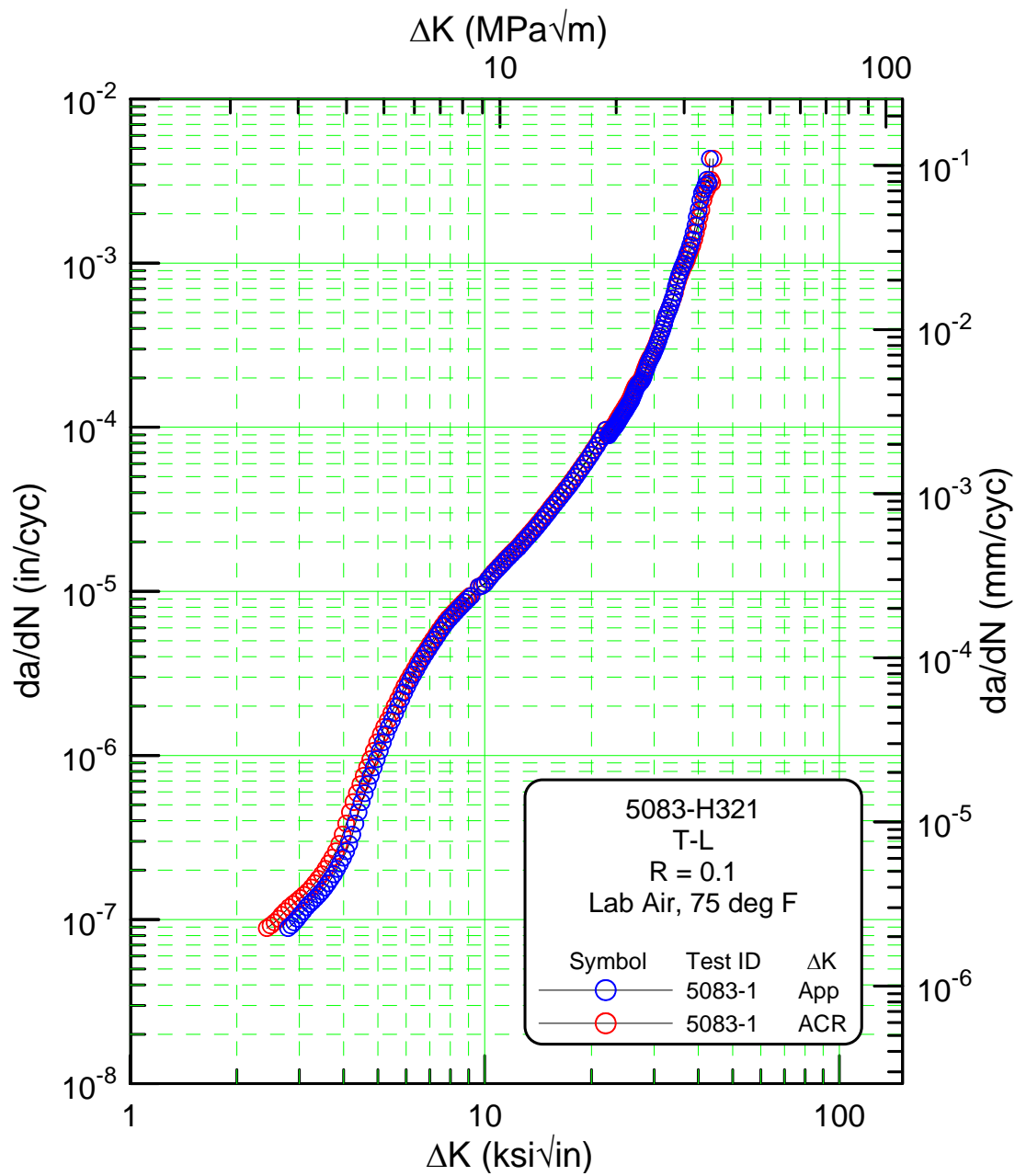
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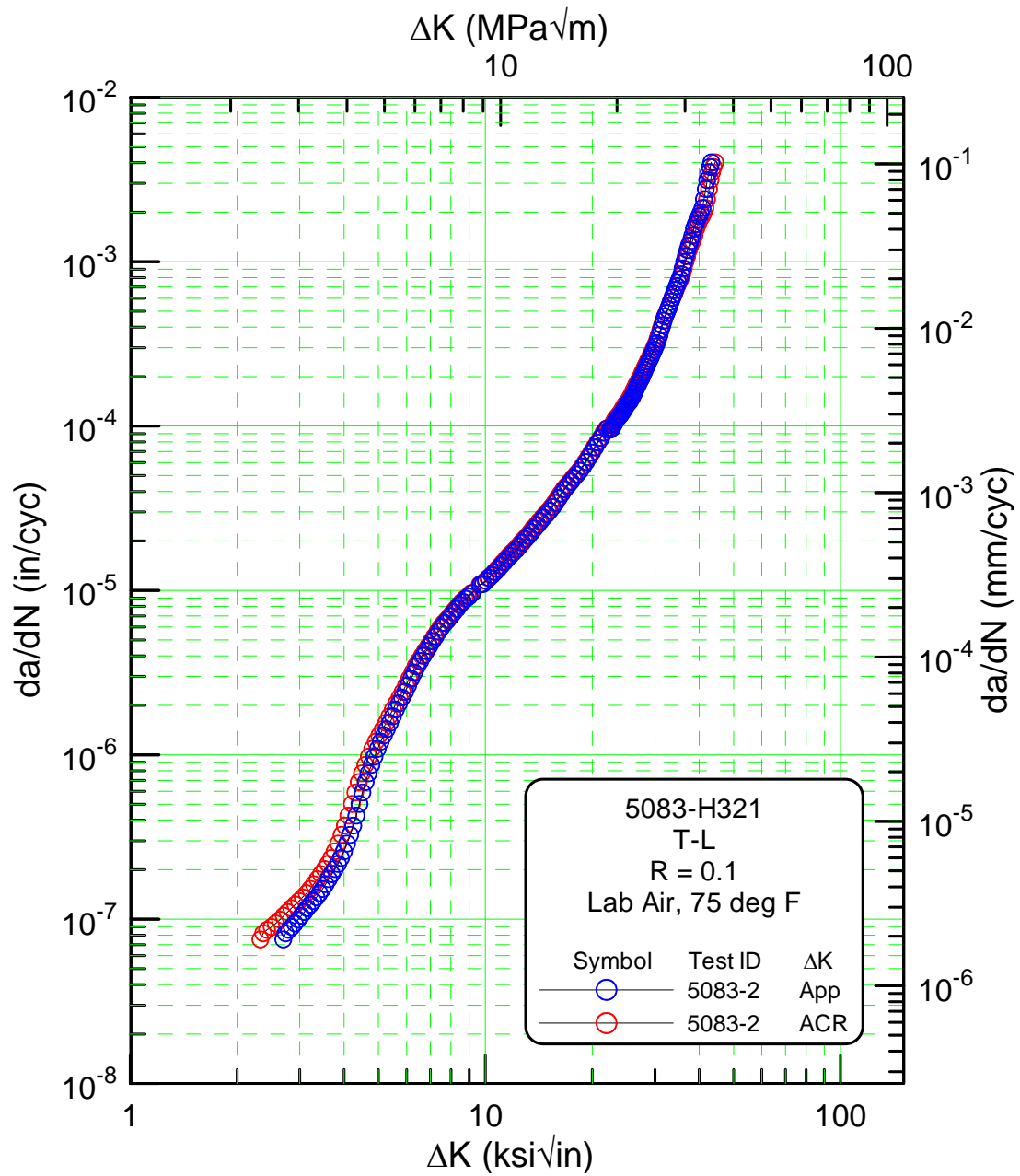
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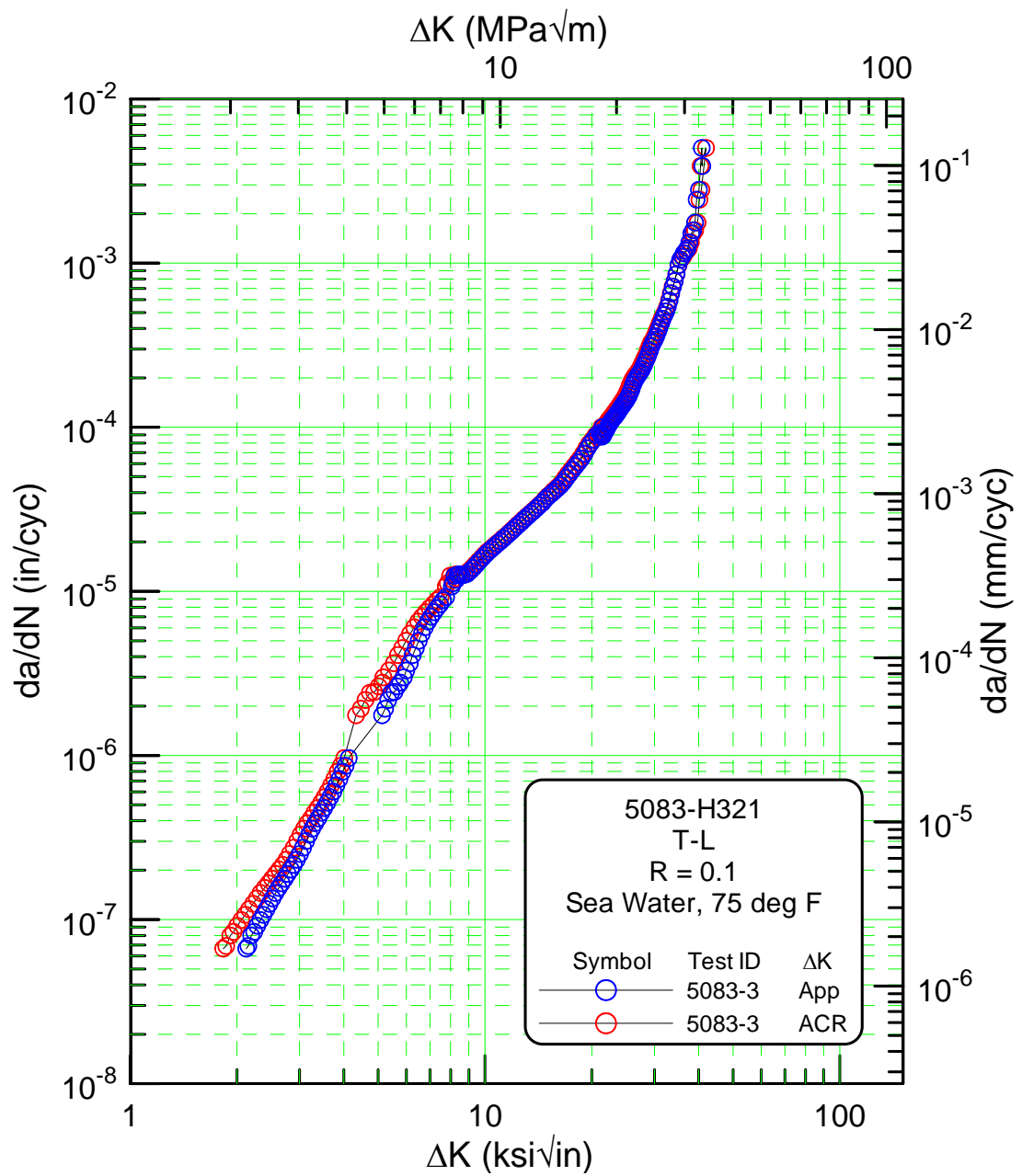
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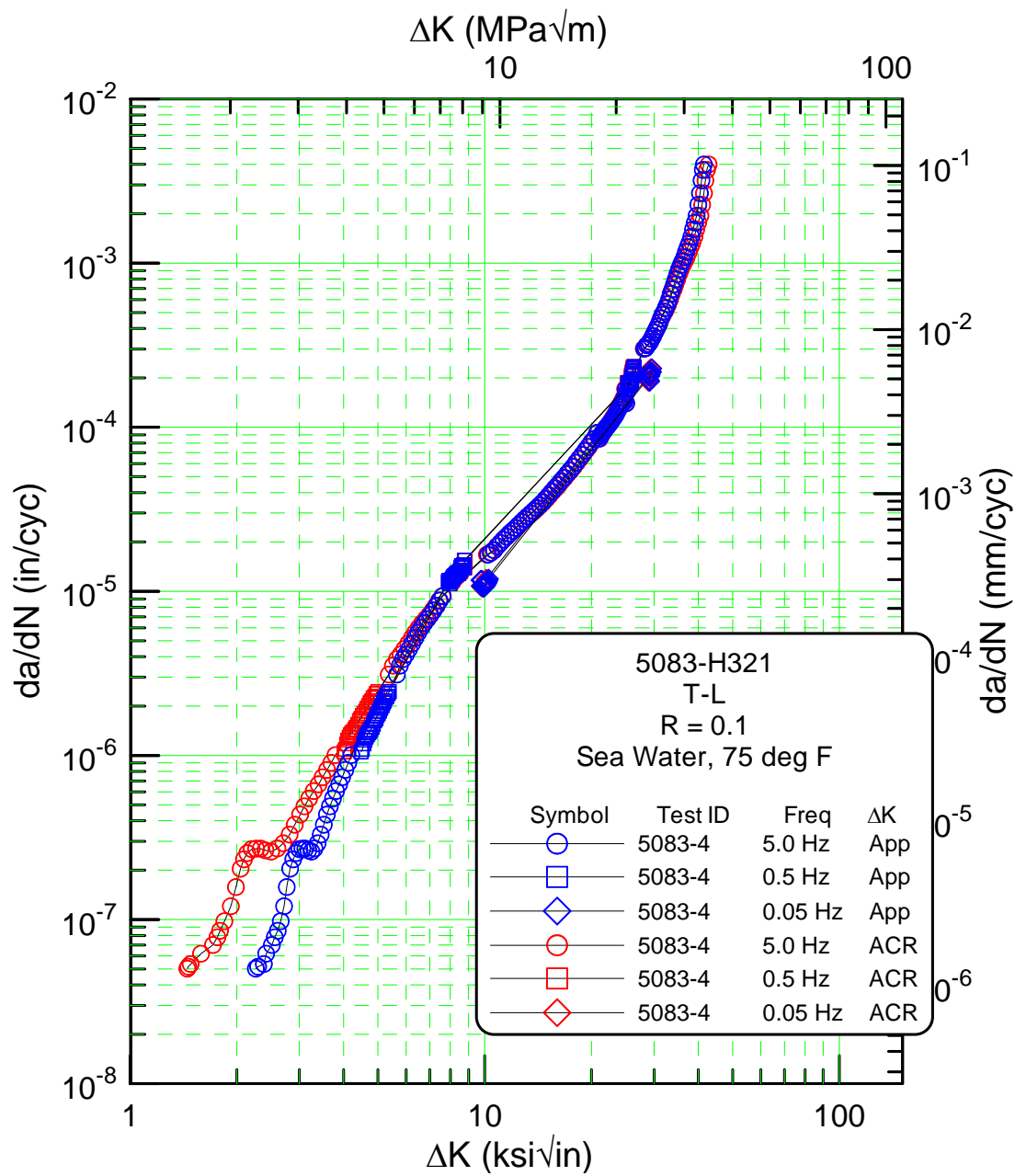
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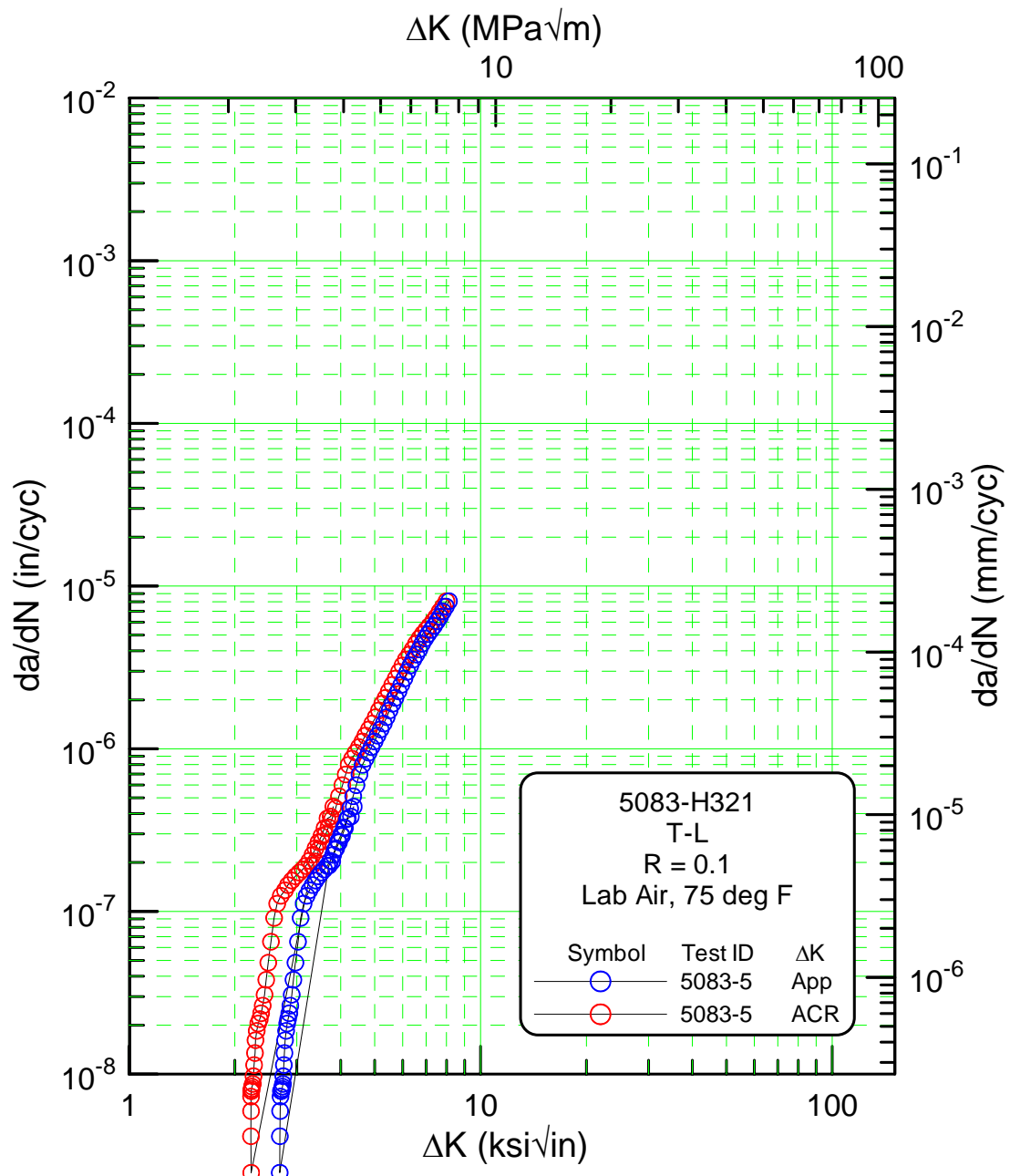
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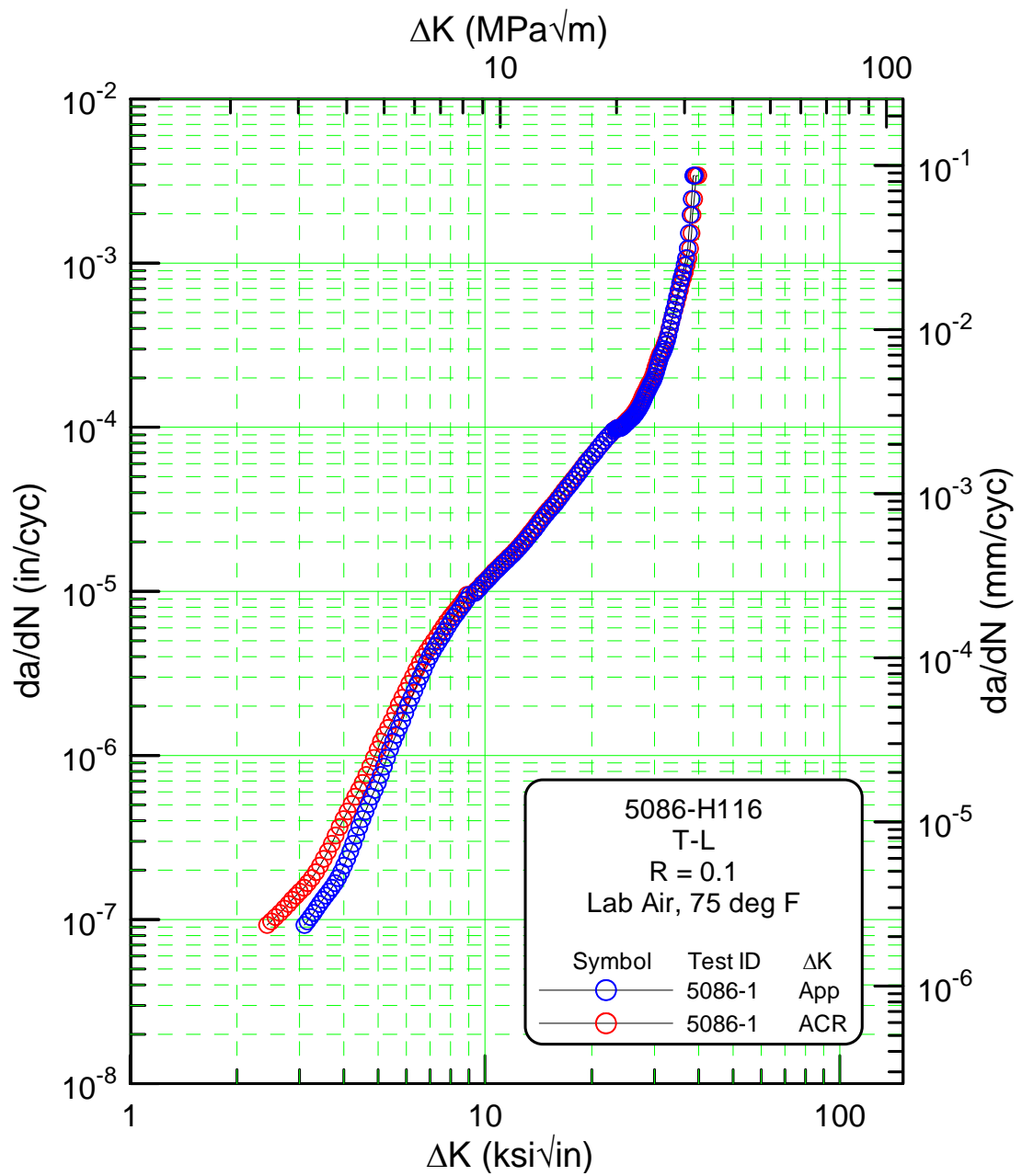
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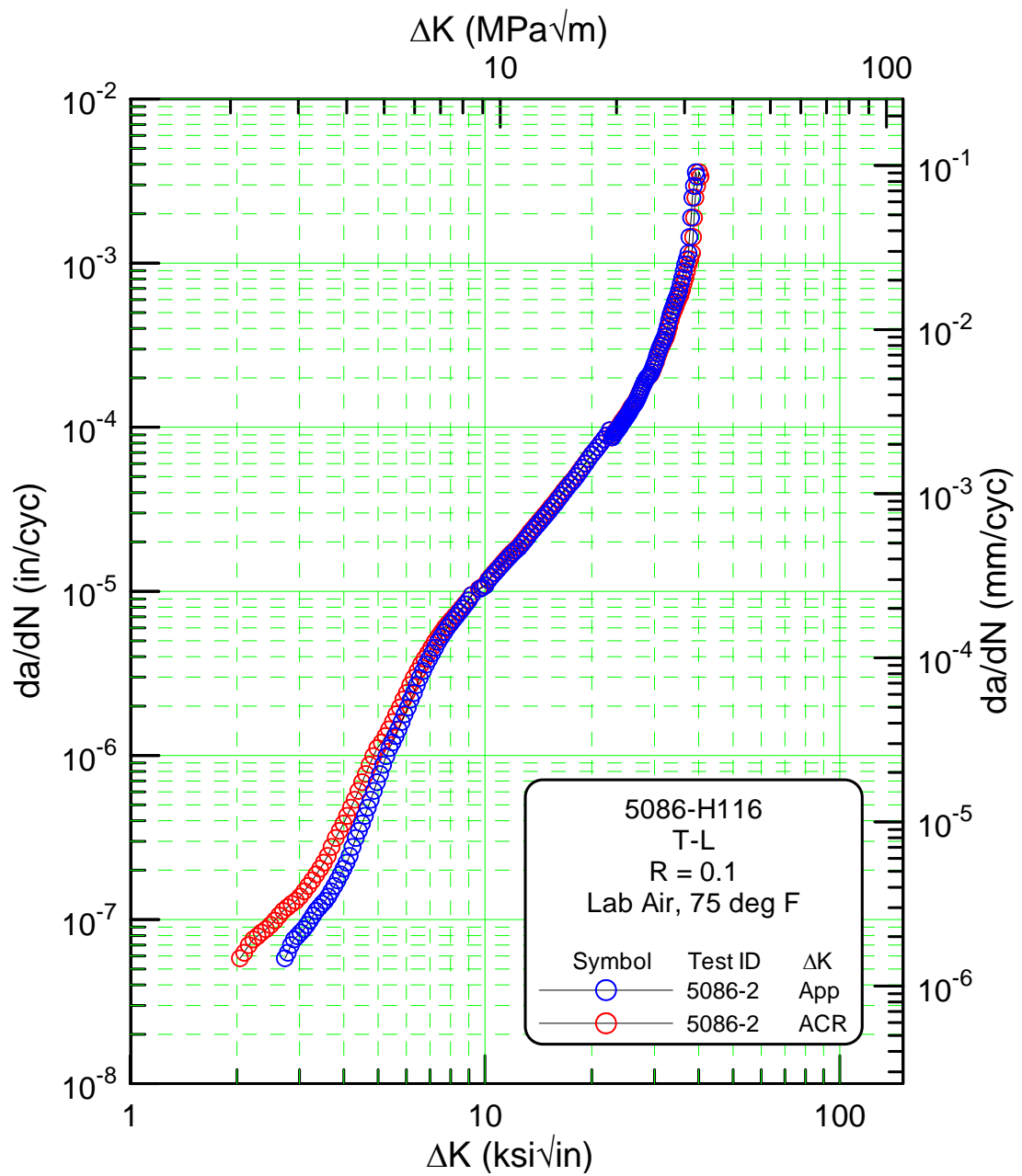
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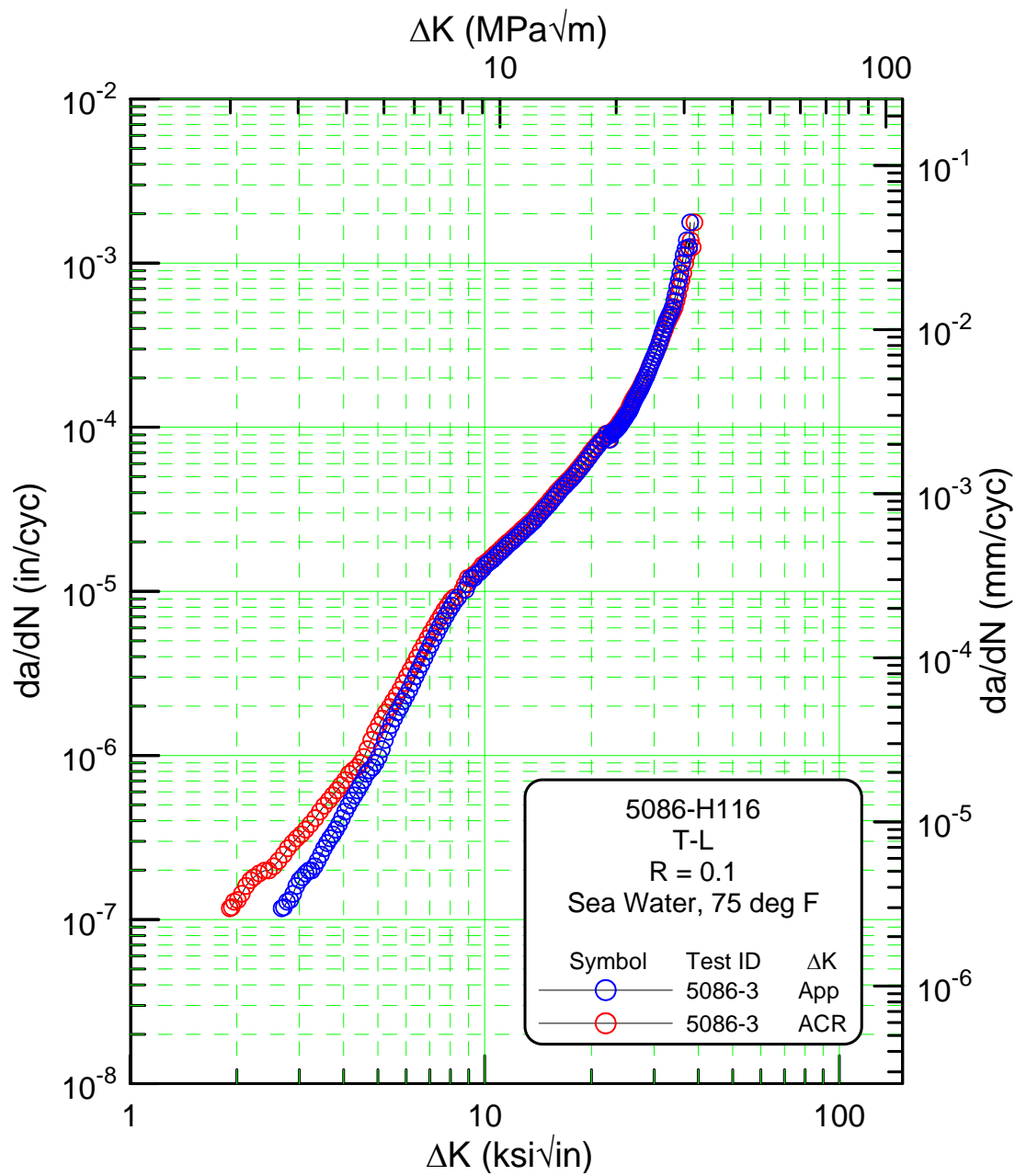
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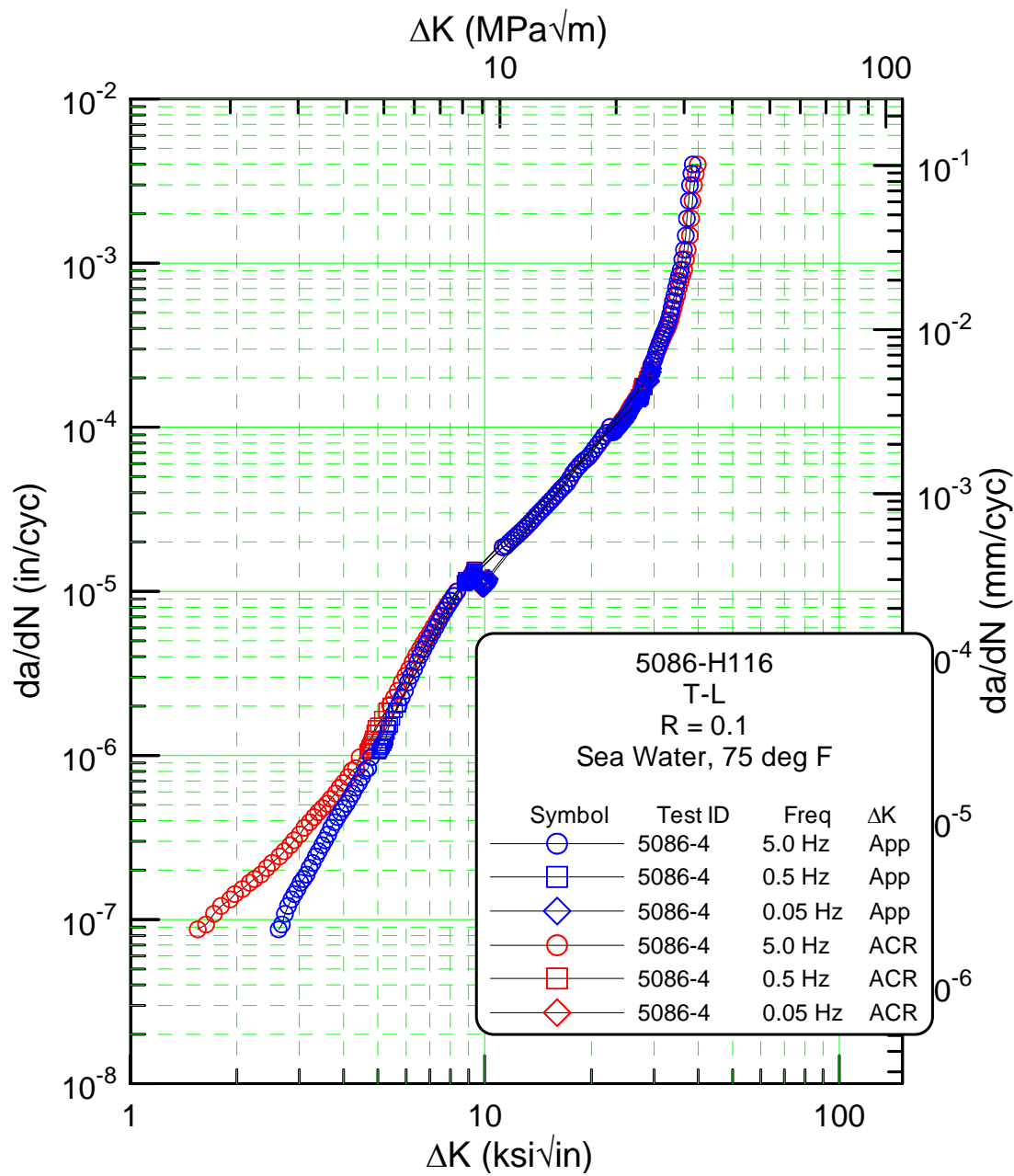
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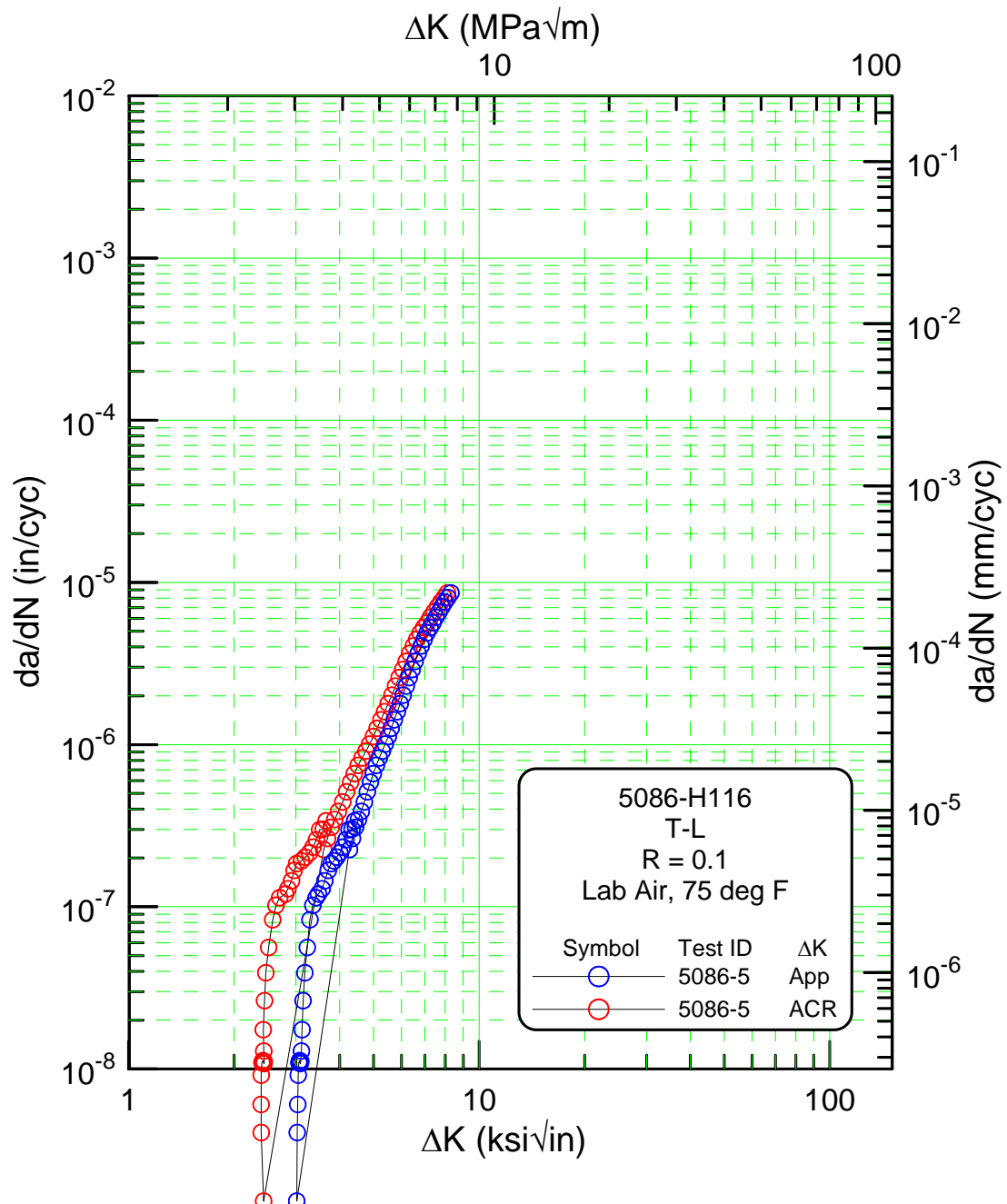
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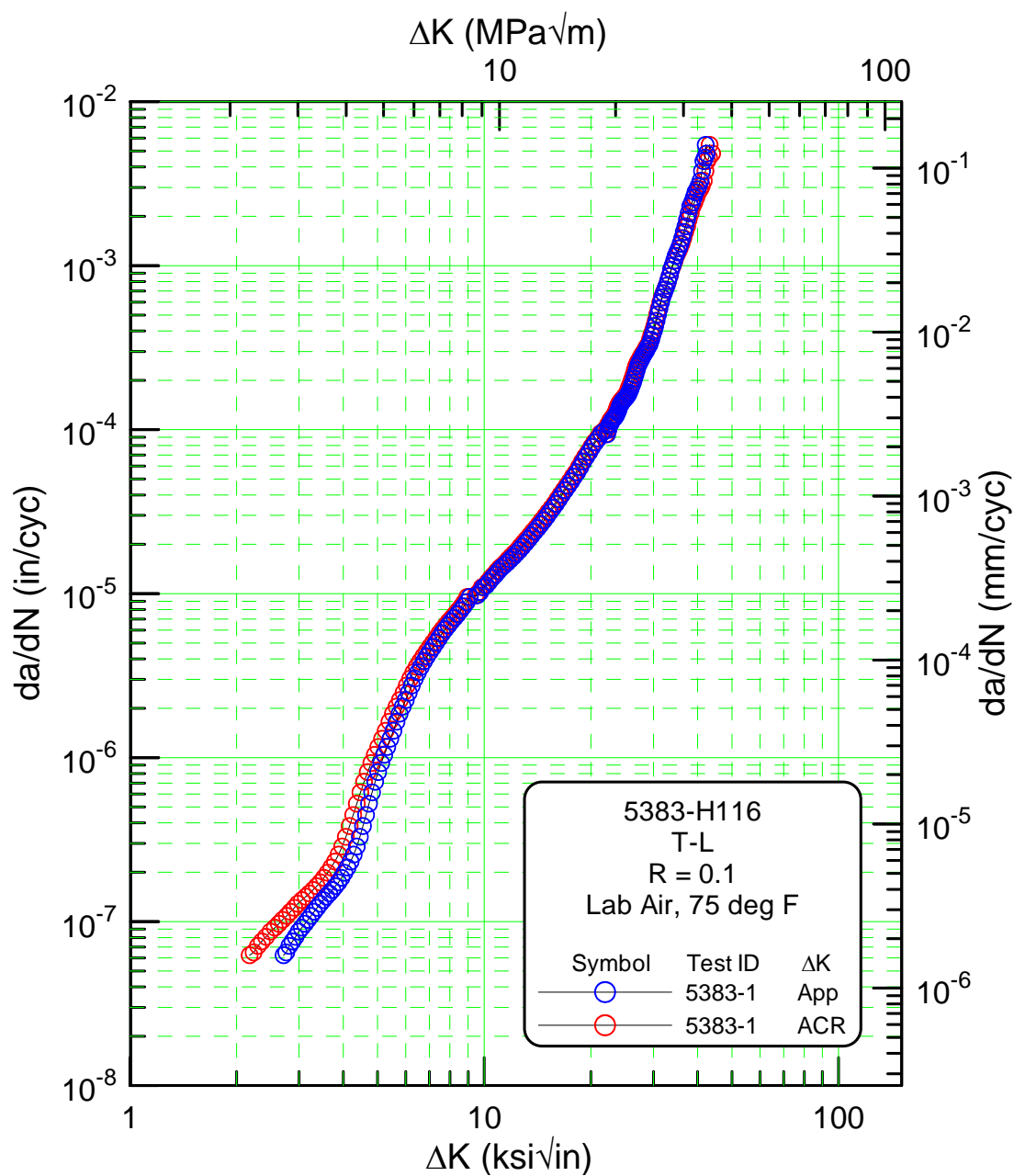
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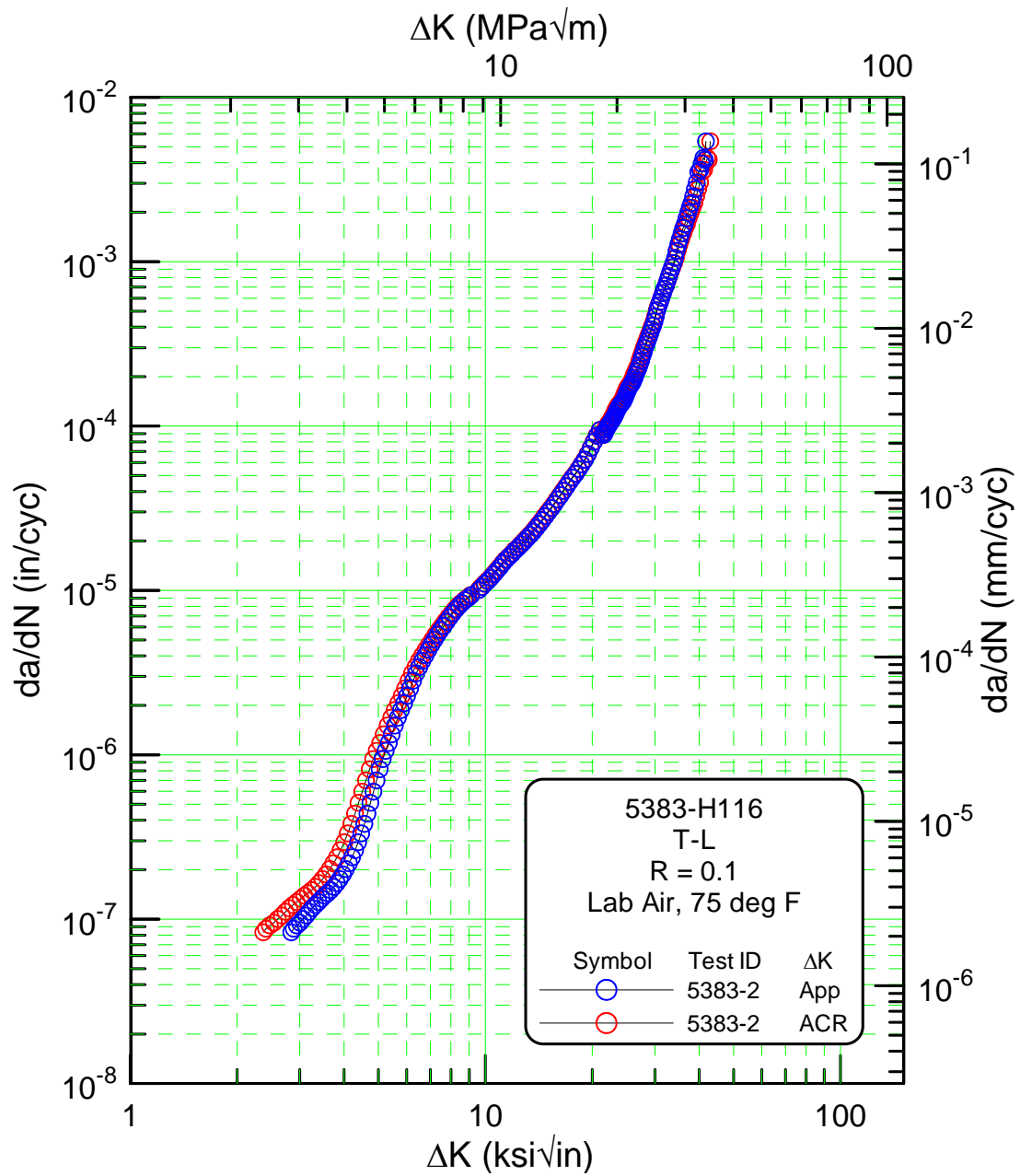
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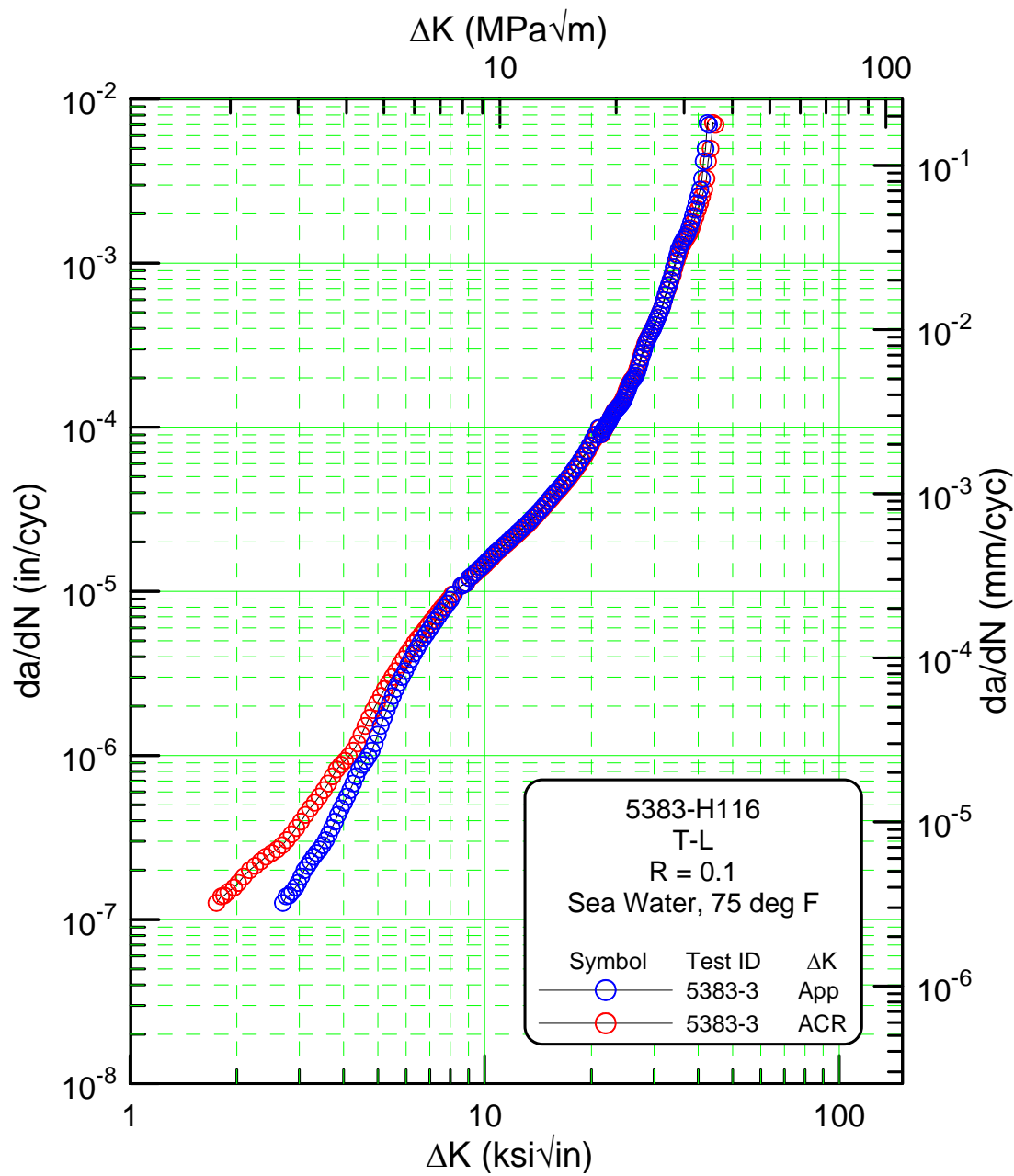
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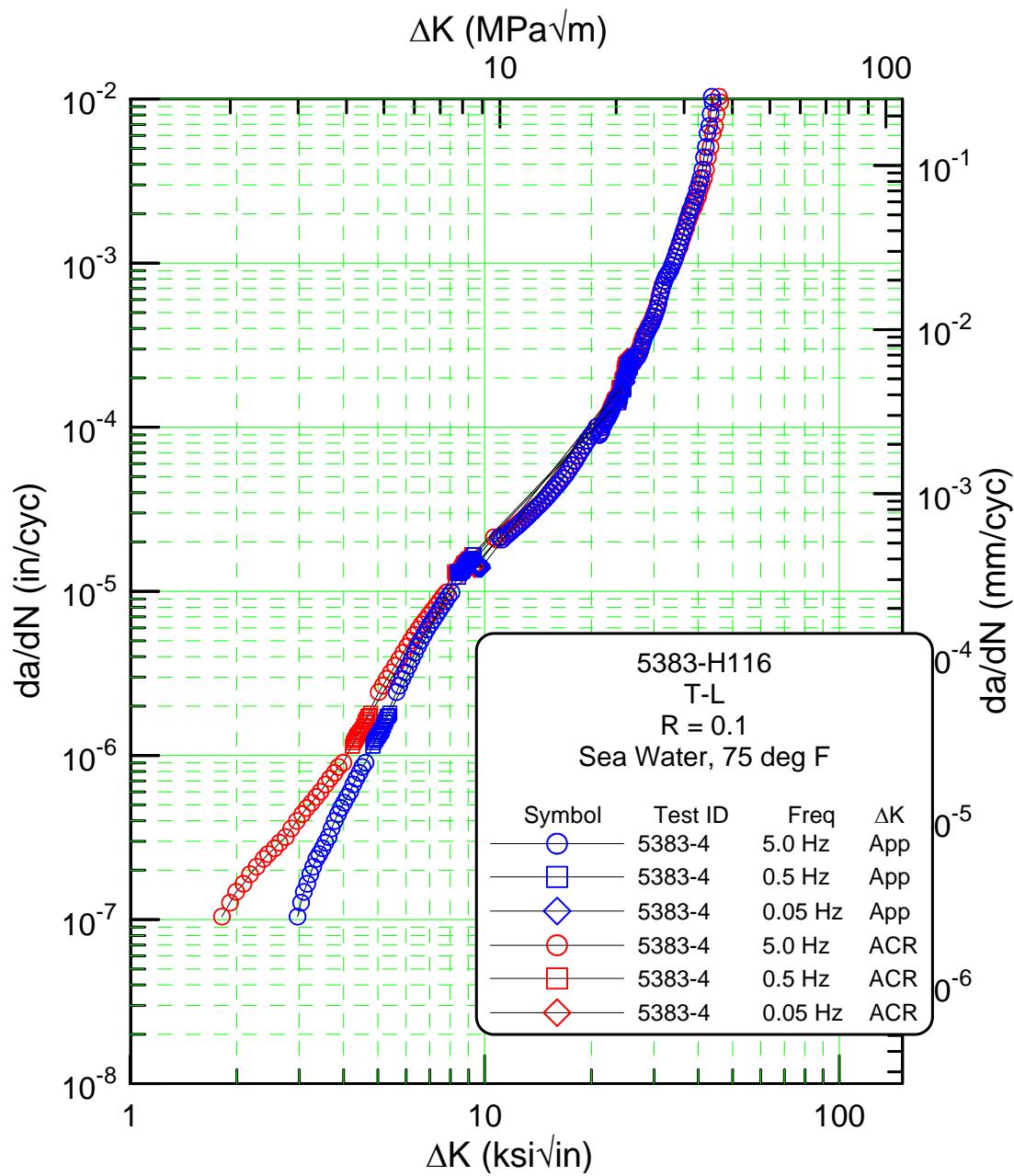
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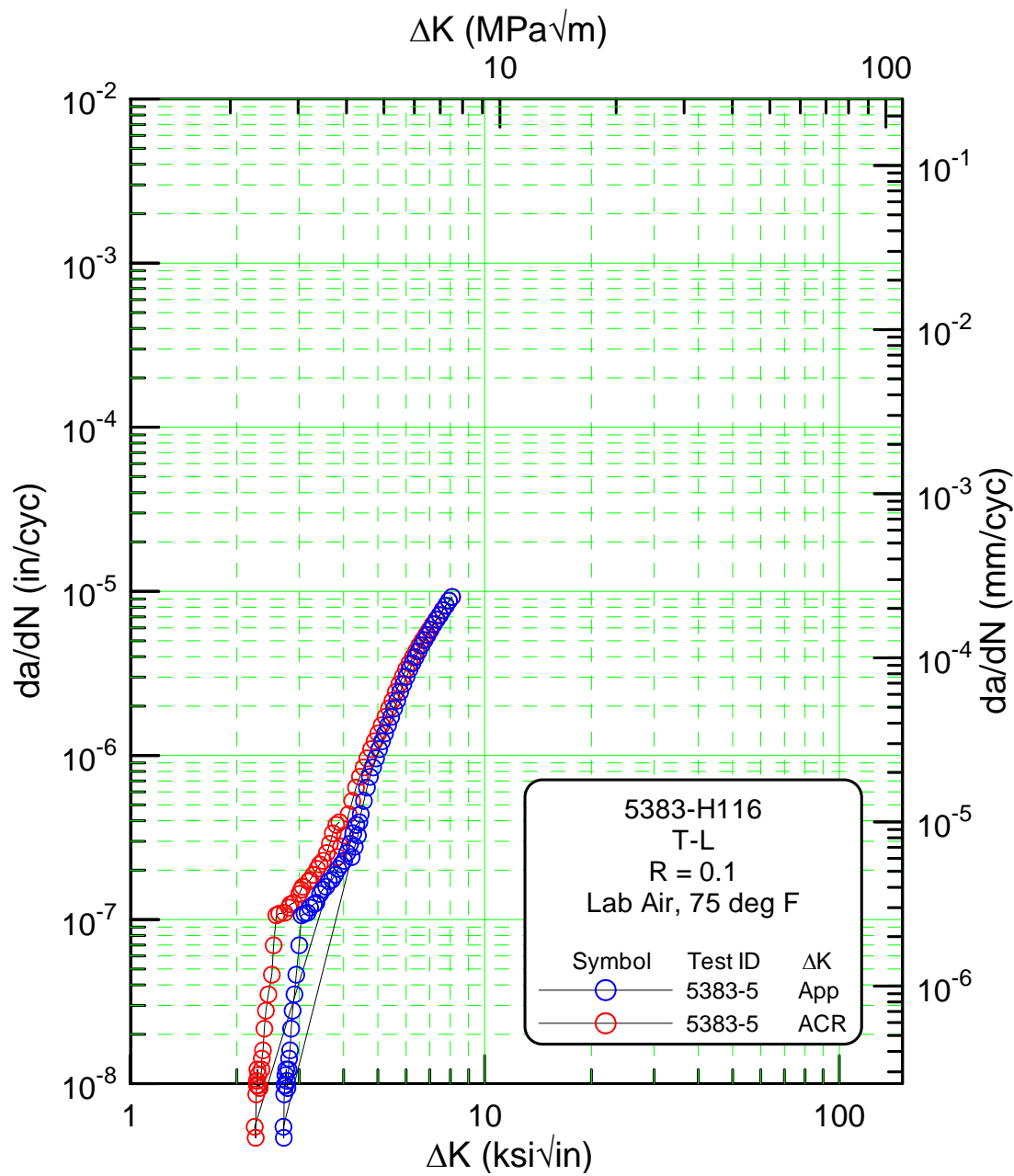
Fatigue Crack Growth Rate vs. Stress Intensity



Fatigue Crack Growth Rate vs. Stress Intensity



Fatigue Crack Growth Rate vs. Stress Intensity



Annex E – Tabular Results – ASTM E647 Analysis

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Automated Fatigue Crack
Growth Rate Analysis

Test ID          5083-FCG-1      Geometry          C(T)
Contract         SSC 10624-01      Orientation        T-L
Material         5083-H321          Yield (ksi)        34.3
Temperature (F)   75              Modulus (Msi)      10.6
Environment      RH = 40%

Specimen Dimensions (in)

Thickness        0.499          Height            2.400
Net Thickness     0.499          Notch Depth       1.000
Width            4.000          Gage Length       0.500

Precrack Parameters

Pmax (lbs)       784.0          Stress Ratio       0.10
Final a (in)     1.050          Kmax (ksi sqr[in]) 4.00

Test Parameters

EvBP    Freq    Pmax    R    Ai    Kmaxi    C    DKi
23.681  10.00    0    0.10  1.140  3.00    4.00  0.00
31.519  10.00    0    0.10  1.456  10.59   2.00  0.00
49.471  5.00     2800  0.10  0.000  0.00    0.00  0.00

C Coeff    C Coeff
.886       1.00098
4.64       -4.66951
-13.32     18.4601
14.72      -236.825
-5.6       1214.88
.           -2143.57

Visual Observations

EvB/P    Crack(EvB/P)  Crack(visual)  Error    CAF
20.683   1.001         1.002         0.001    1.012
21.433   1.040         1.045         0.005    1.010
21.845   1.060         1.055        -0.005    1.009
23.564   1.142         1.150         0.008    1.004
24.665   1.190         1.195         0.005    1.002
26.544   1.267         1.270         0.003    0.998
27.285   1.296         1.295        -0.001    0.996
31.505   1.443         1.430        -0.013    0.988
44.255   1.773         1.765        -0.008    0.972
49.170   1.869         1.865        -0.004    0.967
89.244   2.357         2.365         0.008    0.944

Comments

Date of test: 8/10/2006
Waveform Type          Sine

```

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^1.5) | deltaK |
|--------------|-------|-----------|--------|------------|--------|-------------------|-----------------------|--------|
| | 23.68 | 1.1470 | 52239 | | | | | |
| 568 | 23.79 | 1.1518 | 106926 | 0.0095 | 106637 | 8.875E-8 | 3.099 | 2.789 |
| 577 | 23.89 | 1.1564 | 158876 | 0.0095 | 102998 | 9.213E-8 | 3.162 | 2.846 |
| 587 | 24.00 | 1.1612 | 209924 | 0.0047 | 48855 | 9.610E-8 | 3.225 | 2.902 |
| 597 | 24.11 | 1.1659 | 258943 | 0.0047 | 46770 | 1.012E-7 | 3.289 | 2.960 |
| 607 | 24.21 | 1.1706 | 304075 | 0.0048 | 45029 | 1.068E-7 | 3.354 | 3.019 |
| 617 | 24.32 | 1.1753 | 345371 | 0.0048 | 42580 | 1.125E-7 | 3.422 | 3.080 |
| 628 | 24.43 | 1.1802 | 387545 | 0.0048 | 40217 | 1.188E-7 | 3.492 | 3.142 |
| 639 | 24.55 | 1.1852 | 429050 | 0.0048 | 38501 | 1.243E-7 | 3.562 | 3.206 |
| 650 | 24.66 | 1.1899 | 465404 | 0.0048 | 37173 | 1.293E-7 | 3.635 | 3.271 |
| 660 | 24.77 | 1.1946 | 500243 | 0.0048 | 35193 | 1.352E-7 | 3.707 | 3.336 |
| 672 | 24.88 | 1.1993 | 535082 | 0.0047 | 33173 | 1.415E-7 | 3.781 | 3.403 |
| 683 | 24.99 | 1.2041 | 568406 | 0.0047 | 31760 | 1.483E-7 | 3.857 | 3.471 |
| 694 | 25.10 | 1.2088 | 598700 | 0.0047 | 30195 | 1.566E-7 | 3.934 | 3.541 |
| 706 | 25.21 | 1.2135 | 628088 | 0.0047 | 28428 | 1.664E-7 | 4.012 | 3.611 |
| 718 | 25.33 | 1.2182 | 655961 | 0.0047 | 26631 | 1.770E-7 | 4.093 | 3.683 |
| 730 | 25.44 | 1.2229 | 681411 | 0.0047 | 25137 | 1.888E-7 | 4.174 | 3.757 |
| 743 | 25.56 | 1.2277 | 705649 | 0.0047 | 23309 | 2.036E-7 | 4.258 | 3.832 |
| 755 | 25.67 | 1.2323 | 728190 | 0.0047 | 21539 | 2.199E-7 | 4.343 | 3.909 |
| 768 | 25.79 | 1.2371 | 749519 | 0.0047 | 20011 | 2.384E-7 | 4.429 | 3.986 |
| 781 | 25.90 | 1.2418 | 767940 | 0.0047 | 18427 | 2.606E-7 | 4.518 | 4.066 |
| 794 | 26.02 | 1.2464 | 785195 | 0.0048 | 16764 | 2.893E-7 | 4.606 | 4.146 |
| 807 | 26.13 | 1.2511 | 801479 | 0.0048 | 14884 | 3.298E-7 | 4.700 | 4.230 |
| 821 | 26.26 | 1.2560 | 816211 | 0.0048 | 13221 | 3.848E-7 | 4.795 | 4.316 |
| 835 | 26.38 | 1.2609 | 828774 | 0.0048 | 11604 | 4.511E-7 | 4.895 | 4.405 |
| 850 | 26.51 | 1.2658 | 838825 | 0.0048 | 10015 | 5.199E-7 | 4.994 | 4.494 |
| 864 | 26.62 | 1.2704 | 847267 | 0.0047 | 8565 | 5.885E-7 | 5.094 | 4.584 |
| 878 | 26.74 | 1.2750 | 854817 | 0.0047 | 7329 | 6.671E-7 | 5.195 | 4.676 |
| 894 | 26.86 | 1.2797 | 861569 | 0.0046 | 6441 | 7.515E-7 | 5.296 | 4.766 |
| 908 | 26.98 | 1.2843 | 867603 | 0.0047 | 5780 | 8.458E-7 | 5.402 | 4.862 |
| 923 | 27.10 | 1.2890 | 872748 | 0.0047 | 5166 | 9.484E-7 | 5.508 | 4.957 |
| 939 | 27.23 | 1.2937 | 877473 | 0.0047 | 4589 | 1.065E-6 | 5.619 | 5.057 |
| 955 | 27.36 | 1.2986 | 881948 | 0.0047 | 4066 | 1.203E-6 | 5.733 | 5.160 |
| 972 | 27.48 | 1.3034 | 885810 | 0.0048 | 3685 | 1.346E-6 | 5.848 | 5.263 |
| 988 | 27.61 | 1.3081 | 889103 | 0.0048 | 3331 | 1.491E-6 | 5.965 | 5.369 |
| 1004 | 27.73 | 1.3127 | 891997 | 0.0047 | 2954 | 1.638E-6 | 6.085 | 5.477 |
| 1022 | 27.86 | 1.3175 | 894859 | 0.0047 | 2658 | 1.806E-6 | 6.207 | 5.586 |
| 1039 | 27.99 | 1.3224 | 897460 | 0.0047 | 2421 | 2.000E-6 | 6.331 | 5.698 |
| 1056 | 28.12 | 1.3269 | 899673 | 0.0047 | 2217 | 2.200E-6 | 6.458 | 5.812 |
| 1074 | 28.25 | 1.3317 | 901756 | 0.0047 | 2004 | 2.418E-6 | 6.587 | 5.928 |
| 1093 | 28.38 | 1.3365 | 903631 | 0.0047 | 1818 | 2.641E-6 | 6.717 | 6.046 |
| 1111 | 28.51 | 1.3411 | 905298 | 0.0048 | 1684 | 2.871E-6 | 6.852 | 6.167 |
| 1129 | 28.64 | 1.3458 | 906881 | 0.0048 | 1549 | 3.107E-6 | 6.989 | 6.290 |
| 1149 | 28.77 | 1.3506 | 908369 | 0.0047 | 1426 | 3.347E-6 | 7.131 | 6.418 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^0.5) | deltaK |
|--------------|-------|-----------|--------|------------|------|-------------------|-----------------------|--------|
| 1169 | 28.91 | 1.3556 | 909778 | 0.0047 | 1326 | 3.622E-6 | 7.275 | 6.548 |
| 1189 | 29.04 | 1.3603 | 911052 | 0.0047 | 1232 | 3.896E-6 | 7.422 | 6.680 |
| 1208 | 29.17 | 1.3649 | 912189 | 0.0047 | 1142 | 4.174E-6 | 7.570 | 6.813 |
| 1229 | 29.31 | 1.3696 | 913256 | 0.0047 | 1064 | 4.457E-6 | 7.717 | 6.945 |
| 1249 | 29.44 | 1.3742 | 914270 | 0.0047 | 993 | 4.759E-6 | 7.871 | 7.084 |
| 1270 | 29.58 | 1.3789 | 915219 | 0.0047 | 937 | 5.068E-6 | 8.028 | 7.226 |
| 1292 | 29.72 | 1.3838 | 916159 | 0.0048 | 886 | 5.423E-6 | 8.190 | 7.371 |
| 1314 | 29.86 | 1.3886 | 917012 | 0.0048 | 832 | 5.797E-6 | 8.357 | 7.521 |
| 1337 | 30.00 | 1.3933 | 917811 | 0.0048 | 783 | 6.166E-6 | 8.527 | 7.675 |
| 1360 | 30.14 | 1.3983 | 918571 | 0.0048 | 733 | 6.536E-6 | 8.699 | 7.829 |
| 1383 | 30.28 | 1.4030 | 919262 | 0.0047 | 692 | 6.869E-6 | 8.874 | 7.987 |
| 1406 | 30.42 | 1.4076 | 919919 | 0.0047 | 655 | 7.203E-6 | 9.052 | 8.147 |
| 1430 | 30.56 | 1.4124 | 920559 | 0.0047 | 624 | 7.541E-6 | 9.228 | 8.305 |
| 1453 | 30.70 | 1.4170 | 921163 | 0.0047 | 600 | 7.885E-6 | 9.413 | 8.472 |
| 1478 | 30.85 | 1.4217 | 921739 | 0.0048 | 578 | 8.232E-6 | 9.601 | 8.641 |
| 1503 | 31.00 | 1.4266 | 922315 | 0.0048 | 552 | 8.603E-6 | 9.794 | 8.815 |
| 1529 | 31.15 | 1.4314 | 922864 | 0.0096 | 1070 | 8.991E-6 | 9.992 | 8.993 |
| 1555 | 31.29 | 1.4362 | 923385 | 0.0095 | 1009 | 9.378E-6 | 10.195 | 9.175 |
| | 31.44 | 1.4409 | 923873 | | | | | |
| | 31.52 | 1.4435 | 924558 | | | | | |
| 1615 | 31.81 | 1.4528 | 925419 | 0.0190 | 1776 | 1.067E-5 | 10.702 | 9.632 |
| 1637 | 32.12 | 1.4624 | 926334 | 0.0192 | 1779 | 1.080E-5 | 10.911 | 9.820 |
| 1659 | 32.43 | 1.4720 | 927198 | 0.0189 | 1693 | 1.115E-5 | 11.127 | 10.014 |
| 1681 | 32.73 | 1.4813 | 928027 | 0.0096 | 815 | 1.179E-5 | 11.348 | 10.213 |
| 1704 | 33.05 | 1.4909 | 928822 | 0.0096 | 772 | 1.241E-5 | 11.577 | 10.419 |
| 1728 | 33.38 | 1.5009 | 929582 | 0.0095 | 735 | 1.304E-5 | 11.807 | 10.626 |
| 1751 | 33.70 | 1.5105 | 930308 | 0.0096 | 702 | 1.365E-5 | 12.046 | 10.841 |
| 1775 | 34.02 | 1.5199 | 930964 | 0.0095 | 665 | 1.426E-5 | 12.283 | 11.055 |
| 1799 | 34.34 | 1.5292 | 931605 | 0.0095 | 634 | 1.490E-5 | 12.525 | 11.272 |
| 1823 | 34.67 | 1.5386 | 932236 | 0.0095 | 609 | 1.561E-5 | 12.769 | 11.492 |
| 1847 | 35.00 | 1.5480 | 932812 | 0.0095 | 587 | 1.625E-5 | 13.024 | 11.721 |
| 1872 | 35.35 | 1.5577 | 933388 | 0.0095 | 561 | 1.697E-5 | 13.285 | 11.956 |
| 1899 | 35.71 | 1.5676 | 933964 | 0.0095 | 536 | 1.776E-5 | 13.550 | 12.195 |
| 1924 | 36.06 | 1.5771 | 934486 | 0.0095 | 517 | 1.846E-5 | 13.821 | 12.439 |
| 1949 | 36.40 | 1.5863 | 934973 | 0.0096 | 494 | 1.934E-5 | 14.094 | 12.685 |
| 1976 | 36.76 | 1.5959 | 935454 | 0.0095 | 467 | 2.033E-5 | 14.369 | 12.932 |
| 2002 | 37.11 | 1.6053 | 935913 | 0.0095 | 445 | 2.133E-5 | 14.656 | 13.191 |
| 2029 | 37.49 | 1.6151 | 936349 | 0.0096 | 429 | 2.235E-5 | 14.945 | 13.450 |
| 2056 | 37.86 | 1.6246 | 936765 | 0.0096 | 411 | 2.343E-5 | 15.244 | 13.719 |
| 2084 | 38.23 | 1.6341 | 937157 | 0.0097 | 391 | 2.467E-5 | 15.549 | 13.994 |
| 2112 | 38.62 | 1.6438 | 937548 | 0.0096 | 369 | 2.597E-5 | 15.861 | 14.275 |
| 2141 | 39.02 | 1.6537 | 937922 | 0.0095 | 349 | 2.742E-5 | 16.183 | 14.565 |
| 2170 | 39.42 | 1.6635 | 938259 | 0.0096 | 334 | 2.890E-5 | 16.500 | 14.850 |
| 2198 | 39.79 | 1.6725 | 938562 | 0.0096 | 314 | 3.047E-5 | 16.827 | 15.144 |
| 2226 | 40.18 | 1.6818 | 938861 | 0.0095 | 293 | 3.217E-5 | 17.155 | 15.439 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^5) | deltaK |
|--------------|-------|-----------|--------|------------|-----|-------------------|---------------------|--------|
| 2256 | 40.60 | 1.6916 | 939159 | 0.0094 | 278 | 3.393E-5 | 17.489 | 15.741 |
| 2286 | 41.01 | 1.7011 | 939430 | 0.0096 | 269 | 3.584E-5 | 17.836 | 16.053 |
| 2316 | 41.41 | 1.7105 | 939681 | 0.0097 | 256 | 3.776E-5 | 18.188 | 16.369 |
| 2346 | 41.83 | 1.7199 | 939927 | 0.0096 | 240 | 3.983E-5 | 18.555 | 16.699 |
| 2378 | 42.28 | 1.7301 | 940173 | 0.0096 | 228 | 4.204E-5 | 18.921 | 17.029 |
| 2409 | 42.72 | 1.7397 | 940396 | 0.0096 | 218 | 4.431E-5 | 19.301 | 17.371 |
| 2440 | 43.14 | 1.7490 | 940598 | 0.0098 | 207 | 4.713E-5 | 19.683 | 17.715 |
| 2472 | 43.59 | 1.7586 | 940799 | 0.0096 | 192 | 5.002E-5 | 20.071 | 18.064 |
| 2505 | 44.05 | 1.7683 | 940991 | 0.0095 | 180 | 5.312E-5 | 20.479 | 18.432 |
| 2539 | 44.53 | 1.7785 | 941167 | 0.0096 | 172 | 5.640E-5 | 20.876 | 18.789 |
| 2570 | 44.96 | 1.7875 | 941326 | 0.0097 | 162 | 5.995E-5 | 21.294 | 19.165 |
| 2602 | 45.42 | 1.7968 | 941478 | 0.0096 | 150 | 6.374E-5 | 21.712 | 19.541 |
| 2637 | 45.92 | 1.8069 | 941631 | 0.0095 | 141 | 6.797E-5 | 22.136 | 19.923 |
| 2671 | 46.40 | 1.8166 | 941768 | 0.0096 | 134 | 7.262E-5 | 22.576 | 20.319 |
| 2705 | 46.87 | 1.8258 | 941890 | 0.0097 | 126 | 7.733E-5 | 23.025 | 20.723 |
| 2740 | 47.37 | 1.8354 | 942012 | 0.0097 | 117 | 8.305E-5 | 23.477 | 21.129 |
| 2775 | 47.89 | 1.8453 | 942128 | 0.0196 | 222 | 8.837E-5 | 23.947 | 21.553 |
| 2811 | 48.40 | 1.8551 | 942234 | 0.0195 | 202 | 9.643E-5 | 24.425 | 21.983 |
| | 48.93 | 1.8648 | 942330 | | | | | |
| | 49.47 | 1.8747 | 942436 | | | | | |
| 2800 | 49.96 | 1.8836 | 942538 | 0.0185 | 207 | 8.933E-5 | 24.846 | 22.360 |
| 2800 | 50.50 | 1.8932 | 942643 | 0.0193 | 211 | 9.167E-5 | 25.015 | 22.513 |
| 2800 | 51.05 | 1.9030 | 942749 | 0.0194 | 207 | 9.372E-5 | 25.192 | 22.673 |
| 2800 | 51.61 | 1.9126 | 942850 | 0.0097 | 101 | 9.580E-5 | 25.371 | 22.834 |
| 2800 | 52.16 | 1.9221 | 942948 | 0.0097 | 100 | 9.770E-5 | 25.555 | 22.999 |
| 2800 | 52.75 | 1.9320 | 943046 | 0.0098 | 98 | 9.984E-5 | 25.738 | 23.164 |
| 2800 | 53.33 | 1.9417 | 943143 | 0.0098 | 96 | 1.017E-4 | 25.929 | 23.336 |
| 2800 | 53.94 | 1.9517 | 943241 | 0.0098 | 94 | 1.041E-4 | 26.120 | 23.508 |
| 2800 | 54.55 | 1.9615 | 943334 | 0.0097 | 91 | 1.067E-4 | 26.313 | 23.682 |
| 2800 | 55.16 | 1.9712 | 943424 | 0.0097 | 89 | 1.096E-4 | 26.509 | 23.858 |
| 2800 | 55.78 | 1.9809 | 943509 | 0.0097 | 86 | 1.127E-4 | 26.701 | 24.031 |
| 2800 | 56.38 | 1.9902 | 943590 | 0.0096 | 83 | 1.155E-4 | 26.902 | 24.212 |
| 2800 | 57.03 | 2.0002 | 943676 | 0.0097 | 81 | 1.188E-4 | 27.100 | 24.390 |
| 2800 | 57.69 | 2.0100 | 943757 | 0.0096 | 79 | 1.218E-4 | 27.303 | 24.572 |
| 2800 | 58.32 | 2.0193 | 943833 | 0.0097 | 78 | 1.246E-4 | 27.513 | 24.761 |
| 2800 | 59.00 | 2.0293 | 943910 | 0.0097 | 75 | 1.282E-4 | 27.716 | 24.944 |
| 2800 | 59.67 | 2.0388 | 943983 | 0.0097 | 73 | 1.316E-4 | 27.928 | 25.135 |
| 2800 | 60.34 | 2.0483 | 944056 | 0.0098 | 72 | 1.353E-4 | 28.140 | 25.326 |
| 2800 | 61.04 | 2.0581 | 944126 | 0.0098 | 70 | 1.389E-4 | 28.358 | 25.522 |
| 2800 | 61.77 | 2.0680 | 944196 | 0.0097 | 68 | 1.426E-4 | 28.584 | 25.726 |
| 2800 | 62.53 | 2.0783 | 944267 | 0.0098 | 66 | 1.473E-4 | 28.807 | 25.926 |
| 2800 | 63.25 | 2.0878 | 944330 | 0.0099 | 64 | 1.535E-4 | 29.036 | 26.132 |
| 2800 | 63.97 | 2.0972 | 944392 | 0.0098 | 61 | 1.603E-4 | 29.263 | 26.336 |
| 2800 | 64.73 | 2.1070 | 944452 | 0.0097 | 58 | 1.679E-4 | 29.503 | 26.552 |
| 2800 | 65.57 | 2.1176 | 944511 | 0.0098 | 56 | 1.751E-4 | 29.733 | 26.760 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in]^0.5) |
|--------------|--------|-----------|--------|------------|----|-------------------|--------|-------------------------|
| 2800 | 66.32 | 2.1269 | 944563 | 0.0098 | 55 | 1.802E-4 | 29.981 | 26.983 |
| 2800 | 67.09 | 2.1364 | 944614 | 0.0099 | 53 | 1.843E-4 | 30.220 | 27.198 |
| 2800 | 67.92 | 2.1464 | 944667 | 0.0097 | 52 | 1.869E-4 | 30.463 | 27.417 |
| 2800 | 68.74 | 2.1561 | 944720 | 0.0098 | 51 | 1.907E-4 | 30.719 | 27.646 |
| 2800 | 69.60 | 2.1661 | 944772 | 0.0098 | 50 | 1.962E-4 | 30.970 | 27.872 |
| 2800 | 70.44 | 2.1757 | 944822 | 0.0098 | 48 | 2.056E-4 | 31.231 | 28.108 |
| 2800 | 71.32 | 2.1857 | 944868 | 0.0098 | 45 | 2.174E-4 | 31.486 | 28.337 |
| 2800 | 72.17 | 2.1952 | 944911 | 0.0098 | 43 | 2.293E-4 | 31.757 | 28.581 |
| 2800 | 73.10 | 2.2053 | 944953 | 0.0097 | 41 | 2.411E-4 | 32.023 | 28.820 |
| 2800 | 74.02 | 2.2151 | 944992 | 0.0097 | 39 | 2.521E-4 | 32.296 | 29.066 |
| 2800 | 74.92 | 2.2247 | 945029 | 0.0098 | 38 | 2.612E-4 | 32.570 | 29.312 |
| 2800 | 75.84 | 2.2342 | 945065 | 0.0098 | 36 | 2.699E-4 | 32.849 | 29.563 |
| 2800 | 76.82 | 2.2441 | 945100 | 0.0097 | 35 | 2.792E-4 | 33.130 | 29.816 |
| 2800 | 77.80 | 2.2540 | 945136 | 0.0098 | 33 | 2.925E-4 | 33.422 | 30.079 |
| 2800 | 78.80 | 2.2638 | 945169 | 0.0099 | 32 | 3.057E-4 | 33.711 | 30.339 |
| 2800 | 79.78 | 2.2733 | 945199 | 0.0098 | 31 | 3.198E-4 | 34.016 | 30.613 |
| 2800 | 80.85 | 2.2835 | 945229 | 0.0098 | 29 | 3.391E-4 | 34.317 | 30.884 |
| 2800 | 81.93 | 2.2935 | 945259 | 0.0098 | 27 | 3.580E-4 | 34.627 | 31.163 |
| 2800 | 82.97 | 2.3031 | 945285 | 0.0099 | 26 | 3.772E-4 | 34.941 | 31.445 |
| 2800 | 84.05 | 2.3128 | 945309 | 0.0099 | 25 | 3.990E-4 | 35.250 | 31.723 |
| 2800 | 85.13 | 2.3223 | 945333 | 0.0099 | 23 | 4.256E-4 | 35.574 | 32.015 |
| 2800 | 86.29 | 2.3324 | 945356 | 0.0101 | 22 | 4.590E-4 | 35.906 | 32.313 |
| 2800 | 87.50 | 2.3427 | 945378 | 0.0100 | 21 | 4.863E-4 | 36.245 | 32.618 |
| 2800 | 88.70 | 2.3527 | 945398 | 0.0101 | 20 | 5.123E-4 | 36.611 | 32.946 |
| 2799 | 90.04 | 2.3639 | 945417 | 0.0101 | 19 | 5.399E-4 | 36.952 | 33.255 |
| 2800 | 91.13 | 2.3730 | 945435 | 0.0102 | 18 | 5.757E-4 | 37.317 | 33.582 |
| 2800 | 92.31 | 2.3827 | 945452 | 0.0101 | 17 | 6.112E-4 | 37.671 | 33.902 |
| 2800 | 93.57 | 2.3928 | 945468 | 0.0100 | 15 | 6.597E-4 | 38.046 | 34.240 |
| 2800 | 94.95 | 2.4037 | 945483 | 0.0102 | 14 | 7.230E-4 | 38.416 | 34.569 * |
| 2799 | 96.21 | 2.4134 | 945497 | 0.0103 | 13 | 7.839E-4 | 38.816 | 34.929 * |
| 2799 | 97.56 | 2.4237 | 945509 | 0.0103 | 12 | 8.419E-4 | 39.211 | 35.283 * |
| 2799 | 99.00 | 2.4344 | 945521 | 0.0102 | 12 | 8.904E-4 | 39.609 | 35.641 * |
| 2799 | 100.39 | 2.4444 | 945532 | 0.0103 | 11 | 9.478E-4 | 40.027 | 36.017 * |
| 2799 | 101.81 | 2.4546 | 945542 | 0.0103 | 10 | 9.897E-4 | 40.441 | 36.387 * |
| 2799 | 103.31 | 2.4650 | 945553 | 0.0103 | 10 | 1.048E-3 | 40.866 | 36.771 * |
| 2799 | 104.81 | 2.4753 | 945562 | 0.0104 | 9 | 1.126E-3 | 41.289 | 37.147 * |
| 2798 | 106.29 | 2.4852 | 945571 | 0.0104 | 9 | 1.196E-3 | 41.745 | 37.556 * |
| 2798 | 107.96 | 2.4961 | 945580 | 0.0104 | 8 | 1.283E-3 | 42.193 | 37.957 * |
| 2798 | 109.62 | 2.5068 | 945587 | 0.0107 | 8 | 1.392E-3 | 42.665 | 38.381 * |
| 2798 | 111.26 | 2.5170 | 945595 | 0.0105 | 7 | 1.534E-3 | 43.132 | 38.797 * |
| 2797 | 112.95 | 2.5274 | 945602 | 0.0105 | 6 | 1.693E-3 | 43.654 | 39.266 * |
| 2797 | 114.97 | 2.5395 | 945608 | 0.0105 | 6 | 1.909E-3 | 44.079 | 39.636 * |
| 2794 | 116.50 | 2.5485 | 945613 | 0.0105 | 5 | 2.114E-3 | 44.610 | 40.099 * |
| 2791 | 118.40 | 2.5593 | 945618 | 0.0106 | 5 | 2.415E-3 | 45.100 | 40.539 * |
| 2795 | 120.28 | 2.5699 | 945622 | 0.0101 | 4 | 2.670E-3 | 45.579 | 40.952 * |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in]^0.5) |
|--------------|--------|-----------|--------|------------|----|-------------------|--------|-------------------------|
| 2792 | 122.17 | 2.5802 | 945626 | 0.0104 | 4 | 2.815E-3 | 46.127 | 41.439 * |
| 2789 | 124.18 | 2.5910 | 945629 | 0.0104 | 4 | 2.977E-3 | 46.627 | 41.882 * |
| 2790 | 125.98 | 2.6004 | 945632 | 0.0105 | 3 | 3.221E-3 | 47.141 | 42.324 * |
| 2787 | 128.07 | 2.6111 | 945636 | 0.0216 | 7 | 3.080E-3 | 47.631 | 42.746 * |
| 2779 | 130.25 | 2.6219 | 945639 | 0.0216 | 5 | 4.324E-3 | 48.079 | 43.109 * |
| | 132.46 | 2.6327 | 945641 | | | | | |

Automated Fatigue Crack
Growth Rate Analysis

| | | | |
|-----------------|--------------|---------------|------|
| Test ID | 5083-FCG-2 | Geometry | C(T) |
| Contract | SSC 10624-01 | Orientation | T-L |
| Material | 5083-H321 | Yield (ksi) | 34.3 |
| Temperature (F) | 75 | Modulus (Msi) | 10.5 |
| Environment | RH = 40% | | |

Specimen Dimensions (in)

| | | | |
|---------------|-------|-------------|-------|
| Thickness | 0.498 | Height | 2.400 |
| Net Thickness | 0.498 | Notch Depth | 1.000 |
| Width | 4.000 | Gage Length | 0.500 |

Precrack Parameters

| | | | |
|--------------|-------|---------------------|------|
| Pmax (lbs) | 782.0 | Stress Ratio | 0.10 |
| Final a (in) | 1.050 | Kmax (ksi sqrt(in)) | 4.00 |

Test Parameters

| EvBP | Freq | Pmax | R | Ai | Kmaxi | C | DKi |
|--------|-------|------|------|-------|-------|------|------|
| 23.508 | 10.00 | 0 | 0.10 | 1.140 | 3.00 | 4.00 | 0.00 |
| 31.601 | 10.00 | 0 | 0.10 | 1.455 | 10.58 | 2.00 | 0.00 |
| 49.466 | 5.00 | 2800 | 0.10 | 0.000 | 0.00 | 0.00 | 0.00 |

| K Coeff | C Coeff |
|---------|----------|
| .886 | 1.00098 |
| 4.64 | -4.66951 |
| -13.32 | 18.4601 |
| 14.72 | -236.825 |
| -5.6 | 1214.88 |
| . | -2143.57 |

Visual Observations

| EvB/P | Crack(EvB/P) | Crack(visual) | Error | CAF |
|---------|--------------|---------------|--------|-------|
| 20.449 | 0.996 | 1.000 | 0.004 | 1.019 |
| 21.848 | 1.067 | 1.075 | 0.008 | 1.015 |
| 23.496 | 1.145 | 1.150 | 0.005 | 1.010 |
| 27.159 | 1.296 | 1.295 | -0.001 | 1.001 |
| 31.498 | 1.447 | 1.430 | -0.017 | 0.992 |
| 42.053 | 1.727 | 1.720 | -0.007 | 0.976 |
| 49.149 | 1.870 | 1.870 | 0.000 | 0.968 |
| 104.045 | 2.464 | 2.470 | 0.006 | 0.936 |

Comments

Date of test: 8/14/2006
Waveform Type Sine

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi(in) ^{.5}) |
|--------------|-------|-----------|--------|------------|--------|-------------------|-------|------------------------------------|
| | 23.51 | 1.1452 | 5353 | | | | | |
| 546 | 23.56 | 1.1477 | 40922 | 0.0074 | 98021 | 7.540E-8 | 2.997 | 2.697 |
| 556 | 23.67 | 1.1526 | 103374 | 0.0097 | 117902 | 8.199E-8 | 3.043 | 2.739 |
| 566 | 23.78 | 1.1574 | 158824 | 0.0044 | 51514 | 8.606E-8 | 3.105 | 2.794 |
| 575 | 23.88 | 1.1619 | 211935 | 0.0048 | 53696 | 8.948E-8 | 3.168 | 2.851 |
| 585 | 23.99 | 1.1667 | 263545 | 0.0047 | 50237 | 9.425E-8 | 3.232 | 2.908 |
| 595 | 24.10 | 1.1716 | 314436 | 0.0047 | 47764 | 9.928E-8 | 3.299 | 2.969 |
| 606 | 24.22 | 1.1766 | 363099 | 0.0047 | 45445 | 1.049E-7 | 3.365 | 3.028 |
| 616 | 24.32 | 1.1811 | 404796 | 0.0048 | 43195 | 1.105E-7 | 3.434 | 3.090 |
| 626 | 24.43 | 1.1857 | 445408 | 0.0048 | 41024 | 1.167E-7 | 3.500 | 3.150 |
| 636 | 24.54 | 1.1904 | 484607 | 0.0047 | 38584 | 1.227E-7 | 3.571 | 3.214 |
| 647 | 24.65 | 1.1952 | 522712 | 0.0047 | 36811 | 1.288E-7 | 3.644 | 3.280 |
| 659 | 24.77 | 1.2003 | 560580 | 0.0047 | 34973 | 1.359E-7 | 3.717 | 3.346 |
| 670 | 24.88 | 1.2050 | 594601 | 0.0048 | 33124 | 1.438E-7 | 3.793 | 3.414 |
| 681 | 24.99 | 1.2096 | 625664 | 0.0048 | 31162 | 1.528E-7 | 3.868 | 3.481 |
| 692 | 25.10 | 1.2142 | 655247 | 0.0047 | 28992 | 1.633E-7 | 3.945 | 3.550 |
| 704 | 25.21 | 1.2189 | 683351 | 0.0047 | 27070 | 1.754E-7 | 4.024 | 3.622 |
| 716 | 25.33 | 1.2237 | 709682 | 0.0047 | 25245 | 1.880E-7 | 4.106 | 3.696 |
| 729 | 25.45 | 1.2286 | 734534 | 0.0047 | 23470 | 2.017E-7 | 4.190 | 3.771 |
| 741 | 25.56 | 1.2333 | 757019 | 0.0047 | 21784 | 2.169E-7 | 4.273 | 3.846 |
| 753 | 25.67 | 1.2378 | 777136 | 0.0047 | 20078 | 2.354E-7 | 4.357 | 3.921 |
| 765 | 25.79 | 1.2423 | 796069 | 0.0046 | 18209 | 2.584E-7 | 4.442 | 3.998 |
| 778 | 25.90 | 1.2470 | 814055 | 0.0046 | 16482 | 2.883E-7 | 4.532 | 4.078 |
| 792 | 26.02 | 1.2519 | 830152 | 0.0047 | 15049 | 3.256E-7 | 4.620 | 4.158 |
| 805 | 26.14 | 1.2564 | 843789 | 0.0048 | 13449 | 3.710E-7 | 4.715 | 4.243 |
| 819 | 26.26 | 1.2611 | 855912 | 0.0047 | 11679 | 4.264E-7 | 4.810 | 4.329 |
| 833 | 26.38 | 1.2661 | 867429 | 0.0047 | 10044 | 5.022E-7 | 4.908 | 4.417 |
| 848 | 26.51 | 1.2709 | 876763 | 0.0047 | 8692 | 5.905E-7 | 5.006 | 4.505 |
| 861 | 26.62 | 1.2754 | 884131 | 0.0047 | 7541 | 6.819E-7 | 5.108 | 4.597 |
| 876 | 26.74 | 1.2800 | 890415 | 0.0046 | 6409 | 7.704E-7 | 5.205 | 4.685 |
| 890 | 26.86 | 1.2845 | 895941 | 0.0047 | 5557 | 8.682E-7 | 5.310 | 4.779 |
| 906 | 26.98 | 1.2893 | 901160 | 0.0047 | 4959 | 9.746E-7 | 5.413 | 4.872 |
| 921 | 27.10 | 1.2939 | 905881 | 0.0047 | 4474 | 1.088E-6 | 5.526 | 4.973 |
| 937 | 27.23 | 1.2989 | 910107 | 0.0047 | 4057 | 1.202E-6 | 5.635 | 5.072 |
| 953 | 27.36 | 1.3036 | 913882 | 0.0047 | 3680 | 1.311E-6 | 5.752 | 5.177 |
| 969 | 27.48 | 1.3083 | 917260 | 0.0047 | 3338 | 1.433E-6 | 5.864 | 5.277 |
| 985 | 27.60 | 1.3127 | 920282 | 0.0046 | 3010 | 1.565E-6 | 5.981 | 5.383 |
| 1001 | 27.73 | 1.3173 | 923239 | 0.0046 | 2754 | 1.715E-6 | 6.099 | 5.489 |
| 1019 | 27.86 | 1.3222 | 925906 | 0.0047 | 2529 | 1.885E-6 | 6.219 | 5.597 |
| 1036 | 27.98 | 1.3267 | 928167 | 0.0047 | 2341 | 2.050E-6 | 6.344 | 5.710 |
| 1053 | 28.11 | 1.3314 | 930403 | 0.0047 | 2146 | 2.226E-6 | 6.471 | 5.824 |
| 1071 | 28.24 | 1.3362 | 932435 | 0.0047 | 1959 | 2.414E-6 | 6.601 | 5.941 |
| 1089 | 28.37 | 1.3409 | 934325 | 0.0047 | 1812 | 2.640E-6 | 6.733 | 6.060 |
| 1108 | 28.51 | 1.3457 | 936114 | 0.0047 | 1657 | 2.903E-6 | 6.868 | 6.181 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in]^0.5) |
|--------------|-------|-----------|--------|------------|------|-------------------|--------|-------------------------|
| 1126 | 28.64 | 1.3503 | 937659 | 0.0047 | 1524 | 3.172E-6 | 7.006 | 6.305 |
| 1145 | 28.77 | 1.3550 | 939041 | 0.0047 | 1394 | 3.457E-6 | 7.145 | 6.430 |
| 1165 | 28.90 | 1.3597 | 940342 | 0.0047 | 1270 | 3.724E-6 | 7.289 | 6.560 |
| 1185 | 29.04 | 1.3645 | 941578 | 0.0047 | 1178 | 4.013E-6 | 7.435 | 6.691 |
| 1205 | 29.17 | 1.3692 | 942686 | 0.0047 | 1103 | 4.289E-6 | 7.580 | 6.822 |
| 1224 | 29.30 | 1.3736 | 943733 | 0.0047 | 1032 | 4.592E-6 | 7.735 | 6.961 |
| 1246 | 29.44 | 1.3785 | 944727 | 0.0047 | 965 | 4.918E-6 | 7.885 | 7.097 |
| 1267 | 29.58 | 1.3832 | 945657 | 0.0048 | 912 | 5.252E-6 | 8.046 | 7.242 |
| 1288 | 29.72 | 1.3880 | 946532 | 0.0048 | 856 | 5.623E-6 | 8.210 | 7.389 |
| 1311 | 29.86 | 1.3928 | 947365 | 0.0048 | 802 | 5.980E-6 | 8.377 | 7.539 |
| 1333 | 30.00 | 1.3977 | 948157 | 0.0047 | 753 | 6.334E-6 | 8.549 | 7.694 |
| 1357 | 30.15 | 1.4025 | 948867 | 0.0047 | 707 | 6.642E-6 | 8.720 | 7.848 |
| 1379 | 30.28 | 1.4071 | 949538 | 0.0047 | 667 | 6.989E-6 | 8.893 | 8.004 |
| 1401 | 30.42 | 1.4116 | 950175 | 0.0047 | 629 | 7.364E-6 | 9.064 | 8.158 |
| 1424 | 30.55 | 1.4160 | 950773 | 0.0046 | 601 | 7.731E-6 | 9.244 | 8.319 |
| 1449 | 30.70 | 1.4208 | 951366 | 0.0047 | 578 | 8.157E-6 | 9.424 | 8.482 |
| 1473 | 30.85 | 1.4256 | 951931 | 0.0047 | 558 | 8.532E-6 | 9.615 | 8.654 |
| 1498 | 30.99 | 1.4303 | 952470 | 0.0048 | 534 | 8.911E-6 | 9.814 | 8.832 |
| 1525 | 31.15 | 1.4353 | 953008 | 0.0097 | 1050 | 9.195E-6 | 10.009 | 9.008 |
| 1550 | 31.29 | 1.4400 | 953520 | 0.0093 | 968 | 9.641E-6 | 10.215 | 9.194 |
| | 31.44 | 1.4447 | 953976 | | | | | |
| | 31.60 | 1.4498 | 954790 | | | | | |
| 1612 | 31.80 | 1.4560 | 955367 | 0.0160 | 1474 | 1.087E-5 | 10.765 | 9.689 |
| 1634 | 32.11 | 1.4659 | 956264 | 0.0192 | 1750 | 1.095E-5 | 10.940 | 9.846 |
| 1656 | 32.41 | 1.4752 | 957117 | 0.0190 | 1660 | 1.146E-5 | 11.164 | 10.048 |
| 1679 | 32.73 | 1.4849 | 957924 | 0.0095 | 799 | 1.191E-5 | 11.381 | 10.243 |
| 1701 | 33.04 | 1.4943 | 958705 | 0.0095 | 766 | 1.238E-5 | 11.609 | 10.448 |
| 1724 | 33.36 | 1.5037 | 959432 | 0.0095 | 732 | 1.292E-5 | 11.839 | 10.655 |
| 1748 | 33.68 | 1.5132 | 960160 | 0.0095 | 700 | 1.350E-5 | 12.072 | 10.865 |
| 1772 | 34.01 | 1.5227 | 960860 | 0.0095 | 669 | 1.417E-5 | 12.314 | 11.083 |
| 1796 | 34.34 | 1.5322 | 961506 | 0.0095 | 642 | 1.482E-5 | 12.557 | 11.302 |
| 1820 | 34.67 | 1.5417 | 962126 | 0.0095 | 610 | 1.555E-5 | 12.807 | 11.527 |
| 1845 | 35.01 | 1.5512 | 962718 | 0.0095 | 584 | 1.627E-5 | 13.061 | 11.755 |
| 1870 | 35.35 | 1.5607 | 963284 | 0.0095 | 561 | 1.698E-5 | 13.318 | 11.986 |
| 1894 | 35.69 | 1.5700 | 963822 | 0.0095 | 534 | 1.770E-5 | 13.584 | 12.225 |
| 1920 | 36.05 | 1.5797 | 964361 | 0.0094 | 506 | 1.859E-5 | 13.856 | 12.470 |
| 1947 | 36.41 | 1.5895 | 964873 | 0.0095 | 487 | 1.955E-5 | 14.127 | 12.714 |
| 1972 | 36.75 | 1.5985 | 965328 | 0.0096 | 468 | 2.051E-5 | 14.409 | 12.968 |
| 1998 | 37.11 | 1.6078 | 965755 | 0.0095 | 442 | 2.148E-5 | 14.693 | 13.223 |
| 2026 | 37.49 | 1.6176 | 966204 | 0.0094 | 417 | 2.260E-5 | 14.986 | 13.488 |
| 2054 | 37.88 | 1.6275 | 966630 | 0.0095 | 399 | 2.380E-5 | 15.285 | 13.756 |
| 2081 | 38.24 | 1.6367 | 967012 | 0.0095 | 382 | 2.503E-5 | 15.592 | 14.033 |
| 2109 | 38.62 | 1.6461 | 967375 | 0.0095 | 361 | 2.633E-5 | 15.896 | 14.306 |
| 2136 | 39.00 | 1.6556 | 967721 | 0.0095 | 342 | 2.771E-5 | 16.209 | 14.588 |
| 2165 | 39.39 | 1.6651 | 968049 | 0.0095 | 327 | 2.907E-5 | 16.528 | 14.875 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^0.5) | deltaK |
|--------------|-------|-----------|--------|------------|-----|-------------------|-----------------------|--------|
| 2194 | 39.78 | 1.6744 | 968369 | 0.0095 | 310 | 3.056E-5 | 16.861 | 15.175 |
| 2224 | 40.20 | 1.6843 | 968684 | 0.0095 | 295 | 3.224E-5 | 17.193 | 15.473 |
| 2253 | 40.60 | 1.6938 | 968973 | 0.0096 | 281 | 3.415E-5 | 17.535 | 15.782 |
| 2282 | 41.01 | 1.7031 | 969233 | 0.0096 | 264 | 3.644E-5 | 17.882 | 16.094 |
| 2313 | 41.42 | 1.7126 | 969491 | 0.0095 | 247 | 3.879E-5 | 18.236 | 16.413 |
| 2344 | 41.86 | 1.7225 | 969737 | 0.0096 | 233 | 4.129E-5 | 18.600 | 16.740 |
| 2375 | 42.29 | 1.7320 | 969952 | 0.0096 | 222 | 4.358E-5 | 18.970 | 17.073 |
| 2405 | 42.71 | 1.7413 | 970163 | 0.0096 | 210 | 4.596E-5 | 19.354 | 17.419 |
| 2438 | 43.17 | 1.7513 | 970373 | 0.0096 | 198 | 4.842E-5 | 19.734 | 17.761 |
| 2470 | 43.62 | 1.7609 | 970565 | 0.0096 | 188 | 5.084E-5 | 20.132 | 18.119 |
| 2502 | 44.07 | 1.7704 | 970748 | 0.0095 | 178 | 5.352E-5 | 20.530 | 18.478 |
| 2535 | 44.53 | 1.7800 | 970922 | 0.0095 | 167 | 5.674E-5 | 20.934 | 18.841 |
| 2568 | 44.98 | 1.7894 | 971082 | 0.0095 | 157 | 6.045E-5 | 21.336 | 19.203 |
| 2599 | 45.43 | 1.7984 | 971232 | 0.0095 | 148 | 6.461E-5 | 21.758 | 19.583 |
| 2633 | 45.91 | 1.8080 | 971374 | 0.0095 | 138 | 6.909E-5 | 22.180 | 19.962 |
| 2667 | 46.40 | 1.8178 | 971509 | 0.0095 | 129 | 7.409E-5 | 22.623 | 20.361 |
| 2702 | 46.90 | 1.8274 | 971635 | 0.0096 | 121 | 7.942E-5 | 23.072 | 20.765 |
| 2736 | 47.39 | 1.8369 | 971752 | 0.0096 | 114 | 8.479E-5 | 23.525 | 21.173 |
| 2770 | 47.88 | 1.8463 | 971858 | 0.0189 | 207 | 9.112E-5 | 23.988 | 21.590 |
| 2806 | 48.39 | 1.8558 | 971959 | 0.0190 | 197 | 9.659E-5 | 24.454 | 22.009 |
| | 48.91 | 1.8653 | 972055 | | | | | |
| | 49.47 | 1.8756 | 972161 | | | | | |
| 2800 | 49.96 | 1.8845 | 972258 | 0.0187 | 197 | 9.500E-5 | 24.922 | 22.430 |
| 2800 | 50.51 | 1.8943 | 972358 | 0.0194 | 201 | 9.659E-5 | 25.092 | 22.582 |
| 2800 | 51.06 | 1.9039 | 972459 | 0.0192 | 197 | 9.723E-5 | 25.270 | 22.743 |
| 2800 | 51.62 | 1.9134 | 972555 | 0.0096 | 95 | 1.009E-4 | 25.447 | 22.902 |
| 2800 | 52.16 | 1.9228 | 972647 | 0.0096 | 93 | 1.035E-4 | 25.629 | 23.066 |
| 2800 | 52.75 | 1.9326 | 972738 | 0.0097 | 91 | 1.066E-4 | 25.812 | 23.231 |
| 2800 | 53.34 | 1.9424 | 972829 | 0.0097 | 89 | 1.096E-4 | 26.001 | 23.401 |
| 2800 | 53.94 | 1.9521 | 972916 | 0.0097 | 87 | 1.117E-4 | 26.192 | 23.573 |
| 2800 | 54.55 | 1.9618 | 973002 | 0.0097 | 85 | 1.137E-4 | 26.386 | 23.747 |
| 2800 | 55.17 | 1.9717 | 973086 | 0.0096 | 83 | 1.159E-4 | 26.576 | 23.918 |
| 2800 | 55.76 | 1.9808 | 973166 | 0.0096 | 81 | 1.177E-4 | 26.775 | 24.097 |
| 2800 | 56.40 | 1.9907 | 973248 | 0.0096 | 79 | 1.207E-4 | 26.968 | 24.271 |
| 2800 | 57.03 | 2.0003 | 973327 | 0.0096 | 77 | 1.239E-4 | 27.169 | 24.452 |
| 2800 | 57.67 | 2.0098 | 973404 | 0.0097 | 76 | 1.276E-4 | 27.374 | 24.636 |
| 2800 | 58.34 | 2.0197 | 973477 | 0.0096 | 73 | 1.308E-4 | 27.577 | 24.819 |
| 2800 | 59.00 | 2.0293 | 973550 | 0.0097 | 72 | 1.347E-4 | 27.788 | 25.009 |
| 2800 | 59.68 | 2.0390 | 973620 | 0.0097 | 70 | 1.377E-4 | 27.993 | 25.194 |
| 2800 | 60.33 | 2.0481 | 973687 | 0.0096 | 69 | 1.398E-4 | 28.214 | 25.393 |
| 2800 | 61.08 | 2.0584 | 973758 | 0.0096 | 67 | 1.428E-4 | 28.423 | 25.580 |
| 2800 | 61.77 | 2.0679 | 973824 | 0.0097 | 66 | 1.470E-4 | 28.647 | 25.782 |
| 2800 | 62.48 | 2.0774 | 973889 | 0.0098 | 64 | 1.516E-4 | 28.866 | 25.979 |
| 2800 | 63.20 | 2.0869 | 973952 | 0.0097 | 62 | 1.571E-4 | 29.097 | 26.187 |
| 2800 | 64.00 | 2.0973 | 974014 | 0.0097 | 60 | 1.636E-4 | 29.321 | 26.389 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in]^0.5) |
|--------------|--------|-----------|--------|------------|----|-------------------|--------|-------------------------|
| 2800 | 64.74 | 2.1067 | 974071 | 0.0098 | 58 | 1.697E-4 | 29.562 | 26.605 |
| 2800 | 65.51 | 2.1165 | 974127 | 0.0097 | 55 | 1.762E-4 | 29.796 | 26.816 |
| 2800 | 66.31 | 2.1263 | 974182 | 0.0096 | 53 | 1.825E-4 | 30.034 | 27.030 |
| 2800 | 67.10 | 2.1360 | 974234 | 0.0097 | 51 | 1.888E-4 | 30.273 | 27.245 |
| 2800 | 67.87 | 2.1452 | 974281 | 0.0097 | 50 | 1.947E-4 | 30.516 | 27.463 |
| 2800 | 68.68 | 2.1548 | 974329 | 0.0097 | 48 | 2.024E-4 | 30.761 | 27.685 |
| 2800 | 69.54 | 2.1648 | 974379 | 0.0097 | 46 | 2.111E-4 | 31.014 | 27.912 |
| 2800 | 70.40 | 2.1746 | 974425 | 0.0098 | 45 | 2.197E-4 | 31.274 | 28.146 |
| 2800 | 71.28 | 2.1845 | 974467 | 0.0098 | 43 | 2.287E-4 | 31.536 | 28.382 |
| 2800 | 72.16 | 2.1943 | 974509 | 0.0098 | 41 | 2.383E-4 | 31.802 | 28.621 |
| 2800 | 73.07 | 2.2041 | 974549 | 0.0098 | 39 | 2.476E-4 | 32.068 | 28.861 |
| 2800 | 73.96 | 2.2136 | 974587 | 0.0098 | 38 | 2.575E-4 | 32.341 | 29.106 |
| 2800 | 74.89 | 2.2234 | 974625 | 0.0098 | 36 | 2.688E-4 | 32.617 | 29.355 |
| 2800 | 75.86 | 2.2334 | 974661 | 0.0097 | 35 | 2.798E-4 | 32.902 | 29.611 |
| 2800 | 76.85 | 2.2435 | 974695 | 0.0098 | 34 | 2.909E-4 | 33.185 | 29.866 |
| 2800 | 77.80 | 2.2529 | 974727 | 0.0098 | 32 | 3.046E-4 | 33.470 | 30.122 |
| 2800 | 78.74 | 2.2621 | 974757 | 0.0098 | 31 | 3.182E-4 | 33.764 | 30.387 |
| 2800 | 79.80 | 2.2723 | 974789 | 0.0097 | 29 | 3.364E-4 | 34.056 | 30.649 |
| 2800 | 80.85 | 2.2823 | 974817 | 0.0098 | 28 | 3.579E-4 | 34.364 | 30.926 |
| 2800 | 81.91 | 2.2921 | 974844 | 0.0099 | 26 | 3.843E-4 | 34.675 | 31.206 |
| 2800 | 82.99 | 2.3019 | 974869 | 0.0098 | 24 | 4.105E-4 | 34.987 | 31.487 |
| 2800 | 84.09 | 2.3118 | 974892 | 0.0098 | 23 | 4.371E-4 | 35.306 | 31.773 |
| 2800 | 85.20 | 2.3216 | 974913 | 0.0099 | 21 | 4.650E-4 | 35.621 | 32.056 |
| 2800 | 86.28 | 2.3309 | 974933 | 0.0098 | 20 | 4.871E-4 | 35.954 | 32.356 |
| 2800 | 87.49 | 2.3411 | 974953 | 0.0098 | 19 | 5.112E-4 | 36.287 | 32.656 |
| 2800 | 88.72 | 2.3514 | 974972 | 0.0098 | 18 | 5.382E-4 | 36.621 | 32.956 |
| 2800 | 89.85 | 2.3607 | 974990 | 0.0098 | 17 | 5.723E-4 | 36.977 | 33.276 |
| 2800 | 91.11 | 2.3707 | 975007 | 0.0098 | 16 | 6.044E-4 | 37.312 | 33.577 |
| 2800 | 92.33 | 2.3803 | 975022 | 0.0097 | 16 | 6.339E-4 | 37.666 | 33.896 |
| 2799 | 93.57 | 2.3899 | 975036 | 0.0098 | 15 | 6.730E-4 | 38.026 | 34.219 |
| 2799 | 94.89 | 2.3999 | 975051 | 0.0098 | 14 | 7.110E-4 | 38.384 | 34.540 |
| 2799 | 96.20 | 2.4096 | 975065 | 0.0098 | 13 | 7.489E-4 | 38.763 | 34.880 * |
| 2799 | 97.57 | 2.4196 | 975077 | 0.0099 | 13 | 7.860E-4 | 39.135 | 35.215 * |
| 2799 | 98.92 | 2.4292 | 975089 | 0.0099 | 12 | 8.373E-4 | 39.526 | 35.566 * |
| 2799 | 100.37 | 2.4394 | 975101 | 0.0103 | 11 | 9.104E-4 | 39.917 | 35.918 * |
| 2799 | 101.81 | 2.4493 | 975112 | 0.0104 | 11 | 9.984E-4 | 40.322 | 36.280 * |
| 2799 | 103.31 | 2.4594 | 975122 | 0.0101 | 10 | 1.082E-3 | 40.748 | 36.656 * |
| 2795 | 105.09 | 2.4713 | 975132 | 0.0103 | 9 | 1.177E-3 | 41.191 | 37.057 * |
| 2797 | 106.66 | 2.4819 | 975140 | 0.0103 | 8 | 1.256E-3 | 41.593 | 37.412 * |
| 2797 | 107.89 | 2.4899 | 975147 | 0.0103 | 8 | 1.336E-3 | 42.089 | 37.860 * |
| 2798 | 109.66 | 2.5013 | 975155 | 0.0101 | 7 | 1.443E-3 | 42.494 | 38.226 * |
| 2798 | 111.26 | 2.5113 | 975162 | 0.0101 | 7 | 1.591E-3 | 42.968 | 38.645 * |
| 2796 | 112.86 | 2.5212 | 975168 | 0.0105 | 6 | 1.692E-3 | 43.454 | 39.081 * |
| 2797 | 114.66 | 2.5320 | 975174 | 0.0104 | 6 | 1.810E-3 | 43.921 | 39.499 * |
| 2797 | 116.46 | 2.5427 | 975179 | 0.0104 | 6 | 1.891E-3 | 44.428 | 39.951 * |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in]^0.5) |
|--------------|--------|-----------|--------|------------|----|-------------------|--------|-------------------------|
| 2797 | 118.25 | 2.5530 | 975185 | 0.0104 | 5 | 1.991E-3 | 44.940 | 40.407 * |
| 2795 | 120.18 | 2.5638 | 975190 | 0.0104 | 5 | 2.122E-3 | 45.418 | 40.832 * |
| 2793 | 121.95 | 2.5735 | 975195 | 0.0104 | 5 | 2.398E-3 | 45.910 | 41.256 * |
| 2790 | 123.80 | 2.5835 | 975199 | 0.0107 | 4 | 2.766E-3 | 46.433 | 41.721 * |
| 2792 | 125.86 | 2.5943 | 975203 | 0.0107 | 4 | 3.134E-3 | 46.887 | 42.101 * |
| 2783 | 127.99 | 2.6053 | 975206 | 0.0107 | 3 | 3.510E-3 | 47.418 | 42.547 * |
| 2772 | 130.39 | 2.6173 | 975209 | 0.0226 | 6 | 3.767E-3 | 47.854 | 42.899 * |
| 2763 | 132.56 | 2.6279 | 975212 | 0.0201 | 5 | 4.023E-3 | 48.314 | 43.261 * |
| | 134.56 | 2.6374 | 975214 | | | | | |

Automated Fatigue Crack
Growth Rate Analysis

| | | | |
|-----------------|--------------|---------------|------|
| Test ID | 5083-FCG-3 | Geometry | C(T) |
| Contract | SSC 10624-01 | Orientation | T-L |
| Material | 5083-H321 | Yield (ksi) | 34.3 |
| Temperature (F) | 75 | Modulus (Msi) | 10.5 |
| Environment | Sea Water | | |

Specimen Dimensions (in)

| | | | |
|---------------|-------|-------------|-------|
| Thickness | 0.498 | Height | 2.400 |
| Net Thickness | 0.498 | Notch Depth | 1.000 |
| Width | 4.001 | Gage Length | 0.500 |

Precrack Parameters

| | | | |
|--------------|-------|---------------------|------|
| Pmax (lbs) | 783.0 | Stress Ratio | 0.10 |
| Final a (in) | 1.050 | Kmax (ksi sqrt[in]) | 4.00 |

Test Parameters

| EvBP | Freq | Pmax | R | Ai | Kmaxi | C | DKi |
|--------|------|------|------|-------|-------|------|------|
| 33.806 | 5.00 | 0 | 0.10 | 1.200 | 2.40 | 2.00 | 0.00 |
| 33.806 | 5.00 | 0 | 0.10 | 1.531 | 9.01 | 2.00 | 0.00 |
| 62.078 | 5.00 | 2300 | 0.10 | 0.000 | 0.00 | 0.00 | 0.00 |

| K Coeff | C Coeff |
|---------|----------|
| .886 | 1.00098 |
| 4.64 | -4.66951 |
| -13.32 | 18.4601 |
| 14.72 | -236.825 |
| -5.6 | 1214.88 |
| . | -2143.57 |

Visual Observations

| EvB/P | Crack(EvB/P) | Crack(visual) | Error | CAF |
|--------|--------------|---------------|--------|-------|
| 20.705 | 1.012 | 1.000 | -0.012 | 1.020 |
| 21.841 | 1.068 | 1.060 | -0.008 | 1.016 |
| 23.618 | 1.150 | 1.160 | 0.010 | 1.009 |
| 24.536 | 1.190 | 1.190 | 0.000 | 1.006 |
| 24.722 | 1.197 | 1.200 | 0.003 | 1.006 |
| 25.856 | 1.244 | 1.250 | 0.006 | 1.002 |
| 29.095 | 1.363 | 1.370 | 0.007 | 0.993 |
| 33.824 | 1.512 | 1.510 | -0.002 | 0.982 |
| 47.605 | 1.831 | 1.830 | -0.001 | 0.959 |
| 58.004 | 2.003 | 2.000 | -0.003 | 0.947 |

Comments

Date of test: 8/21/2006
Waveform Type Sine

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in]^0.5) |
|--------------|-------|-----------|--------|------------|--------|-------------------|-------|-------------------------|
| | 24.73 | 1.1979 | 1932 | | | | | |
| 417 | 24.77 | 1.1996 | 27582 | 0.0057 | 85243 | 6.655E-8 | 2.359 | 2.124 |
| 423 | 24.87 | 1.2035 | 87175 | 0.0085 | 123618 | 6.901E-8 | 2.392 | 2.153 |
| 430 | 24.98 | 1.2081 | 151200 | 0.0040 | 51273 | 7.998E-8 | 2.436 | 2.192 |
| 437 | 25.09 | 1.2127 | 207030 | 0.0045 | 54630 | 8.420E-8 | 2.485 | 2.237 |
| 445 | 25.21 | 1.2175 | 258821 | 0.0047 | 51470 | 9.169E-8 | 2.535 | 2.281 |
| 452 | 25.32 | 1.2221 | 309570 | 0.0046 | 47230 | 9.928E-8 | 2.586 | 2.327 |
| 460 | 25.44 | 1.2268 | 355363 | 0.0046 | 43823 | 1.069E-7 | 2.638 | 2.374 |
| 468 | 25.55 | 1.2315 | 395997 | 0.0046 | 40644 | 1.155E-7 | 2.690 | 2.421 |
| 475 | 25.67 | 1.2360 | 434579 | 0.0046 | 37438 | 1.248E-7 | 2.743 | 2.469 |
| 483 | 25.78 | 1.2405 | 469966 | 0.0047 | 34855 | 1.347E-7 | 2.797 | 2.517 |
| 491 | 25.90 | 1.2452 | 502687 | 0.0047 | 32526 | 1.452E-7 | 2.852 | 2.567 |
| 500 | 26.02 | 1.2498 | 534196 | 0.0047 | 30338 | 1.561E-7 | 2.912 | 2.620 |
| 509 | 26.14 | 1.2548 | 564493 | 0.0047 | 28278 | 1.664E-7 | 2.970 | 2.673 |
| 517 | 26.26 | 1.2596 | 591155 | 0.0046 | 26379 | 1.775E-7 | 3.031 | 2.728 |
| 526 | 26.38 | 1.2641 | 616605 | 0.0047 | 24682 | 1.896E-7 | 3.090 | 2.781 |
| 534 | 26.50 | 1.2685 | 639631 | 0.0046 | 22864 | 2.019E-7 | 3.152 | 2.837 |
| 544 | 26.62 | 1.2731 | 660960 | 0.0046 | 21491 | 2.154E-7 | 3.213 | 2.892 |
| 553 | 26.74 | 1.2778 | 682289 | 0.0046 | 19996 | 2.317E-7 | 3.278 | 2.950 |
| 562 | 26.86 | 1.2824 | 701679 | 0.0047 | 18614 | 2.515E-7 | 3.344 | 3.010 |
| 572 | 26.99 | 1.2872 | 720100 | 0.0046 | 17256 | 2.744E-7 | 3.411 | 3.070 |
| 582 | 27.11 | 1.2917 | 736580 | 0.0046 | 15666 | 3.013E-7 | 3.480 | 3.132 |
| 592 | 27.24 | 1.2965 | 751313 | 0.0046 | 14358 | 3.296E-7 | 3.549 | 3.194 |
| 602 | 27.36 | 1.3010 | 764496 | 0.0046 | 13108 | 3.577E-7 | 3.619 | 3.257 |
| 611 | 27.48 | 1.3054 | 776283 | 0.0046 | 12016 | 3.862E-7 | 3.691 | 3.322 |
| 622 | 27.60 | 1.3101 | 787825 | 0.0046 | 11133 | 4.144E-7 | 3.763 | 3.387 |
| 632 | 27.73 | 1.3147 | 798747 | 0.0046 | 10342 | 4.473E-7 | 3.839 | 3.455 |
| 643 | 27.86 | 1.3194 | 808675 | 0.0046 | 9702 | 4.790E-7 | 3.915 | 3.524 |
| 654 | 27.99 | 1.3240 | 818108 | 0.0046 | 9037 | 5.161E-7 | 3.994 | 3.594 |
| 665 | 28.12 | 1.3286 | 826549 | 0.0046 | 8342 | 5.571E-7 | 4.071 | 3.664 |
| 676 | 28.24 | 1.3330 | 834497 | 0.0046 | 7746 | 6.031E-7 | 4.154 | 3.738 |
| 687 | 28.37 | 1.3378 | 842046 | 0.0046 | 7127 | 6.579E-7 | 4.235 | 3.812 |
| 699 | 28.50 | 1.3424 | 848798 | 0.0046 | 6567 | 7.198E-7 | 4.321 | 3.889 |
| 711 | 28.64 | 1.3471 | 855150 | 0.0047 | 6004 | 7.953E-7 | 4.407 | 3.967 |
| 723 | 28.77 | 1.3518 | 860867 | 0.0093 | 10798 | 8.655E-7 | 4.497 | 4.047 |
| 736 | 28.91 | 1.3564 | 865948 | 0.0093 | 9654 | 9.630E-7 | 4.586 | 4.128 |
| 748 | 29.04 | 1.3611 | 870521 | 0.0461 | 73444 | 6.278E-7 | 0.000 | 0.000 |
| 869 | 30.27 | 1.4025 | 939392 | 0.0461 | 71574 | 6.442E-7 | 0.000 | 0.000 |
| 884 | 30.41 | 1.4072 | 942095 | 0.0092 | 5243 | 1.759E-6 | 5.695 | 5.126 |
| 899 | 30.55 | 1.4118 | 944635 | 0.0096 | 4953 | 1.929E-6 | 5.813 | 5.232 |
| 915 | 30.71 | 1.4167 | 947048 | 0.0097 | 4471 | 2.177E-6 | 5.930 | 5.337 |
| 931 | 30.86 | 1.4215 | 949106 | 0.0047 | 2012 | 2.411E-6 | 6.051 | 5.446 |
| 947 | 31.00 | 1.4260 | 950915 | 0.0045 | 1895 | 2.440E-6 | 6.174 | 5.557 |
| 963 | 31.15 | 1.4307 | 952622 | 0.0048 | 1772 | 2.636E-6 | 6.296 | 5.666 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^0.5) | deltaK |
|--------------|-------|-----------|--------|------------|------|-------------------|-----------------------|--------|
| 979 | 31.29 | 1.4354 | 954167 | 0.0046 | 1633 | 2.780E-6 | 6.407 | 5.766 |
| 992 | 31.40 | 1.4387 | 956007 | 0.0047 | 1548 | 2.992E-6 | 6.558 | 5.902 |
| 1014 | 31.61 | 1.4453 | 957682 | 0.0046 | 1448 | 3.295E-6 | 6.664 | 5.997 |
| 1029 | 31.73 | 1.4492 | 958902 | 0.0046 | 1345 | 3.649E-6 | 6.822 | 6.139 |
| 1047 | 31.89 | 1.4539 | 960203 | 0.0048 | 1186 | 4.096E-6 | 6.947 | 6.252 |
| 1064 | 32.04 | 1.4585 | 961309 | 0.0045 | 1046 | 4.508E-6 | 7.086 | 6.377 |
| 1082 | 32.18 | 1.4631 | 962235 | 0.0047 | 967 | 4.997E-6 | 7.225 | 6.503 |
| 1100 | 32.34 | 1.4677 | 963123 | 0.0047 | 862 | 5.526E-6 | 7.371 | 6.634 |
| 1119 | 32.49 | 1.4725 | 963956 | 0.0047 | 784 | 6.038E-6 | 7.519 | 6.767 |
| 1138 | 32.65 | 1.4772 | 964706 | 0.0047 | 729 | 6.539E-6 | 7.672 | 6.904 |
| 1158 | 32.81 | 1.4819 | 965374 | 0.0047 | 675 | 6.997E-6 | 7.824 | 7.041 |
| 1177 | 32.96 | 1.4864 | 966012 | 0.0047 | 626 | 7.472E-6 | 7.983 | 7.185 |
| 1197 | 33.12 | 1.4912 | 966610 | 0.0046 | 587 | 7.902E-6 | 8.138 | 7.324 |
| 1217 | 33.27 | 1.4957 | 967175 | 0.0046 | 555 | 8.333E-6 | 8.304 | 7.473 |
| 1238 | 33.44 | 1.5004 | 967714 | 0.0093 | 1051 | 8.826E-6 | 8.464 | 7.618 |
| 1258 | 33.59 | 1.5049 | 968226 | 0.0091 | 989 | 9.235E-6 | 8.634 | 7.771 |
| | 33.75 | 1.5095 | 968703 | | | | | |
| | 33.81 | 1.5111 | 969068 | | | | | |
| 1295 | 33.92 | 1.5145 | 969361 | 0.0079 | 742 | 1.071E-5 | 8.952 | 8.057 |
| 1304 | 34.08 | 1.5190 | 969810 | 0.0095 | 847 | 1.122E-5 | 9.030 | 8.127 |
| 1313 | 34.26 | 1.5240 | 970208 | 0.0093 | 745 | 1.245E-5 | 9.115 | 8.204 |
| 1321 | 34.41 | 1.5283 | 970555 | 0.0050 | 443 | 1.174E-5 | 9.205 | 8.285 |
| 1330 | 34.57 | 1.5329 | 970967 | 0.0058 | 497 | 1.262E-5 | 9.294 | 8.364 |
| 1339 | 34.74 | 1.5376 | 971394 | 0.0065 | 554 | 1.271E-5 | 9.407 | 8.466 |
| 1353 | 35.00 | 1.5446 | 972016 | 0.0074 | 622 | 1.253E-5 | 9.545 | 8.591 |
| 1371 | 35.34 | 1.5539 | 972793 | 0.0083 | 670 | 1.262E-5 | 9.709 | 8.738 |
| 1389 | 35.68 | 1.5633 | 973533 | 0.0090 | 707 | 1.279E-5 | 9.904 | 8.913 |
| 1408 | 36.04 | 1.5730 | 974287 | 0.0094 | 706 | 1.330E-5 | 10.099 | 9.089 |
| 1428 | 36.40 | 1.5825 | 974987 | 0.0094 | 675 | 1.391E-5 | 10.302 | 9.272 |
| 1447 | 36.76 | 1.5918 | 975634 | 0.0094 | 646 | 1.456E-5 | 10.504 | 9.454 |
| 1466 | 37.12 | 1.6010 | 976253 | 0.0093 | 611 | 1.526E-5 | 10.710 | 9.639 |
| 1485 | 37.48 | 1.6103 | 976845 | 0.0093 | 584 | 1.596E-5 | 10.919 | 9.827 |
| 1505 | 37.85 | 1.6197 | 977411 | 0.0094 | 561 | 1.669E-5 | 11.131 | 10.018 |
| 1525 | 38.22 | 1.6289 | 977950 | 0.0094 | 541 | 1.740E-5 | 11.352 | 10.217 |
| 1545 | 38.61 | 1.6384 | 978488 | 0.0094 | 521 | 1.809E-5 | 11.576 | 10.418 |
| 1566 | 39.01 | 1.6480 | 979000 | 0.0094 | 501 | 1.879E-5 | 11.810 | 10.629 |
| 1588 | 39.40 | 1.6576 | 979499 | 0.0095 | 486 | 1.953E-5 | 12.043 | 10.839 |
| 1609 | 39.80 | 1.6669 | 979968 | 0.0094 | 464 | 2.025E-5 | 12.285 | 11.057 |
| 1630 | 40.20 | 1.6763 | 980416 | 0.0094 | 445 | 2.098E-5 | 12.528 | 11.275 |
| 1652 | 40.61 | 1.6859 | 980864 | 0.0093 | 428 | 2.177E-5 | 12.770 | 11.493 |
| 1673 | 41.01 | 1.6949 | 981270 | 0.0094 | 413 | 2.263E-5 | 13.023 | 11.721 |
| 1695 | 41.42 | 1.7041 | 981669 | 0.0094 | 399 | 2.349E-5 | 13.273 | 11.946 |
| 1718 | 41.84 | 1.7135 | 982067 | 0.0094 | 382 | 2.447E-5 | 13.539 | 12.185 |
| 1741 | 42.28 | 1.7233 | 982447 | 0.0094 | 369 | 2.546E-5 | 13.804 | 12.424 |
| 1764 | 42.71 | 1.7327 | 982809 | 0.0094 | 356 | 2.649E-5 | 14.079 | 12.671 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in]^0.5) |
|--------------|-------|-----------|--------|------------|-----|-------------------|--------|-------------------------|
| 1787 | 43.15 | 1.7420 | 983155 | 0.0095 | 342 | 2.761E-5 | 14.354 | 12.919 |
| 1810 | 43.59 | 1.7513 | 983483 | 0.0094 | 329 | 2.864E-5 | 14.636 | 13.172 |
| 1834 | 44.04 | 1.7607 | 983803 | 0.0094 | 317 | 2.976E-5 | 14.926 | 13.434 |
| 1858 | 44.51 | 1.7704 | 984119 | 0.0095 | 305 | 3.094E-5 | 15.221 | 13.699 |
| 1882 | 44.97 | 1.7798 | 984421 | 0.0095 | 296 | 3.213E-5 | 15.525 | 13.973 |
| 1907 | 45.44 | 1.7893 | 984709 | 0.0096 | 286 | 3.339E-5 | 15.829 | 14.246 |
| 1931 | 45.92 | 1.7987 | 984983 | 0.0095 | 273 | 3.469E-5 | 16.146 | 14.531 |
| 1957 | 46.42 | 1.8085 | 985258 | 0.0095 | 260 | 3.654E-5 | 16.465 | 14.818 |
| 1982 | 46.91 | 1.8181 | 985518 | 0.0095 | 249 | 3.811E-5 | 16.789 | 15.110 |
| 2007 | 47.39 | 1.8272 | 985754 | 0.0095 | 241 | 3.949E-5 | 17.129 | 15.415 |
| 2034 | 47.92 | 1.8371 | 985980 | 0.0094 | 230 | 4.096E-5 | 17.453 | 15.708 |
| 2059 | 48.40 | 1.8461 | 986204 | 0.0094 | 221 | 4.256E-5 | 17.802 | 16.022 |
| 2085 | 48.92 | 1.8556 | 986427 | 0.0095 | 212 | 4.430E-5 | 18.145 | 16.331 |
| 2112 | 49.45 | 1.8651 | 986640 | 0.0094 | 203 | 4.635E-5 | 18.506 | 16.655 |
| 2139 | 49.99 | 1.8748 | 986841 | 0.0095 | 194 | 4.920E-5 | 18.867 | 16.980 |
| 2166 | 50.52 | 1.8841 | 987024 | 0.0095 | 183 | 5.209E-5 | 19.242 | 17.317 |
| 2193 | 51.06 | 1.8934 | 987199 | 0.0095 | 173 | 5.499E-5 | 19.620 | 17.658 |
| 2221 | 51.64 | 1.9032 | 987369 | 0.0094 | 163 | 5.800E-5 | 20.003 | 18.003 |
| 2249 | 52.19 | 1.9126 | 987526 | 0.0095 | 156 | 6.103E-5 | 20.395 | 18.355 |
| 2276 | 52.75 | 1.9219 | 987675 | 0.0096 | 148 | 6.442E-5 | 20.790 | 18.710 |
| 2304 | 53.33 | 1.9312 | 987817 | 0.0096 | 138 | 6.910E-5 | 21.200 | 19.080 |
| 2333 | 53.94 | 1.9412 | 987960 | 0.0095 | 130 | 7.445E-5 | 21.615 | 19.453 |
| 2363 | 54.55 | 1.9509 | 988088 | 0.0095 | 122 | 7.954E-5 | 22.055 | 19.849 |
| 2393 | 55.18 | 1.9608 | 988198 | 0.0096 | 115 | 8.411E-5 | 22.482 | 20.234 |
| 2422 | 55.76 | 1.9697 | 988303 | 0.0096 | 108 | 8.935E-5 | 22.928 | 20.635 |
| 2451 | 56.38 | 1.9792 | 988408 | 0.0190 | 206 | 9.246E-5 | 23.383 | 21.034 |
| 2483 | 57.02 | 1.9888 | 988509 | 0.0198 | 197 | 1.003E-4 | 23.848 | 21.455 |
| | 57.71 | 1.9989 | 988605 | | | | | |
| | 62.08 | 2.0637 | 989903 | | | | | |
| 2300 | 62.51 | 2.0697 | 989969 | 0.0161 | 180 | 8.943E-5 | 23.567 | 21.211 |
| 2300 | 63.23 | 2.0798 | 990083 | 0.0200 | 228 | 8.770E-5 | 23.720 | 21.348 |
| 2300 | 63.96 | 2.0897 | 990197 | 0.0203 | 229 | 8.882E-5 | 23.915 | 21.523 |
| 2300 | 64.73 | 2.1001 | 990312 | 0.0103 | 111 | 9.251E-5 | 24.114 | 21.702 |
| 2300 | 65.52 | 2.1106 | 990422 | 0.0103 | 108 | 9.529E-5 | 24.316 | 21.885 |
| 2300 | 66.30 | 2.1208 | 990527 | 0.0103 | 104 | 9.873E-5 | 24.526 | 22.073 |
| 2300 | 67.12 | 2.1313 | 990632 | 0.0102 | 100 | 1.023E-4 | 24.732 | 22.258 |
| 2300 | 67.92 | 2.1413 | 990728 | 0.0102 | 97 | 1.053E-4 | 24.942 | 22.448 |
| 2300 | 68.73 | 2.1514 | 990819 | 0.0102 | 95 | 1.083E-4 | 25.153 | 22.637 |
| 2300 | 69.56 | 2.1615 | 990911 | 0.0102 | 92 | 1.115E-4 | 25.367 | 22.831 |
| 2300 | 70.41 | 2.1717 | 991003 | 0.0102 | 89 | 1.137E-4 | 25.589 | 23.030 |
| 2300 | 71.31 | 2.1823 | 991094 | 0.0102 | 88 | 1.165E-4 | 25.814 | 23.232 |
| 2300 | 72.20 | 2.1926 | 991181 | 0.0102 | 85 | 1.195E-4 | 26.039 | 23.435 |
| 2300 | 73.06 | 2.2024 | 991263 | 0.0102 | 83 | 1.228E-4 | 26.272 | 23.644 |
| 2300 | 73.99 | 2.2128 | 991344 | 0.0101 | 80 | 1.262E-4 | 26.494 | 23.845 |
| 2300 | 74.88 | 2.2226 | 991421 | 0.0101 | 78 | 1.296E-4 | 26.732 | 24.059 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^0.5) | deltaK |
|--------------|--------|-----------|--------|------------|----|-------------------|-----------------------|----------|
| 2300 | 75.81 | 2.2327 | 991498 | 0.0102 | 76 | 1.333E-4 | 26.968 | 24.271 |
| 2300 | 76.79 | 2.2431 | 991574 | 0.0102 | 74 | 1.371E-4 | 27.209 | 24.488 |
| 2300 | 77.75 | 2.2532 | 991647 | 0.0103 | 73 | 1.412E-4 | 27.461 | 24.715 |
| 2300 | 78.77 | 2.2636 | 991720 | 0.0103 | 71 | 1.451E-4 | 27.714 | 24.943 |
| 2300 | 79.82 | 2.2741 | 991790 | 0.0102 | 68 | 1.499E-4 | 27.975 | 25.177 |
| 2300 | 80.86 | 2.2845 | 991858 | 0.0103 | 66 | 1.555E-4 | 28.232 | 25.409 |
| 2300 | 81.87 | 2.2943 | 991921 | 0.0103 | 63 | 1.625E-4 | 28.498 | 25.648 |
| 2300 | 82.95 | 2.3046 | 991983 | 0.0102 | 60 | 1.711E-4 | 28.764 | 25.887 |
| 2300 | 84.07 | 2.3150 | 992043 | 0.0102 | 56 | 1.819E-4 | 29.042 | 26.137 |
| 2300 | 85.23 | 2.3256 | 992099 | 0.0103 | 54 | 1.915E-4 | 29.316 | 26.384 |
| 2300 | 86.32 | 2.3354 | 992148 | 0.0103 | 52 | 1.985E-4 | 29.603 | 26.642 |
| 2300 | 87.48 | 2.3457 | 992196 | 0.0102 | 50 | 2.053E-4 | 29.885 | 26.896 |
| 2300 | 88.66 | 2.3560 | 992246 | 0.0101 | 48 | 2.112E-4 | 30.177 | 27.159 |
| 2300 | 89.88 | 2.3663 | 992296 | 0.0103 | 47 | 2.178E-4 | 30.472 | 27.424 |
| 2300 | 91.09 | 2.3764 | 992341 | 0.0104 | 46 | 2.260E-4 | 30.768 | 27.690 |
| 2300 | 92.29 | 2.3862 | 992384 | 0.0102 | 43 | 2.364E-4 | 31.079 | 27.970 |
| 2300 | 93.62 | 2.3969 | 992428 | 0.0102 | 41 | 2.491E-4 | 31.393 | 28.253 |
| 2300 | 95.00 | 2.4078 | 992470 | 0.0103 | 39 | 2.619E-4 | 31.708 | 28.536 |
| 2300 | 96.25 | 2.4174 | 992506 | 0.0104 | 38 | 2.750E-4 | 32.039 | 28.834 |
| 2300 | 97.60 | 2.4276 | 992542 | 0.0102 | 35 | 2.921E-4 | 32.359 | 29.122 |
| 2300 | 99.00 | 2.4380 | 992577 | 0.0102 | 33 | 3.111E-4 | 32.695 | 29.424 |
| 2300 | 100.44 | 2.4484 | 992610 | 0.0103 | 32 | 3.278E-4 | 33.032 | 29.728 |
| 2300 | 101.85 | 2.4584 | 992638 | 0.0102 | 30 | 3.413E-4 | 33.385 | 30.045 |
| 2300 | 103.35 | 2.4689 | 992667 | 0.0102 | 28 | 3.582E-4 | 33.732 | 30.358 |
| 2300 | 104.84 | 2.4791 | 992696 | 0.0103 | 27 | 3.798E-4 | 34.090 | 30.679 |
| 2300 | 106.34 | 2.4891 | 992723 | 0.0103 | 26 | 4.040E-4 | 34.451 | 31.004 |
| 2300 | 107.88 | 2.4992 | 992747 | 0.0103 | 24 | 4.307E-4 | 34.827 | 31.342 |
| 2300 | 109.57 | 2.5099 | 992770 | 0.0103 | 23 | 4.583E-4 | 35.198 | 31.675 |
| 2300 | 111.17 | 2.5200 | 992791 | 0.0102 | 21 | 4.833E-4 | 35.598 | 32.035 |
| 2300 | 112.87 | 2.5304 | 992812 | 0.0102 | 20 | 5.081E-4 | 35.993 | 32.391 |
| 2300 | 114.65 | 2.5411 | 992833 | 0.0101 | 19 | 5.425E-4 | 36.380 | 32.738 |
| 2300 | 116.24 | 2.5504 | 992850 | 0.0102 | 17 | 5.912E-4 | 36.792 | 33.109 * |
| 2300 | 118.00 | 2.5605 | 992867 | 0.0102 | 16 | 6.549E-4 | 37.185 | 33.462 * |
| 2300 | 119.79 | 2.5706 | 992882 | 0.0101 | 15 | 7.173E-4 | 37.605 | 33.839 * |
| 2300 | 121.68 | 2.5810 | 992895 | 0.0103 | 14 | 7.773E-4 | 38.046 | 34.234 * |
| 2300 | 123.68 | 2.5917 | 992908 | 0.0103 | 12 | 8.570E-4 | 38.480 | 34.624 * |
| 2300 | 125.60 | 2.6018 | 992920 | 0.0110 | 11 | 9.696E-4 | 38.939 | 35.036 * |
| 2299 | 127.61 | 2.6121 | 992931 | 0.0103 | 10 | 1.050E-3 | 39.397 | 35.445 * |
| 2300 | 129.68 | 2.6225 | 992940 | 0.0103 | 10 | 1.095E-3 | 39.952 | 35.945 * |
| 2300 | 132.57 | 2.6365 | 992950 | 0.0104 | 9 | 1.148E-3 | 40.343 | 36.297 * |
| 2300 | 133.91 | 2.6429 | 992957 | 0.0103 | 9 | 1.192E-3 | 40.923 | 36.819 * |
| 2300 | 136.13 | 2.6533 | 992966 | 0.0103 | 8 | 1.231E-3 | 41.343 | 37.198 * |
| 2300 | 138.55 | 2.6643 | 992975 | 0.0098 | 8 | 1.335E-3 | 41.833 | 37.637 * |
| 2299 | 140.76 | 2.6741 | 992982 | 0.0106 | 7 | 1.517E-3 | 42.371 | 38.119 * |
| 2299 | 143.17 | 2.6846 | 992989 | 0.0097 | 7 | 1.586E-3 | 42.889 | 38.579 * |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^0.5) | deltaK |
|--------------|--------|-----------|--------|------------|----|-------------------|-----------------------|----------|
| 2298 | 145.73 | 2.6954 | 992995 | 0.0103 | 6 | 1.764E-3 | 43.453 | 39.082 * |
| 2298 | 148.40 | 2.7064 | 993000 | 0.0129 | 5 | 2.440E-3 | 43.865 | 39.448 * |
| 2298 | 149.67 | 2.7116 | 993005 | 0.0101 | 4 | 2.800E-3 | 44.542 | 40.046 * |
| 2296 | 153.30 | 2.7259 | 993010 | 0.0403 | 8 | 5.033E-3 | 45.401 | 40.818 * |
| 2295 | 160.22 | 2.7518 | 993013 | 0.0195 | 5 | 3.904E-3 | 45.568 | 40.951 * |
| | 158.47 | 2.7454 | 993015 | | | | | |

Automated Fatigue Crack
Growth Rate Analysis

| | | | |
|-----------------|--------------|---------------|------|
| Test ID | 5083-FCG-45 | Geometry | C(T) |
| Contract | SSC 10624-01 | Orientation | T-L |
| Material | 5083-H321 | Yield (ksi) | 34.3 |
| Temperature (F) | 75 | Modulus (Msi) | 10.5 |
| Environment | Sea Water | | |

Specimen Dimensions (in)

| | | | |
|---------------|-------|-------------|-------|
| Thickness | 0.499 | Height | 2.400 |
| Net Thickness | 0.499 | Notch Depth | 1.000 |
| Width | 4.000 | Gage Length | 0.500 |

Precrack Parameters

| | | | |
|--------------|-------|--------------------|------|
| Pmax (lbs) | 784.0 | Stress Ratio | 0.10 |
| Final a (in) | 1.050 | Kmax (ksi sqr[in]) | 4.00 |

Test Parameters

| EvBP | Freq | Pmax | R | Ai | Kmaxi | C | DKi |
|--------|------|------|------|-------|-------|------|------|
| 24.522 | 5.00 | 0 | 0.10 | 1.195 | 2.70 | 4.00 | 0.00 |
| 32.544 | 5.00 | 0 | 0.10 | 1.491 | 8.80 | 2.00 | 0.00 |
| 55.204 | 5.00 | 2450 | 0.10 | 0.000 | 0.00 | 0.00 | 0.00 |

| K Coeff | C Coeff |
|---------|----------|
| .886 | 1.00098 |
| 4.64 | -4.66951 |
| -13.32 | 18.4601 |
| 14.72 | -236.825 |
| -5.6 | 1214.88 |
| . | -2143.57 |

Visual Observations

| EvB/P | Crack(EvB/P) | Crack(visual) | Error | CAF |
|--------|--------------|---------------|--------|-------|
| 20.869 | 1.012 | 1.000 | -0.012 | 1.013 |
| 21.842 | 1.062 | 1.065 | 0.003 | 1.010 |
| 23.217 | 1.127 | 1.125 | -0.002 | 1.006 |
| 24.253 | 1.174 | 1.170 | -0.004 | 1.004 |
| 24.439 | 1.182 | 1.195 | 0.013 | 1.003 |
| 28.306 | 1.335 | 1.350 | 0.015 | 0.995 |
| 32.493 | 1.475 | 1.480 | 0.005 | 0.987 |
| 34.530 | 1.535 | 1.530 | -0.005 | 0.984 |
| 36.488 | 1.589 | 1.580 | -0.009 | 0.982 |
| 46.151 | 1.812 | 1.805 | -0.007 | 0.970 |
| 54.785 | 1.965 | 1.955 | -0.010 | 0.962 |
| 72.549 | 2.199 | 2.210 | 0.011 | 0.951 |

Comments

Date of test: 9/10/2006
Waveform Type Sine

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in]^0.5) |
|--------------|-------|-----------|---------|------------|--------|-------------------|-------|-------------------------|
| | 24.52 | 1.1852 | 52230 | | | | | |
| 449 | 24.60 | 1.1888 | 140390 | 0.0079 | 158059 | 5.019E-8 | 2.513 | 2.262 |
| 456 | 24.71 | 1.1932 | 210289 | 0.0078 | 151828 | 5.159E-8 | 2.550 | 2.295 |
| 461 | 24.79 | 1.1966 | 292218 | 0.0040 | 74574 | 5.363E-8 | 2.649 | 2.384 |
| 487 | 24.90 | 1.2012 | 372041 | 0.0043 | 67562 | 6.198E-8 | 2.689 | 2.420 |
| 493 | 24.98 | 1.2047 | 425966 | 0.0044 | 64350 | 7.006E-8 | 2.790 | 2.511 |
| 501 | 25.08 | 1.2090 | 499674 | 0.0044 | 59975 | 7.804E-8 | 2.842 | 2.558 |
| 510 | 25.21 | 1.2143 | 545760 | 0.0045 | 53716 | 8.544E-8 | 2.899 | 2.609 |
| 519 | 25.33 | 1.2194 | 596390 | 0.0048 | 50101 | 9.771E-8 | 2.953 | 2.658 |
| 526 | 25.42 | 1.2230 | 652069 | 0.0049 | 41088 | 1.205E-7 | 3.019 | 2.717 |
| 536 | 25.55 | 1.2284 | 694335 | 0.0048 | 36412 | 1.578E-7 | 3.073 | 2.766 |
| 545 | 25.68 | 1.2336 | 726571 | 0.0047 | 30946 | 2.041E-7 | 3.140 | 2.826 |
| 555 | 25.79 | 1.2384 | 746204 | 0.0049 | 24251 | 2.327E-7 | 3.203 | 2.882 |
| 564 | 25.91 | 1.2429 | 764234 | 0.0048 | 19921 | 2.538E-7 | 3.268 | 2.941 |
| 573 | 26.02 | 1.2476 | 782068 | 0.0047 | 17651 | 2.683E-7 | 3.332 | 2.998 |
| 583 | 26.14 | 1.2523 | 797577 | 0.0047 | 17687 | 2.705E-7 | 3.399 | 3.059 |
| 593 | 26.26 | 1.2570 | 813862 | 0.0047 | 17862 | 2.701E-7 | 3.466 | 3.120 |
| 603 | 26.38 | 1.2617 | 832474 | 0.0047 | 17733 | 2.645E-7 | 3.537 | 3.183 |
| 613 | 26.49 | 1.2664 | 852328 | 0.0047 | 17862 | 2.595E-7 | 3.607 | 3.247 |
| 624 | 26.62 | 1.2712 | 871405 | 0.0048 | 17603 | 2.711E-7 | 3.679 | 3.311 |
| 634 | 26.74 | 1.2760 | 888464 | 0.0048 | 16595 | 2.920E-7 | 3.754 | 3.378 |
| 645 | 26.86 | 1.2807 | 904747 | 0.0048 | 14878 | 3.297E-7 | 3.831 | 3.448 |
| 657 | 27.00 | 1.2859 | 919480 | 0.0047 | 13156 | 3.783E-7 | 3.906 | 3.516 |
| 668 | 27.11 | 1.2903 | 932043 | 0.0048 | 11769 | 4.365E-7 | 3.987 | 3.588 |
| 679 | 27.24 | 1.2950 | 941598 | 0.0048 | 10314 | 4.900E-7 | 4.064 | 3.658 |
| 690 | 27.35 | 1.2995 | 950338 | 0.0047 | 8984 | 5.469E-7 | 4.148 | 3.733 |
| 702 | 27.49 | 1.3046 | 959080 | 0.0047 | 7895 | 6.074E-7 | 4.229 | 3.806 |
| 714 | 27.61 | 1.3093 | 966630 | 0.0047 | 7245 | 6.672E-7 | 4.317 | 3.886 |
| 726 | 27.74 | 1.3141 | 973381 | 0.0048 | 6678 | 7.367E-7 | 4.400 | 3.960 |
| 738 | 27.86 | 1.3185 | 979415 | 0.0047 | 5941 | 8.173E-7 | 4.491 | 4.042 |
| 751 | 27.99 | 1.3234 | 985069 | 0.0099 | 10989 | 9.020E-7 | 4.580 | 4.122 |
| 764 | 28.13 | 1.3284 | 990404 | 0.0097 | 9654 | 1.004E-6 | 4.673 | 4.205 |
| 777 | 28.26 | 1.3331 | 994723 | 0.0654 | 39796 | 1.643E-6 | 0.000 | 0.000 |
| 965 | 29.99 | 1.3938 | 1030200 | 0.0653 | 37065 | 1.762E-6 | 0.000 | 0.000 |
| 981 | 30.12 | 1.3984 | 1031788 | 0.0096 | 3071 | 3.115E-6 | 6.281 | 5.653 |
| 998 | 30.27 | 1.4034 | 1033271 | 0.0097 | 2763 | 3.526E-6 | 6.404 | 5.764 |
| 1015 | 30.41 | 1.4081 | 1034551 | 0.0096 | 2475 | 3.864E-6 | 6.535 | 5.881 |
| 1032 | 30.56 | 1.4129 | 1035746 | 0.0048 | 1183 | 4.122E-6 | 6.665 | 5.999 |
| 1049 | 30.70 | 1.4177 | 1036891 | 0.0048 | 1077 | 4.458E-6 | 6.800 | 6.120 |
| 1067 | 30.85 | 1.4225 | 1037937 | 0.0047 | 998 | 4.806E-6 | 6.936 | 6.243 |
| 1085 | 31.00 | 1.4273 | 1038883 | 0.0047 | 925 | 5.201E-6 | 7.074 | 6.366 |
| 1103 | 31.14 | 1.4319 | 1039733 | 0.0047 | 854 | 5.608E-6 | 7.214 | 6.492 |
| 1121 | 31.28 | 1.4365 | 1040536 | 0.0048 | 797 | 6.010E-6 | 7.358 | 6.622 |
| 1141 | 31.43 | 1.4414 | 1041298 | 0.0048 | 751 | 6.399E-6 | 7.504 | 6.754 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^-.5) | deltaK |
|--------------|-------|-----------|---------|------------|------|-------------------|-----------------------|--------|
| 1160 | 31.58 | 1.4461 | 1042012 | 0.0048 | 711 | 6.782E-6 | 7.658 | 6.892 |
| 1181 | 31.73 | 1.4510 | 1042716 | 0.0048 | 667 | 7.198E-6 | 7.816 | 7.034 |
| 1201 | 31.89 | 1.4560 | 1043388 | 0.0048 | 625 | 7.655E-6 | 7.974 | 7.177 |
| 1221 | 32.04 | 1.4607 | 1043997 | 0.0048 | 591 | 8.173E-6 | 8.135 | 7.322 |
| 1242 | 32.19 | 1.4653 | 1044539 | 0.0092 | 1050 | 8.788E-6 | 8.295 | 7.465 |
| 1262 | 32.34 | 1.4699 | 1045047 | 0.0095 | 1016 | 9.359E-6 | 8.462 | 7.616 |
| | 32.50 | 1.4748 | 1045555 | | | | | |
| | 36.74 | 1.5959 | 1054252 | | | | | |
| 1551 | 37.09 | 1.6053 | 1054821 | 0.0191 | 1138 | 1.676E-5 | 11.357 | 10.222 |
| 1572 | 37.47 | 1.6150 | 1055390 | 0.0193 | 1120 | 1.723E-5 | 11.581 | 10.423 |
| 1593 | 37.84 | 1.6246 | 1055941 | 0.0192 | 1078 | 1.784E-5 | 11.811 | 10.630 |
| 1614 | 38.22 | 1.6342 | 1056468 | 0.0096 | 511 | 1.886E-5 | 12.047 | 10.842 |
| 1636 | 38.61 | 1.6440 | 1056972 | 0.0097 | 491 | 1.974E-5 | 12.286 | 11.058 |
| 1658 | 39.00 | 1.6536 | 1057440 | 0.0097 | 470 | 2.066E-5 | 12.531 | 11.278 |
| 1680 | 39.39 | 1.6632 | 1057887 | 0.0096 | 447 | 2.154E-5 | 12.783 | 11.505 |
| 1702 | 39.79 | 1.6729 | 1058334 | 0.0096 | 426 | 2.247E-5 | 13.040 | 11.736 |
| 1726 | 40.21 | 1.6828 | 1058761 | 0.0096 | 410 | 2.338E-5 | 13.296 | 11.967 |
| 1748 | 40.60 | 1.6920 | 1059147 | 0.0096 | 395 | 2.431E-5 | 13.564 | 12.208 |
| 1771 | 41.01 | 1.7015 | 1059525 | 0.0096 | 377 | 2.536E-5 | 13.829 | 12.446 |
| 1795 | 41.43 | 1.7112 | 1059899 | 0.0095 | 360 | 2.644E-5 | 14.105 | 12.695 |
| 1818 | 41.85 | 1.7208 | 1060257 | 0.0096 | 348 | 2.751E-5 | 14.387 | 12.948 |
| 1842 | 42.29 | 1.7305 | 1060598 | 0.0096 | 334 | 2.861E-5 | 14.673 | 13.205 |
| 1867 | 42.72 | 1.7400 | 1060923 | 0.0096 | 321 | 2.978E-5 | 14.962 | 13.466 |
| 1891 | 43.15 | 1.7495 | 1061233 | 0.0095 | 308 | 3.092E-5 | 15.257 | 13.731 |
| 1915 | 43.59 | 1.7589 | 1061531 | 0.0095 | 295 | 3.213E-5 | 15.558 | 14.002 |
| 1941 | 44.04 | 1.7686 | 1061824 | 0.0095 | 284 | 3.351E-5 | 15.863 | 14.277 |
| 1965 | 44.49 | 1.7780 | 1062103 | 0.0096 | 274 | 3.493E-5 | 16.178 | 14.560 |
| 1991 | 44.96 | 1.7876 | 1062370 | 0.0097 | 263 | 3.667E-5 | 16.495 | 14.846 |
| 2017 | 45.43 | 1.7972 | 1062624 | 0.0096 | 250 | 3.845E-5 | 16.825 | 15.142 |
| 2043 | 45.92 | 1.8070 | 1062878 | 0.0097 | 239 | 4.048E-5 | 17.163 | 15.447 |
| 2070 | 46.42 | 1.8170 | 1063109 | 0.0097 | 228 | 4.247E-5 | 17.501 | 15.751 |
| 2096 | 46.88 | 1.8262 | 1063323 | 0.0097 | 218 | 4.451E-5 | 17.855 | 16.070 |
| 2123 | 47.39 | 1.8360 | 1063536 | 0.0096 | 205 | 4.688E-5 | 18.205 | 16.385 |
| 2151 | 47.90 | 1.8457 | 1063739 | 0.0096 | 195 | 4.923E-5 | 18.571 | 16.713 |
| 2179 | 48.42 | 1.8554 | 1063933 | 0.0097 | 187 | 5.189E-5 | 18.936 | 17.042 |
| 2206 | 48.92 | 1.8648 | 1064105 | 0.0097 | 178 | 5.451E-5 | 19.312 | 17.380 |
| 2234 | 49.44 | 1.8743 | 1064276 | 0.0097 | 168 | 5.746E-5 | 19.697 | 17.727 |
| 2263 | 50.00 | 1.8844 | 1064447 | 0.0097 | 159 | 6.082E-5 | 20.085 | 18.076 |
| 2292 | 50.54 | 1.8940 | 1064601 | 0.0097 | 151 | 6.422E-5 | 20.492 | 18.442 |
| 2321 | 51.09 | 1.9036 | 1064747 | 0.0096 | 143 | 6.794E-5 | 20.899 | 18.809 |
| 2350 | 51.65 | 1.9134 | 1064886 | 0.0096 | 134 | 7.192E-5 | 21.307 | 19.176 |
| 2379 | 52.20 | 1.9228 | 1065011 | 0.0096 | 127 | 7.592E-5 | 21.727 | 19.554 |
| 2408 | 52.76 | 1.9322 | 1065132 | 0.0096 | 119 | 8.071E-5 | 22.150 | 19.935 |
| 2438 | 53.34 | 1.9419 | 1065250 | 0.0195 | 230 | 8.487E-5 | 22.586 | 20.327 |
| 2469 | 53.94 | 1.9517 | 1065362 | 0.0196 | 212 | 9.237E-5 | 23.035 | 20.731 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in]^0.5) |
|--------------|--------|-----------|---------|------------|-----|-------------------|--------|-------------------------|
| | 54.55 | 1.9615 | 1065462 | | | | | |
| | 55.20 | 1.9719 | 1065576 | | | | | |
| 2450 | 55.75 | 1.9804 | 1065678 | 0.0181 | 212 | 8.538E-5 | 23.373 | 21.036 |
| 2450 | 56.37 | 1.9900 | 1065788 | 0.0195 | 220 | 8.858E-5 | 23.537 | 21.183 |
| 2450 | 57.02 | 1.9999 | 1065898 | 0.0196 | 216 | 9.059E-5 | 23.712 | 21.341 |
| 2450 | 57.66 | 2.0096 | 1066004 | 0.0097 | 104 | 9.258E-5 | 23.891 | 21.502 |
| 2450 | 58.32 | 2.0192 | 1066105 | 0.0098 | 102 | 9.495E-5 | 24.071 | 21.664 |
| 2450 | 58.98 | 2.0289 | 1066207 | 0.0098 | 100 | 9.728E-5 | 24.253 | 21.827 |
| 2450 | 59.65 | 2.0385 | 1066304 | 0.0098 | 98 | 9.924E-5 | 24.440 | 21.996 |
| 2450 | 60.36 | 2.0486 | 1066402 | 0.0098 | 96 | 1.011E-4 | 24.629 | 22.166 |
| 2450 | 61.08 | 2.0585 | 1066500 | 0.0098 | 94 | 1.034E-4 | 24.822 | 22.339 |
| 2450 | 61.79 | 2.0681 | 1066593 | 0.0098 | 92 | 1.055E-4 | 25.015 | 22.514 |
| 2450 | 62.50 | 2.0778 | 1066683 | 0.0097 | 90 | 1.079E-4 | 25.212 | 22.690 |
| 2450 | 63.25 | 2.0877 | 1066772 | 0.0097 | 87 | 1.107E-4 | 25.408 | 22.867 |
| 2450 | 63.99 | 2.0973 | 1066858 | 0.0097 | 85 | 1.137E-4 | 25.610 | 23.049 |
| 2450 | 64.74 | 2.1070 | 1066943 | 0.0097 | 83 | 1.165E-4 | 25.812 | 23.230 |
| 2450 | 65.51 | 2.1167 | 1067024 | 0.0097 | 81 | 1.197E-4 | 26.018 | 23.416 |
| 2450 | 66.29 | 2.1265 | 1067104 | 0.0098 | 79 | 1.238E-4 | 26.225 | 23.602 |
| 2450 | 67.08 | 2.1361 | 1067182 | 0.0097 | 76 | 1.281E-4 | 26.438 | 23.794 |
| 2450 | 67.89 | 2.1459 | 1067256 | 0.0097 | 73 | 1.322E-4 | 26.656 | 23.990 |
| 2450 | 68.75 | 2.1561 | 1067331 | 0.0097 | 71 | 1.366E-4 | 26.872 | 24.184 |
| 2450 | 69.56 | 2.1655 | 1067398 | 0.0098 | 69 | 1.411E-4 | 27.094 | 24.384 |
| 2450 | 70.38 | 2.1749 | 1067464 | 0.0091 | 63 | 1.456E-4 | 27.315 | 24.583 |
| 2450 | 71.25 | 2.1847 | 1067531 | 0.0077 | 52 | 1.517E-4 | 27.542 | 24.787 |
| 2450 | 72.16 | 2.1948 | 1067596 | 0.0064 | 42 | 1.433E-4 | 27.628 | 24.765 |
| 2432 | 72.69 | 2.2007 | 1067632 | 0.0052 | 33 | 1.401E-4 | 27.847 | 25.045 |
| 2447 | 72.82 | 2.2021 | 1067640 | 0.0034 | 20 | 1.711E-4 | 27.859 | 24.971 |
| 2450 | 72.99 | 2.2041 | 1067652 | 0.0040 | 24 | 1.647E-4 | 27.983 | 25.168 |
| 2450 | 73.17 | 2.2061 | 1067664 | 0.1146 | 509 | 2.252E-4 | 0.000 | 0.000 |
| 2450 | 84.23 | 2.3187 | 1068161 | 0.1216 | 527 | 2.308E-4 | 0.000 | 0.000 |
| 2450 | 85.21 | 2.3277 | 1068191 | 0.0190 | 63 | 3.015E-4 | 31.301 | 28.170 |
| 2450 | 86.33 | 2.3377 | 1068224 | 0.0200 | 66 | 3.035E-4 | 31.578 | 28.419 |
| 2450 | 87.46 | 2.3477 | 1068257 | 0.0202 | 64 | 3.159E-4 | 31.880 | 28.692 |
| 2450 | 88.64 | 2.3579 | 1068288 | 0.0102 | 32 | 3.212E-4 | 32.195 | 28.975 |
| 2450 | 89.91 | 2.3687 | 1068321 | 0.0102 | 31 | 3.315E-4 | 32.510 | 29.258 |
| 2450 | 91.13 | 2.3788 | 1068352 | 0.0102 | 29 | 3.460E-4 | 32.834 | 29.549 |
| 2450 | 92.34 | 2.3887 | 1068380 | 0.0102 | 28 | 3.601E-4 | 33.155 | 29.838 |
| 2450 | 93.58 | 2.3987 | 1068407 | 0.0101 | 27 | 3.769E-4 | 33.479 | 30.129 |
| 2450 | 94.87 | 2.4088 | 1068432 | 0.0102 | 26 | 3.933E-4 | 33.815 | 30.431 |
| 2450 | 96.21 | 2.4191 | 1068458 | 0.0103 | 25 | 4.114E-4 | 34.159 | 30.740 |
| 2450 | 97.59 | 2.4295 | 1068483 | 0.0103 | 24 | 4.328E-4 | 34.511 | 31.057 |
| 2450 | 98.98 | 2.4398 | 1068507 | 0.0104 | 23 | 4.614E-4 | 34.876 | 31.385 |
| 2450 | 100.44 | 2.4503 | 1068529 | 0.0103 | 22 | 4.854E-4 | 35.240 | 31.712 |
| 2450 | 101.88 | 2.4606 | 1068549 | 0.0103 | 21 | 5.071E-4 | 35.622 | 32.055 |
| 2449 | 103.43 | 2.4713 | 1068568 | 0.0104 | 19 | 5.334E-4 | 35.986 | 32.383 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in] ^{0.5}) | deltaK |
|--------------|--------|-----------|---------|------------|----|-------------------|-----------------------------------|----------|
| 2450 | 104.83 | 2.4808 | 1068587 | 0.0102 | 18 | 5.626E-4 | 36.381 | 32.737 |
| 2449 | 106.40 | 2.4914 | 1068606 | 0.0102 | 17 | 5.999E-4 | 36.767 | 33.084 |
| 2449 | 108.05 | 2.5021 | 1068623 | 0.0101 | 16 | 6.495E-4 | 37.156 | 33.433 |
| 2449 | 109.57 | 2.5118 | 1068637 | 0.0102 | 15 | 6.934E-4 | 37.564 | 33.799 * |
| 2449 | 111.16 | 2.5217 | 1068651 | 0.0103 | 14 | 7.435E-4 | 37.966 | 34.160 * |
| 2449 | 112.86 | 2.5321 | 1068664 | 0.0101 | 13 | 7.969E-4 | 38.375 | 34.527 * |
| 2449 | 114.54 | 2.5422 | 1068677 | 0.0102 | 12 | 8.574E-4 | 38.809 | 34.914 * |
| 2448 | 116.36 | 2.5529 | 1068689 | 0.0103 | 11 | 9.184E-4 | 39.234 | 35.295 * |
| 2448 | 118.10 | 2.5628 | 1068699 | 0.0105 | 11 | 9.759E-4 | 39.681 | 35.693 * |
| 2448 | 119.92 | 2.5730 | 1068709 | 0.0102 | 10 | 1.028E-3 | 40.130 | 36.096 * |
| 2448 | 121.83 | 2.5835 | 1068719 | 0.0102 | 9 | 1.086E-3 | 40.593 | 36.501 * |
| 2448 | 123.98 | 2.5950 | 1068729 | 0.0103 | 9 | 1.169E-3 | 41.037 | 36.905 * |
| 2446 | 125.61 | 2.6035 | 1068737 | 0.0103 | 8 | 1.254E-3 | 41.538 | 37.342 * |
| 2447 | 127.69 | 2.6141 | 1068745 | 0.0102 | 8 | 1.331E-3 | 41.993 | 37.753 * |
| 2446 | 129.80 | 2.6247 | 1068752 | 0.0101 | 7 | 1.450E-3 | 42.514 | 38.220 * |
| 2446 | 131.94 | 2.6351 | 1068759 | 0.0104 | 7 | 1.608E-3 | 42.992 | 38.638 * |
| 2444 | 134.01 | 2.6450 | 1068766 | 0.0103 | 6 | 1.765E-3 | 43.511 | 39.096 * |
| 2443 | 136.26 | 2.6555 | 1068771 | 0.0104 | 6 | 1.944E-3 | 44.021 | 39.546 * |
| 2443 | 138.60 | 2.6661 | 1068776 | 0.0106 | 5 | 2.272E-3 | 44.531 | 39.986 * |
| 2441 | 140.87 | 2.6761 | 1068781 | 0.0107 | 4 | 2.669E-3 | 45.043 | 40.424 * |
| 2434 | 143.35 | 2.6868 | 1068785 | 0.0105 | 4 | 3.189E-3 | 45.532 | 40.821 * |
| 2425 | 146.13 | 2.6985 | 1068788 | 0.0222 | 6 | 3.695E-3 | 46.002 | 41.185 * |
| 2419 | 148.68 | 2.7090 | 1068791 | 0.0200 | 5 | 3.994E-3 | 46.399 | 41.471 * |
| | 151.06 | 2.7185 | 1068793 | | | | | |

Automated Fatigue Crack
Growth Rate Analysis

| | | | |
|-----------------|---------------|---------------|------|
| Test ID | 5083-FCG-4pt5 | Geometry | C(T) |
| Contract | SSC 10624-01 | Orientation | T-L |
| Material | 5083-H321 | Yield (ksi) | 34.3 |
| Temperature (F) | 75 | Modulus (Msi) | 10.5 |
| Environment | Sea Water | | |

Specimen Dimensions (in)

| | | | |
|---------------|-------|-------------|-------|
| Thickness | 0.499 | Height | 2.400 |
| Net Thickness | 0.499 | Notch Depth | 1.000 |
| Width | 4.000 | Gage Length | 0.500 |

Precrack Parameters

| | | | |
|--------------|-------|--------------------|------|
| Pmax (lbs) | 784.0 | Stress Ratio | 0.10 |
| Final a (in) | 1.050 | Kmax (ksi sqr[in]) | 4.00 |

Test Parameters

| EvBP | Freq | Pmax | R | Ai | Kmaxi | C | DKi |
|--------|------|------|------|-------|-------|------|------|
| 24.520 | 0.50 | 0 | 0.10 | 1.195 | 2.70 | 4.00 | 0.00 |
| 32.540 | 0.50 | 0 | 0.10 | 1.491 | 8.80 | 2.00 | 0.00 |
| 55.204 | 0.50 | 2450 | 0.10 | 0.000 | 0.00 | 0.00 | 0.00 |

| K Coeff | C Coeff |
|---------|----------|
| .886 | 1.00098 |
| 4.64 | -4.66951 |
| -13.32 | 18.4601 |
| 14.72 | -236.825 |
| -5.6 | 1214.88 |
| . | -2143.57 |

Visual Observations

| EvB/P | Crack(EvB/P) | Crack(visual) | Error | CAF |
|--------|--------------|---------------|--------|-------|
| 20.869 | 1.012 | 1.000 | -0.012 | 1.013 |
| 21.842 | 1.062 | 1.065 | 0.003 | 1.010 |
| 23.217 | 1.127 | 1.125 | -0.002 | 1.006 |
| 24.253 | 1.174 | 1.170 | -0.004 | 1.004 |
| 24.439 | 1.182 | 1.195 | 0.013 | 1.003 |
| 28.306 | 1.335 | 1.350 | 0.015 | 0.995 |
| 32.493 | 1.475 | 1.480 | 0.005 | 0.987 |
| 34.530 | 1.535 | 1.530 | -0.005 | 0.984 |
| 36.488 | 1.589 | 1.580 | -0.009 | 0.982 |
| 46.151 | 1.812 | 1.805 | -0.007 | 0.970 |
| 54.785 | 1.965 | 1.955 | -0.010 | 0.962 |
| 72.549 | 2.199 | 2.210 | 0.011 | 0.951 |

Comments

Date of test: 9/10/2006

Waveform Type

Sine

Test ID 5083-FCG-4pt5

Page 1

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^0.5) | deltaK |
|--------------|-------|-----------|---------|------------|-------|-------------------|-----------------------|--------|
| | 28.48 | 1.3413 | 998455 | | | | | |
| 806 | 28.53 | 1.3430 | 1000171 | 0.0037 | 3556 | 1.051E-6 | 4.981 | 4.483 |
| 812 | 28.59 | 1.3450 | 1002011 | 0.0038 | 3513 | 1.088E-6 | 5.019 | 4.517 |
| 817 | 28.64 | 1.3469 | 1003684 | 0.0019 | 1632 | 1.178E-6 | 5.061 | 4.555 |
| 823 | 28.70 | 1.3489 | 1005309 | 0.0019 | 1565 | 1.241E-6 | 5.101 | 4.591 |
| 829 | 28.75 | 1.3508 | 1006809 | 0.0019 | 1477 | 1.294E-6 | 5.143 | 4.629 |
| 834 | 28.81 | 1.3528 | 1008246 | 0.0019 | 1427 | 1.338E-6 | 5.184 | 4.665 |
| 840 | 28.86 | 1.3546 | 1009559 | 0.0019 | 1375 | 1.371E-6 | 5.224 | 4.702 |
| 845 | 28.91 | 1.3564 | 1010871 | 0.0019 | 1344 | 1.398E-6 | 5.266 | 4.739 |
| 851 | 28.96 | 1.3583 | 1012246 | 0.0019 | 1313 | 1.438E-6 | 5.307 | 4.776 |
| 857 | 29.02 | 1.3603 | 1013559 | 0.0019 | 1270 | 1.487E-6 | 5.349 | 4.814 |
| 862 | 29.07 | 1.3621 | 1014871 | 0.0019 | 1226 | 1.549E-6 | 5.394 | 4.854 |
| 869 | 29.13 | 1.3642 | 1016121 | 0.0019 | 1171 | 1.629E-6 | 5.436 | 4.892 |
| 874 | 29.18 | 1.3660 | 1017181 | 0.0019 | 1127 | 1.674E-6 | 5.480 | 4.932 |
| 880 | 29.23 | 1.3678 | 1018227 | 0.0019 | 1082 | 1.750E-6 | 5.523 | 4.971 |
| 886 | 29.29 | 1.3697 | 1019273 | 0.0019 | 1040 | 1.798E-6 | 5.564 | 5.008 |
| 891 | 29.34 | 1.3715 | 1020318 | 0.0019 | 1013 | 1.861E-6 | 5.612 | 5.050 |
| 898 | 29.40 | 1.3736 | 1021364 | 0.0019 | 978 | 1.934E-6 | 5.654 | 5.088 |
| 904 | 29.45 | 1.3754 | 1022360 | 0.0019 | 951 | 2.009E-6 | 5.702 | 5.132 |
| 910 | 29.51 | 1.3774 | 1023256 | 0.0019 | 911 | 2.090E-6 | 5.746 | 5.171 |
| 916 | 29.56 | 1.3792 | 1024096 | 0.0019 | 871 | 2.149E-6 | 5.792 | 5.213 |
| 922 | 29.62 | 1.3811 | 1024980 | 0.0019 | 844 | 2.237E-6 | 5.837 | 5.253 |
| 928 | 29.67 | 1.3829 | 1025782 | 0.0019 | 823 | 2.290E-6 | 5.884 | 5.295 |
| 935 | 29.72 | 1.3848 | 1026592 | 0.0039 | 1642 | 2.381E-6 | 5.932 | 5.339 |
| 942 | 29.78 | 1.3868 | 1027424 | 0.0039 | 1600 | 2.451E-6 | 5.979 | 5.381 |
| 948 | 29.84 | 1.3887 | 1028192 | 0.0895 | 18520 | 4.831E-6 | 0.000 | 0.000 |
| 1293 | 32.54 | 1.4763 | 1045944 | 0.0890 | 17884 | 4.979E-6 | 0.000 | 0.000 |
| 1296 | 32.59 | 1.4778 | 1046076 | 0.0032 | 293 | 1.107E-5 | 0.000 | 0.000 |
| 1299 | 32.65 | 1.4796 | 1046237 | 0.0038 | 333 | 1.146E-5 | 0.760 | 7.884 |
| 1303 | 32.72 | 1.4816 | 1046409 | 0.0039 | 337 | 1.167E-5 | 0.793 | 7.914 |
| 1306 | 32.78 | 1.4835 | 1046574 | 0.0035 | 317 | 1.112E-5 | 0.826 | 7.944 |
| 1309 | 32.83 | 1.4851 | 1046726 | 0.0019 | 165 | 1.147E-5 | 0.863 | 7.976 |
| 1313 | 32.90 | 1.4872 | 1046904 | 0.0019 | 163 | 1.149E-5 | 0.898 | 8.008 |
| 1317 | 32.97 | 1.4894 | 1047083 | 0.0019 | 163 | 1.169E-5 | 0.931 | 8.038 |
| 1320 | 33.02 | 1.4909 | 1047228 | 0.0019 | 162 | 1.183E-5 | 0.970 | 8.073 |
| 1324 | 33.09 | 1.4928 | 1047386 | 0.0019 | 159 | 1.190E-5 | 9.003 | 8.102 |
| 1327 | 33.16 | 1.4949 | 1047551 | 0.0019 | 156 | 1.215E-5 | 9.037 | 8.134 |
| 1331 | 33.22 | 1.4967 | 1047697 | 0.0019 | 156 | 1.230E-5 | 9.074 | 8.167 |
| 1334 | 33.28 | 1.4985 | 1047855 | 0.0019 | 153 | 1.239E-5 | 9.111 | 8.200 |
| 1338 | 33.35 | 1.5007 | 1048021 | 0.0019 | 151 | 1.250E-5 | 9.146 | 8.231 |
| 1342 | 33.41 | 1.5025 | 1048166 | 0.0019 | 153 | 1.249E-5 | 9.183 | 8.264 |
| 1345 | 33.47 | 1.5043 | 1048305 | 0.0019 | 150 | 1.269E-5 | 9.218 | 8.297 |
| 1349 | 33.54 | 1.5062 | 1048457 | 0.0019 | 146 | 1.285E-5 | 9.253 | 8.328 |
| 1353 | 33.60 | 1.5081 | 1048615 | 0.0019 | 148 | 1.287E-5 | 9.291 | 8.362 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^0.5) | deltaK |
|--------------|-------|-----------|---------|------------|-------|-------------------|-----------------------|--------|
| 1356 | 33.67 | 1.5101 | 1048754 | 0.0019 | 150 | 1.281E-5 | 9.328 | 8.395 |
| 1360 | 33.73 | 1.5120 | 1048895 | 0.0019 | 147 | 1.285E-5 | 9.364 | 8.428 |
| 1364 | 33.79 | 1.5138 | 1049055 | 0.0019 | 143 | 1.312E-5 | 9.402 | 8.462 |
| 1367 | 33.86 | 1.5158 | 1049207 | 0.0019 | 144 | 1.318E-5 | 9.437 | 8.493 |
| 1371 | 33.92 | 1.5176 | 1049339 | 0.0019 | 142 | 1.347E-5 | 9.476 | 8.529 |
| 1375 | 33.99 | 1.5196 | 1049475 | 0.0019 | 136 | 1.396E-5 | 9.512 | 8.561 |
| 1378 | 34.05 | 1.5215 | 1049617 | 0.0019 | 133 | 1.431E-5 | 9.551 | 8.596 |
| 1382 | 34.12 | 1.5234 | 1049744 | 0.0019 | 134 | 1.423E-5 | 9.588 | 8.629 |
| 1386 | 34.19 | 1.5252 | 1049871 | 0.0019 | 134 | 1.427E-5 | 9.626 | 8.664 |
| 1390 | 34.25 | 1.5272 | 1050003 | 0.0019 | 131 | 1.451E-5 | 9.662 | 8.696 |
| 1393 | 34.31 | 1.5289 | 1050140 | 0.0038 | 275 | 1.386E-5 | 9.703 | 8.732 |
| 1397 | 34.39 | 1.5310 | 1050278 | 0.0040 | 260 | 1.549E-5 | 9.740 | 8.766 |
| 1401 | 34.45 | 1.5330 | 1050400 | 0.6731 | 17374 | 3.874E-5 | 0.000 | 0.000 |
| 2450 | 72.99 | 2.2041 | 1067652 | 0.6731 | 17264 | 3.899E-5 | 0.000 | 0.000 |
| 2450 | 73.17 | 2.2061 | 1067664 | 0.0040 | 24 | 1.662E-4 | 0.000 | 0.000 |
| 2450 | 73.35 | 2.2081 | 1067676 | 0.0043 | 24 | 1.784E-4 | 28.101 | 25.291 |
| 2450 | 73.55 | 2.2104 | 1067688 | 0.0041 | 22 | 1.872E-4 | 28.148 | 25.333 |
| 2450 | 73.72 | 2.2122 | 1067698 | 0.0039 | 22 | 1.792E-4 | 28.201 | 25.380 |
| 2450 | 73.90 | 2.2143 | 1067710 | 0.0021 | 11 | 1.832E-4 | 28.250 | 25.425 |
| 2450 | 74.09 | 2.2164 | 1067721 | 0.0020 | 11 | 1.836E-4 | 28.299 | 25.469 |
| 2450 | 74.27 | 2.2184 | 1067732 | 0.0020 | 11 | 1.828E-4 | 28.351 | 25.516 |
| 2450 | 74.46 | 2.2204 | 1067743 | 0.0020 | 11 | 1.841E-4 | 28.401 | 25.561 |
| 2450 | 74.65 | 2.2226 | 1067755 | 0.0020 | 11 | 1.832E-4 | 28.451 | 25.606 |
| 2450 | 74.83 | 2.2245 | 1067765 | 0.0020 | 11 | 1.833E-4 | 28.502 | 25.652 |
| 2450 | 75.01 | 2.2265 | 1067776 | 0.0021 | 11 | 1.854E-4 | 28.552 | 25.697 |
| 2450 | 75.21 | 2.2286 | 1067788 | 0.0020 | 11 | 1.873E-4 | 28.602 | 25.742 |
| 2450 | 75.39 | 2.2305 | 1067798 | 0.0021 | 11 | 1.863E-4 | 28.655 | 25.789 |
| 2450 | 75.60 | 2.2328 | 1067809 | 0.0021 | 11 | 1.877E-4 | 28.706 | 25.836 |
| 2450 | 75.79 | 2.2348 | 1067821 | 0.0020 | 11 | 1.900E-4 | 28.761 | 25.884 |
| 2450 | 75.98 | 2.2369 | 1067832 | 0.0021 | 11 | 1.932E-4 | 28.812 | 25.931 |
| 2450 | 76.17 | 2.2389 | 1067842 | 0.0020 | 10 | 1.976E-4 | 28.864 | 25.978 |
| 2450 | 76.35 | 2.2409 | 1067852 | 0.0021 | 10 | 2.053E-4 | 28.915 | 26.023 |
| 2450 | 76.55 | 2.2429 | 1067861 | 0.0020 | 10 | 2.092E-4 | 28.966 | 26.069 |
| 2450 | 76.74 | 2.2450 | 1067871 | 0.0020 | 10 | 2.138E-4 | 29.020 | 26.118 |
| 2450 | 76.95 | 2.2471 | 1067881 | 0.0021 | 9 | 2.189E-4 | 29.071 | 26.164 |
| 2450 | 77.13 | 2.2491 | 1067890 | 0.0021 | 9 | 2.215E-4 | 29.126 | 26.213 |
| 2450 | 77.33 | 2.2511 | 1067899 | 0.0020 | 9 | 2.264E-4 | 29.179 | 26.261 |
| 2450 | 77.53 | 2.2532 | 1067908 | 0.0020 | 9 | 2.299E-4 | 29.232 | 26.308 |
| 2450 | 77.74 | 2.2553 | 1067917 | 0.0040 | 17 | 2.345E-4 | 29.285 | 26.356 |
| 2450 | 77.92 | 2.2572 | 1067925 | 0.0039 | 17 | 2.319E-4 | 29.338 | 26.404 |
| | 78.12 | 2.2593 | 1067934 | | | | | |

Automated Fatigue Crack
Growth Rate Analysis

| | | | |
|-----------------|----------------|---------------|------|
| Test ID | 5083-FCG-4pt05 | Geometry | C(T) |
| Contract | SSC 10624-01 | Orientation | T-L |
| Material | 5083-H321 | Yield (ksi) | 34.3 |
| Temperature (F) | 75 | Modulus (Msi) | 10.5 |
| Environment | Sea Water | | |

Specimen Dimensions (in)

| | | | |
|---------------|-------|-------------|-------|
| Thickness | 0.499 | Height | 2.400 |
| Net Thickness | 0.499 | Notch Depth | 1.000 |
| Width | 4.000 | Gage Length | 0.500 |

Precrack Parameters

| | | | |
|--------------|-------|--------------------|------|
| Pmax (lbs) | 784.0 | Stress Ratio | 0.10 |
| Final a (in) | 1.050 | Kmax (ksi sqr[in]) | 4.00 |

Test Parameters

| EvBP | Freq | Pmax | R | Ai | Kmaxi | C | DKi |
|--------|------|------|------|-------|-------|------|------|
| 32.540 | 0.05 | 0 | 0.10 | 1.491 | 8.80 | 2.00 | 0.00 |
| 55.200 | 0.05 | 2450 | 0.10 | 0.000 | 0.00 | 0.00 | 0.00 |

| K Coeff | C Coeff |
|---------|----------|
| .886 | 1.00098 |
| 4.64 | -4.66951 |
| -13.32 | 18.4601 |
| 14.72 | -236.825 |
| -5.6 | 1214.88 |
| . | -2143.57 |

Visual Observations

| EvB/P | Crack(EvB/P) | Crack(visual) | Error | CAF |
|--------|--------------|---------------|--------|-------|
| 20.869 | 1.012 | 1.000 | -0.012 | 1.013 |
| 21.842 | 1.062 | 1.065 | 0.003 | 1.010 |
| 23.217 | 1.127 | 1.125 | -0.002 | 1.006 |
| 24.253 | 1.174 | 1.170 | -0.004 | 1.004 |
| 24.439 | 1.182 | 1.195 | 0.013 | 1.003 |
| 28.306 | 1.335 | 1.350 | 0.015 | 0.995 |
| 32.493 | 1.475 | 1.480 | 0.005 | 0.987 |
| 34.530 | 1.535 | 1.530 | -0.005 | 0.984 |
| 36.488 | 1.589 | 1.580 | -0.009 | 0.982 |
| 46.151 | 1.812 | 1.805 | -0.007 | 0.970 |
| 54.785 | 1.965 | 1.955 | -0.010 | 0.962 |
| 72.549 | 2.199 | 2.210 | 0.011 | 0.951 |

Comments

Date of test: 9/11/2006
Waveform Type Sine

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in]^0.5) |
|--------------|-------|-----------|---------|------------|-------|-------------------|--------|-------------------------|
| | 34.57 | 1.5362 | 1050529 | | | | | |
| 1412 | 34.64 | 1.5383 | 1050642 | 0.0043 | 232 | 1.844E-5 | 9.890 | 8.901 |
| 1416 | 34.72 | 1.5408 | 1050761 | 0.0041 | 240 | 1.702E-5 | 9.932 | 8.939 |
| 1420 | 34.79 | 1.5424 | 1050882 | 0.0020 | 132 | 1.588E-5 | 9.973 | 8.976 |
| 1424 | 34.85 | 1.5442 | 1051008 | 0.0020 | 140 | 1.460E-5 | 10.011 | 9.010 |
| 1427 | 34.91 | 1.5461 | 1051155 | 0.0019 | 145 | 1.338E-5 | 10.051 | 9.046 |
| 1431 | 34.99 | 1.5481 | 1051322 | 0.0019 | 149 | 1.277E-5 | 10.091 | 9.082 |
| 1435 | 35.06 | 1.5501 | 1051481 | 0.0039 | 310 | 1.247E-5 | 10.132 | 9.118 |
| 1439 | 35.12 | 1.5520 | 1051632 | 0.0038 | 297 | 1.290E-5 | 10.173 | 9.156 |
| 1443 | 35.20 | 1.5540 | 1051778 | 0.7117 | 16317 | 4.362E-5 | 0.000 | 0.000 |
| 2450 | 78.55 | 2.2636 | 1067949 | 0.7113 | 16179 | 4.396E-5 | 0.000 | 0.000 |
| 2450 | 78.71 | 2.2653 | 1067957 | 0.0039 | 17 | 2.278E-4 | 29.553 | 26.596 |
| 2450 | 78.93 | 2.2675 | 1067966 | 0.0041 | 18 | 2.268E-4 | 29.602 | 26.642 |
| 2450 | 79.11 | 2.2693 | 1067975 | 0.0040 | 17 | 2.349E-4 | 29.661 | 26.694 |
| 2450 | 79.32 | 2.2715 | 1067983 | 0.0021 | 8 | 2.461E-4 | 29.711 | 26.741 |
| 2450 | 79.53 | 2.2735 | 1067992 | 0.0020 | 8 | 2.490E-4 | 29.769 | 26.792 |
| 2450 | 79.73 | 2.2756 | 1067999 | 0.0021 | 8 | 2.548E-4 | 29.825 | 26.842 |
| 2450 | 79.94 | 2.2777 | 1068007 | 0.0021 | 8 | 2.524E-4 | 29.878 | 26.891 |
| 2450 | 80.15 | 2.2797 | 1068016 | 0.0021 | 8 | 2.536E-4 | 29.938 | 26.943 |
| 2450 | 80.37 | 2.2819 | 1068024 | 0.0021 | 8 | 2.503E-4 | 29.991 | 26.993 |
| 2450 | 80.58 | 2.2839 | 1068033 | 0.0021 | 8 | 2.582E-4 | 30.050 | 27.045 |
| 2450 | 80.79 | 2.2860 | 1068041 | 0.0021 | 8 | 2.671E-4 | 30.107 | 27.096 |
| 2450 | 81.00 | 2.2880 | 1068048 | 0.0020 | 8 | 2.676E-4 | 30.162 | 27.146 |
| 2450 | 81.21 | 2.2901 | 1068055 | 0.0020 | 8 | 2.730E-4 | 30.221 | 27.198 |
| 2450 | 81.43 | 2.2923 | 1068063 | 0.0020 | 8 | 2.719E-4 | 30.273 | 27.245 |
| 2450 | 81.61 | 2.2940 | 1068070 | 0.0020 | 8 | 2.680E-4 | 30.330 | 27.297 |
| 2450 | 81.83 | 2.2961 | 1068078 | 0.0020 | 8 | 2.679E-4 | 30.386 | 27.347 |
| 2450 | 82.05 | 2.2982 | 1068086 | 0.0020 | 8 | 2.709E-4 | 30.442 | 27.398 |
| 2450 | 82.26 | 2.3002 | 1068093 | 0.0021 | 8 | 2.757E-4 | 30.499 | 27.449 |
| 2450 | 82.47 | 2.3022 | 1068100 | 0.0021 | 8 | 2.769E-4 | 30.558 | 27.502 |
| 2450 | 82.69 | 2.3043 | 1068108 | 0.0020 | 7 | 2.775E-4 | 30.615 | 27.552 |
| 2450 | 82.92 | 2.3065 | 1068115 | 0.0042 | 15 | 2.772E-4 | 30.672 | 27.606 |
| 2450 | 83.13 | 2.3085 | 1068123 | 0.0040 | 15 | 2.669E-4 | 30.732 | 27.657 |
| | 83.34 | 2.3105 | 1068130 | | | | | |

Automated Fatigue Crack
Growth Rate Analysis

| | | |
|-----------------|-------------------------|---------------|
| Test ID | 5083-FCG-4Cpt05Geometry | C(T) |
| Contract | SSC 10624-01 | Orientation |
| Material | 5083-H321 | Yield (ksi) |
| Temperature (F) | 75 | Modulus (Msi) |
| Environment | Sea Water | |

Specimen Dimensions (in)

| | | | |
|---------------|-------|-------------|-------|
| Thickness | 0.499 | Height | 2.400 |
| Net Thickness | 0.499 | Notch Depth | 1.000 |
| Width | 4.000 | Gage Length | 0.500 |

Precrack Parameters

| | | | |
|--------------|-------|--------------------|------|
| Pmax (lbs) | 784.0 | Stress Ratio | 0.10 |
| Final a (in) | 1.050 | Kmax (ksi sqr[in]) | 4.00 |

Test Parameters

| | | | | | | | |
|--------|------|------|------|-------|-------|------|------|
| EvBP | Freq | Pmax | R | Ai | Kmaxi | C | DKi |
| 32.540 | 0.05 | 0 | 0.10 | 1.491 | 8.80 | 2.00 | 0.00 |

| | |
|---------|----------|
| K Coeff | C Coeff |
| .886 | 1.00098 |
| 4.64 | -4.66951 |
| -13.32 | 18.4601 |
| 14.72 | -236.825 |
| -5.6 | 1214.88 |
| . | -2143.57 |

Visual Observations

| EvB/P | Crack(EvB/P) | Crack(visual) | Error | CAF |
|--------|--------------|---------------|--------|-------|
| 20.869 | 1.012 | 1.000 | -0.012 | 1.013 |
| 21.842 | 1.062 | 1.065 | 0.003 | 1.010 |
| 23.217 | 1.127 | 1.125 | -0.002 | 1.006 |
| 24.253 | 1.174 | 1.170 | -0.004 | 1.004 |
| 24.439 | 1.182 | 1.195 | 0.013 | 1.003 |
| 28.306 | 1.335 | 1.350 | 0.015 | 0.995 |
| 32.493 | 1.475 | 1.480 | 0.005 | 0.987 |
| 34.530 | 1.535 | 1.530 | -0.005 | 0.984 |
| 36.488 | 1.589 | 1.580 | -0.009 | 0.982 |
| 46.151 | 1.812 | 1.805 | -0.007 | 0.970 |
| 54.785 | 1.965 | 1.955 | -0.010 | 0.962 |
| 72.549 | 2.199 | 2.210 | 0.011 | 0.951 |

Comments

Date of test: 9/11/2006
Waveform Type Sine

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in]^0.5) |
|--------------|-------|-----------|---------|------------|-----|-------------------|--------|-------------------------|
| | 35.27 | 1.5561 | 1052018 | | | | | |
| 1450 | 35.32 | 1.5574 | 1052093 | 0.0033 | 193 | 1.702E-5 | 10.294 | 9.264 |
| 1454 | 35.39 | 1.5594 | 1052211 | 0.0039 | 239 | 1.636E-5 | 10.330 | 9.297 |
| 1458 | 35.46 | 1.5613 | 1052332 | 0.0018 | 108 | 1.733E-5 | 10.372 | 9.335 |
| 1463 | 35.54 | 1.5634 | 1052446 | 0.0019 | 113 | 1.699E-5 | 10.415 | 9.373 |
| 1467 | 35.61 | 1.5654 | 1052559 | 0.0019 | 110 | 1.717E-5 | 10.455 | 9.410 |
| 1470 | 35.67 | 1.5672 | 1052668 | 0.0019 | 108 | 1.746E-5 | 10.496 | 9.447 |
| 1474 | 35.74 | 1.5689 | 1052772 | 0.0019 | 107 | 1.754E-5 | 10.536 | 9.482 |
| 1478 | 35.81 | 1.5708 | 1052872 | 0.0019 | 107 | 1.762E-5 | 10.577 | 9.519 |
| 1482 | 35.88 | 1.5728 | 1052981 | 0.0019 | 105 | 1.785E-5 | 10.618 | 9.556 |
| 1486 | 35.95 | 1.5747 | 1053090 | 0.0019 | 104 | 1.792E-5 | 10.660 | 9.594 |
| 1490 | 36.02 | 1.5766 | 1053198 | 0.0019 | 105 | 1.810E-5 | 10.701 | 9.631 |
| 1494 | 36.08 | 1.5784 | 1053298 | 0.0019 | 105 | 1.825E-5 | 10.742 | 9.668 |
| 1498 | 36.15 | 1.5802 | 1053394 | 0.0019 | 104 | 1.849E-5 | 10.786 | 9.707 |
| 1502 | 36.23 | 1.5823 | 1053503 | 0.0019 | 104 | 1.864E-5 | 10.827 | 9.744 |
| 1506 | 36.30 | 1.5842 | 1053611 | 0.0039 | 213 | 1.820E-5 | 10.873 | 9.786 |
| 1510 | 36.37 | 1.5862 | 1053716 | 0.0039 | 209 | 1.850E-5 | 10.916 | 9.824 |
| | 36.44 | 1.5881 | 1053820 | | | | | |

Automated Fatigue Crack
Growth Rate Analysis

| | | | |
|-----------------|--------------|---------------|------|
| Test ID | 5083-FCG-5 | Geometry | C(T) |
| Contract | SSC 10624-01 | Orientation | T-L |
| Material | 5083-H321 | Yield (ksi) | 34.3 |
| Temperature (F) | 75 | Modulus (Msi) | 10.5 |
| Environment | RH = 40% | | |

Specimen Dimensions (in)

| | | | |
|---------------|-------|-------------|-------|
| Thickness | 0.501 | Height | 2.400 |
| Net Thickness | 0.501 | Notch Depth | 1.000 |
| Width | 4.000 | Gage Length | 0.500 |

Precrack Parameters

| | | | |
|--------------|-------|---------------------|------|
| Pmax (lbs) | 970.0 | Stress Ratio | 0.10 |
| Final a (in) | 1.070 | Kmax (ksi sqrt[in]) | 5.00 |

Test Parameters

| | | | | | | | |
|--------|-------|------|------|-------|-------|-------|------|
| EvBP | Freq | Pmax | R | Ai | Kmaxi | C | DKi |
| 22.377 | 24.00 | 0 | 0.10 | 1.070 | 5.00 | -4.00 | 0.00 |
| 25.814 | 24.00 | 0 | 0.10 | 1.220 | 3.00 | 4.00 | 0.00 |

| | | |
|---------|----------|------------------------------|
| K Coeff | C Coeff | da/dN Fit Parameters (DKapp) |
| .886 | 1.00098 | Upper da/dN limit |
| 4.64 | -4.66951 | Lower da/dN limit |
| -13.32 | 18.4601 | da/dN intercept (C) |
| 14.72 | -236.825 | da/dN slope (m) |
| -5.6 | 1214.88 | da/dN for delta K |
| . | -2143.57 | delta K |

Visual Observations

| | | | | |
|--------|--------------|---------------|--------|-------|
| EvB/P | Crack(EvB/P) | Crack(visual) | Error | CAF |
| 20.596 | 0.986 | 1.002 | 0.016 | 1.004 |
| 22.230 | 1.095 | 1.085 | -0.010 | 1.022 |
| 23.182 | 1.153 | 1.130 | -0.023 | 1.031 |
| 25.135 | 1.263 | 1.280 | 0.017 | 1.050 |
| 29.099 | 1.377 | 1.380 | 0.003 | 1.007 |
| 33.040 | 1.491 | 1.485 | -0.006 | 0.986 |
| 36.200 | 1.571 | 1.575 | 0.004 | 0.972 |

Comments

Date of test: 9/15/2006
Waveform Type Sine

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^0.5) | deltaK |
|--------------|-------|-----------|---------|------------|--------|-------------------|-----------------------|--------|
| | 22.38 | 1.1041 | 10728 | | | | | |
| 915 | 22.47 | 1.1100 | 23029 | 0.0121 | 27551 | 4.410E-7 | 4.839 | 4.355 |
| 893 | 22.57 | 1.1163 | 38279 | 0.0123 | 32016 | 3.831E-7 | 4.750 | 4.275 |
| 873 | 22.67 | 1.1222 | 55045 | 0.0061 | 18007 | 3.736E-7 | 4.656 | 4.190 |
| 852 | 22.77 | 1.1286 | 75113 | 0.0061 | 19963 | 3.249E-7 | 4.568 | 4.111 |
| 832 | 22.88 | 1.1348 | 96589 | 0.0060 | 22076 | 2.914E-7 | 4.481 | 4.033 |
| 814 | 22.97 | 1.1406 | 118770 | 0.0061 | 24696 | 2.664E-7 | 4.396 | 3.957 |
| 796 | 23.07 | 1.1464 | 142808 | 0.0061 | 26807 | 2.441E-7 | 4.316 | 3.884 |
| 778 | 23.17 | 1.1523 | 170733 | 0.0061 | 28683 | 2.229E-7 | 4.232 | 3.809 |
| 759 | 23.28 | 1.1589 | 203223 | 0.0061 | 30846 | 2.046E-7 | 4.151 | 3.736 |
| 741 | 23.38 | 1.1652 | 235954 | 0.0061 | 32699 | 1.905E-7 | 4.069 | 3.662 |
| 724 | 23.49 | 1.1712 | 268687 | 0.0061 | 34308 | 1.810E-7 | 3.990 | 3.591 |
| 707 | 23.59 | 1.1772 | 303843 | 0.0061 | 35864 | 1.732E-7 | 3.914 | 3.523 |
| 691 | 23.69 | 1.1831 | 339000 | 0.0059 | 38490 | 1.643E-7 | 3.840 | 3.456 |
| 676 | 23.79 | 1.1891 | 376581 | 0.0061 | 41052 | 1.551E-7 | 3.767 | 3.390 |
| 660 | 23.90 | 1.1952 | 418404 | 0.0060 | 43715 | 1.453E-7 | 3.697 | 3.327 |
| 646 | 24.00 | 1.2008 | 466891 | 0.0060 | 50006 | 1.350E-7 | 3.622 | 3.260 |
| 629 | 24.12 | 1.2078 | 514999 | 0.0060 | 59226 | 1.248E-7 | 3.556 | 3.201 |
| 615 | 24.22 | 1.2134 | 566135 | 0.0058 | 69269 | 1.118E-7 | 3.484 | 3.136 |
| 601 | 24.33 | 1.2193 | 639038 | 0.0056 | 78447 | 9.119E-8 | 3.419 | 3.077 |
| 587 | 24.44 | 1.2254 | 731939 | 0.0050 | 87071 | 6.515E-8 | 3.359 | 3.023 |
| 576 | 24.53 | 1.2302 | 834016 | 0.0045 | 95189 | 4.837E-8 | 3.305 | 2.975 |
| 568 | 24.60 | 1.2341 | 937571 | 0.0039 | 99681 | 3.802E-8 | 3.260 | 2.934 |
| 560 | 24.66 | 1.2376 | 1037427 | 0.0032 | 100841 | 3.077E-8 | 3.226 | 2.904 |
| 554 | 24.71 | 1.2401 | 1137270 | 0.0027 | 100470 | 2.639E-8 | 3.194 | 2.875 |
| 549 | 24.75 | 1.2425 | 1237125 | 0.0025 | 99854 | 2.368E-8 | 3.173 | 2.856 |
| 546 | 24.78 | 1.2443 | 1336982 | 0.0022 | 99852 | 2.176E-8 | 3.149 | 2.834 |
| 541 | 24.83 | 1.2466 | 1436838 | 0.0020 | 99854 | 2.047E-8 | 3.129 | 2.816 |
| 536 | 24.87 | 1.2488 | 1536694 | 0.0017 | 99854 | 1.844E-8 | 3.108 | 2.797 |
| 532 | 24.90 | 1.2507 | 1636537 | 0.0016 | 99854 | 1.620E-8 | 3.089 | 2.780 |
| 529 | 24.93 | 1.2522 | 1736391 | 0.0014 | 99854 | 1.348E-8 | 3.074 | 2.767 |
| 527 | 24.94 | 1.2530 | 1836248 | 0.0012 | 99852 | 1.136E-8 | 3.063 | 2.756 |
| 525 | 24.96 | 1.2539 | 1936105 | 0.0010 | 99854 | 9.715E-9 | 3.053 | 2.747 |
| 523 | 24.98 | 1.2550 | 2035961 | 0.0008 | 99854 | 8.715E-9 | 3.044 | 2.739 |
| 521 | 25.00 | 1.2560 | 2135807 | 0.0008 | 99854 | 8.383E-9 | 3.034 | 2.731 |
| 520 | 25.01 | 1.2566 | 2235659 | 0.0008 | 99854 | 8.113E-9 | 3.027 | 2.724 |
| 519 | 25.02 | 1.2573 | 2335516 | 0.0008 | 99853 | 7.915E-9 | 3.019 | 2.717 |
| 517 | 25.04 | 1.2581 | 2435373 | 0.0008 | 99853 | 7.876E-9 | 3.012 | 2.711 |
| 515 | 25.06 | 1.2590 | 2535229 | 0.0008 | 99854 | 7.890E-9 | 3.004 | 2.704 |
| 513 | 25.07 | 1.2599 | 2635076 | 0.0007 | 99854 | 7.276E-9 | 2.996 | 2.697 |
| 512 | 25.09 | 1.2606 | 2734926 | 0.0006 | 99854 | 5.927E-9 | 2.989 | 2.690 |
| 511 | 25.10 | 1.2611 | 2834782 | 0.0004 | 99853 | 4.154E-9 | 2.984 | 2.685 |
| 510 | 25.10 | 1.2615 | 2934639 | 0.0003 | 99853 | 2.475E-9 | 2.981 | 2.683 |
| | 25.10 | 1.2615 | 3034496 | | | | | |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^0.5) | deltaK |
|--------------|-------|-----------|---------|------------|---------|-------------------|-----------------------|--------|
| 510 | 25.10 | 1.2615 | 3134345 | -0.0001 | 199697 | -4.017E-10 | 2.977 | 2.680 |
| 510 | 25.10 | 1.2615 | 3234193 | 0.0395 | 1938770 | -2.037E-8 | 0.000 | 0.000 |
| 674 | 27.12 | 1.3010 | 1195575 | 0.0444 | 2015140 | -2.204E-8 | 0.000 | 0.000 |
| 685 | 27.24 | 1.3059 | 1219053 | 0.0094 | 48927 | 1.915E-7 | 4.117 | 3.706 |
| 696 | 27.36 | 1.3104 | 1244502 | 0.0098 | 48475 | 2.027E-7 | 4.202 | 3.781 |
| 709 | 27.49 | 1.3157 | 1267528 | 0.0099 | 41447 | 2.400E-7 | 4.281 | 3.853 |
| 720 | 27.61 | 1.3203 | 1285949 | 0.0049 | 19014 | 2.689E-7 | 4.368 | 3.931 |
| 732 | 27.73 | 1.3251 | 1303205 | 0.0050 | 17151 | 2.972E-7 | 4.454 | 4.009 |
| 744 | 27.86 | 1.3302 | 1318713 | 0.0049 | 15278 | 3.288E-7 | 4.541 | 4.087 |
| 757 | 27.98 | 1.3350 | 1333137 | 0.0050 | 13697 | 3.702E-7 | 4.635 | 4.171 |
| 770 | 28.11 | 1.3402 | 1347407 | 0.0050 | 12211 | 4.295E-7 | 4.728 | 4.255 |
| 783 | 28.25 | 1.3454 | 1359195 | 0.0051 | 10885 | 5.102E-7 | 4.823 | 4.340 |
| 795 | 28.37 | 1.3501 | 1368130 | 0.0051 | 9434 | 5.970E-7 | 4.923 | 4.431 |
| 810 | 28.51 | 1.3552 | 1376473 | 0.0050 | 7861 | 6.949E-7 | 5.026 | 4.523 |
| 825 | 28.66 | 1.3609 | 1384022 | 0.0049 | 6683 | 7.959E-7 | 5.128 | 4.616 |
| 838 | 28.78 | 1.3657 | 1389742 | 0.0049 | 5941 | 8.682E-7 | 5.232 | 4.709 |
| 851 | 28.90 | 1.3702 | 1394570 | 0.0048 | 5194 | 9.459E-7 | 5.335 | 4.802 |
| 865 | 29.03 | 1.3749 | 1399295 | 0.0046 | 4512 | 1.024E-6 | 5.433 | 4.890 |
| 879 | 29.16 | 1.3793 | 1403773 | 0.0044 | 4073 | 1.109E-6 | 5.546 | 4.992 |
| 895 | 29.31 | 1.3840 | 1407636 | 0.0044 | 3751 | 1.204E-6 | 5.654 | 5.088 |
| 911 | 29.45 | 1.3882 | 1411091 | 0.0043 | 3397 | 1.314E-6 | 5.770 | 5.193 |
| 926 | 29.58 | 1.3924 | 1414180 | 0.0043 | 3037 | 1.428E-6 | 5.888 | 5.299 |
| 943 | 29.73 | 1.3967 | 1417074 | 0.0042 | 2740 | 1.563E-6 | 6.003 | 5.403 |
| 959 | 29.87 | 1.4010 | 1419676 | 0.0042 | 2473 | 1.724E-6 | 6.122 | 5.509 |
| 974 | 30.00 | 1.4049 | 1421993 | 0.0042 | 2264 | 1.891E-6 | 6.242 | 5.618 |
| 991 | 30.14 | 1.4092 | 1424076 | 0.0041 | 2060 | 2.057E-6 | 6.361 | 5.725 |
| 1007 | 30.28 | 1.4132 | 1425930 | 0.0041 | 1863 | 2.252E-6 | 6.486 | 5.838 |
| 1024 | 30.42 | 1.4175 | 1427764 | 0.0042 | 1711 | 2.471E-6 | 6.610 | 5.949 |
| 1041 | 30.56 | 1.4216 | 1429431 | 0.0042 | 1588 | 2.704E-6 | 6.741 | 6.067 |
| 1059 | 30.70 | 1.4257 | 1430851 | 0.0043 | 1459 | 2.970E-6 | 6.873 | 6.186 |
| 1077 | 30.85 | 1.4300 | 1432260 | 0.0042 | 1319 | 3.252E-6 | 7.012 | 6.311 |
| 1096 | 31.00 | 1.4345 | 1433602 | 0.0042 | 1212 | 3.537E-6 | 7.153 | 6.438 |
| 1115 | 31.15 | 1.4388 | 1434685 | 0.0042 | 1132 | 3.789E-6 | 7.291 | 6.562 |
| 1132 | 31.28 | 1.4425 | 1435677 | 0.0042 | 1039 | 4.081E-6 | 7.437 | 6.693 |
| 1152 | 31.43 | 1.4468 | 1436702 | 0.0042 | 944 | 4.424E-6 | 7.577 | 6.819 |
| 1171 | 31.58 | 1.4511 | 1437641 | 0.0042 | 889 | 4.767E-6 | 7.729 | 6.956 |
| 1191 | 31.74 | 1.4554 | 1438494 | 0.0042 | 850 | 5.068E-6 | 7.878 | 7.090 |
| 1211 | 31.89 | 1.4595 | 1439263 | 0.0042 | 789 | 5.380E-6 | 8.039 | 7.235 |
| 1232 | 32.04 | 1.4638 | 1440019 | 0.0042 | 735 | 5.695E-6 | 8.193 | 7.374 |
| 1253 | 32.19 | 1.4680 | 1440779 | 0.0042 | 688 | 6.085E-6 | 8.357 | 7.522 |
| 1274 | 32.34 | 1.4722 | 1441436 | 0.0042 | 652 | 6.474E-6 | 8.518 | 7.666 |
| 1295 | 32.49 | 1.4762 | 1442048 | 0.0042 | 613 | 6.983E-6 | 8.686 | 7.818 |
| 1317 | 32.65 | 1.4805 | 1442624 | 0.0084 | 1126 | 7.480E-6 | 8.851 | 7.966 |
| 1338 | 32.80 | 1.4846 | 1443174 | 0.0086 | 1071 | 8.070E-6 | 9.033 | 8.130 |
| | 32.97 | 1.4892 | 1443695 | | | | | |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^0.5) | deltaK |
|--------------|-------|-----------|---|------------|----|-------------------|-----------------------|--------|
|--------------|-------|-----------|---|------------|----|-------------------|-----------------------|--------|

Automated Fatigue Crack
Growth Rate Analysis

| | | | |
|-----------------|--------------|---------------|------|
| Test ID | 5086-FCG-1 | Geometry | C(T) |
| Contract | SSC 10624-01 | Orientation | T-L |
| Material | 5086-H116 | Yield (ksi) | 27.0 |
| Temperature (F) | 75 | Modulus (Msi) | 10.5 |
| Environment | RH = 40% | | |

Specimen Dimensions (in)

| | | | |
|---------------|-------|-------------|-------|
| Thickness | 0.496 | Height | 2.400 |
| Net Thickness | 0.496 | Notch Depth | 1.000 |
| Width | 4.000 | Gage Length | 0.500 |

Precrack Parameters

| | | | |
|--------------|-------|---------------------|------|
| Pmax (lbs) | 779.0 | Stress Ratio | 0.10 |
| Final a (in) | 1.050 | Kmax (ksi sqrt(in)) | 4.00 |

Test Parameters

| EvBP | Freq | Pmax | R | Ai | Kmaxi | C | DKi |
|--------|-------|------|------|-------|-------|------|------|
| 22.978 | 10.00 | 0 | 0.10 | 1.100 | 3.20 | 4.00 | 0.00 |
| 29.766 | 10.00 | 0 | 0.10 | 1.396 | 10.42 | 2.00 | 0.00 |
| 47.942 | 5.00 | 2975 | 0.10 | 0.000 | 0.00 | 0.00 | 0.00 |

| K Coeff | C Coeff |
|---------|----------|
| .886 | 1.00098 |
| 4.64 | -4.66951 |
| -13.32 | 18.4601 |
| 14.72 | -236.825 |
| -5.6 | 1214.88 |
| . | -2143.57 |

Visual Observations

| EvB/P | Crack(EvB/P) | Crack(visual) | Error | CAF |
|--------|--------------|---------------|--------|-------|
| 20.484 | 0.989 | 1.001 | 0.013 | 1.011 |
| 21.438 | 1.038 | 1.035 | -0.003 | 1.009 |
| 21.843 | 1.059 | 1.055 | -0.004 | 1.007 |
| 22.920 | 1.110 | 1.115 | 0.005 | 1.005 |
| 24.869 | 1.197 | 1.195 | -0.002 | 1.000 |
| 26.312 | 1.256 | 1.255 | -0.001 | 0.997 |
| 27.456 | 1.301 | 1.295 | -0.006 | 0.994 |
| 29.780 | 1.384 | 1.380 | -0.004 | 0.990 |
| 39.990 | 1.675 | 1.665 | -0.010 | 0.975 |
| 47.607 | 1.838 | 1.850 | 0.012 | 0.967 |

Comments

Date of test: 8/16/2006
Waveform Type Sine

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in] ^{.5}) |
|--------------|-------|-----------|--------|------------|--------|-------------------|-------|------------------------------------|
| | 23.06 | 1.1171 | 66929 | | | | | |
| 639 | 23.17 | 1.1219 | 119196 | 0.0095 | 102819 | 9.261E-8 | 3.441 | 3.097 |
| 650 | 23.27 | 1.1267 | 169748 | 0.0095 | 97833 | 9.739E-8 | 3.510 | 3.159 |
| 661 | 23.37 | 1.1314 | 217029 | 0.0048 | 46026 | 1.035E-7 | 3.580 | 3.222 |
| 672 | 23.48 | 1.1360 | 260146 | 0.0047 | 43374 | 1.097E-7 | 3.652 | 3.286 |
| 683 | 23.58 | 1.1408 | 302605 | 0.0047 | 40604 | 1.166E-7 | 3.724 | 3.352 |
| 695 | 23.69 | 1.1457 | 343082 | 0.0047 | 38177 | 1.245E-7 | 3.799 | 3.419 |
| 707 | 23.79 | 1.1504 | 379439 | 0.0048 | 36445 | 1.322E-7 | 3.875 | 3.487 |
| 718 | 23.90 | 1.1550 | 413372 | 0.0048 | 34216 | 1.401E-7 | 3.953 | 3.558 |
| 731 | 24.01 | 1.1598 | 446093 | 0.0047 | 31913 | 1.478E-7 | 4.033 | 3.630 |
| 744 | 24.12 | 1.1648 | 478814 | 0.0047 | 30297 | 1.563E-7 | 4.114 | 3.702 |
| 756 | 24.23 | 1.1694 | 507899 | 0.0048 | 28681 | 1.666E-7 | 4.196 | 3.777 |
| 768 | 24.33 | 1.1739 | 534561 | 0.0048 | 26662 | 1.789E-7 | 4.280 | 3.852 |
| 781 | 24.44 | 1.1787 | 561222 | 0.0047 | 24440 | 1.943E-7 | 4.365 | 3.929 |
| 795 | 24.55 | 1.1837 | 585460 | 0.0047 | 22501 | 2.132E-7 | 4.453 | 4.008 |
| 808 | 24.66 | 1.1883 | 606062 | 0.0047 | 20642 | 2.345E-7 | 4.542 | 4.088 |
| 821 | 24.77 | 1.1929 | 625453 | 0.0047 | 18525 | 2.600E-7 | 4.632 | 4.169 |
| 835 | 24.88 | 1.1976 | 642904 | 0.0047 | 16553 | 2.898E-7 | 4.723 | 4.251 |
| 849 | 24.99 | 1.2022 | 658414 | 0.0047 | 14981 | 3.249E-7 | 4.817 | 4.335 |
| 863 | 25.10 | 1.2069 | 672371 | 0.0047 | 13404 | 3.662E-7 | 4.914 | 4.422 |
| 878 | 25.21 | 1.2117 | 684779 | 0.0048 | 12067 | 4.094E-7 | 5.011 | 4.510 |
| 893 | 25.33 | 1.2164 | 695946 | 0.0048 | 10823 | 4.558E-7 | 5.115 | 4.603 |
| 909 | 25.44 | 1.2213 | 705875 | 0.0047 | 9675 | 5.053E-7 | 5.218 | 4.696 |
| 924 | 25.56 | 1.2262 | 715306 | 0.0047 | 8719 | 5.608E-7 | 5.325 | 4.792 |
| 940 | 25.68 | 1.2308 | 723351 | 0.0047 | 7863 | 6.164E-7 | 5.431 | 4.888 |
| 956 | 25.79 | 1.2354 | 730421 | 0.0047 | 7108 | 6.811E-7 | 5.540 | 4.986 |
| 972 | 25.91 | 1.2401 | 737090 | 0.0047 | 6341 | 7.605E-7 | 5.648 | 5.083 |
| 988 | 26.02 | 1.2447 | 743124 | 0.0047 | 5686 | 8.554E-7 | 5.762 | 5.186 |
| 1005 | 26.14 | 1.2496 | 748523 | 0.0047 | 5111 | 9.653E-7 | 5.877 | 5.290 |
| 1022 | 26.26 | 1.2544 | 753350 | 0.0047 | 4542 | 1.090E-6 | 5.996 | 5.397 |
| 1040 | 26.38 | 1.2591 | 757468 | 0.0047 | 4040 | 1.216E-6 | 6.118 | 5.506 |
| 1057 | 26.50 | 1.2637 | 761087 | 0.0047 | 3639 | 1.337E-6 | 6.237 | 5.613 |
| 1074 | 26.62 | 1.2684 | 764339 | 0.0047 | 3268 | 1.471E-6 | 6.361 | 5.725 |
| 1092 | 26.74 | 1.2730 | 767363 | 0.0047 | 2933 | 1.623E-6 | 6.489 | 5.840 |
| 1112 | 26.86 | 1.2779 | 770355 | 0.0047 | 2653 | 1.816E-6 | 6.620 | 5.958 |
| 1131 | 26.99 | 1.2828 | 772957 | 0.0047 | 2416 | 2.034E-6 | 6.751 | 6.076 |
| 1149 | 27.11 | 1.2873 | 775065 | 0.0047 | 2190 | 2.246E-6 | 6.888 | 6.199 |
| 1168 | 27.23 | 1.2919 | 777003 | 0.0047 | 1955 | 2.480E-6 | 7.022 | 6.320 |
| 1188 | 27.35 | 1.2967 | 778836 | 0.0047 | 1758 | 2.737E-6 | 7.161 | 6.445 |
| 1208 | 27.48 | 1.3013 | 780503 | 0.0048 | 1608 | 3.011E-6 | 7.307 | 6.577 |
| 1229 | 27.61 | 1.3063 | 782086 | 0.0048 | 1472 | 3.322E-6 | 7.456 | 6.710 |
| 1251 | 27.74 | 1.3112 | 783507 | 0.0048 | 1345 | 3.664E-6 | 7.605 | 6.845 |
| 1271 | 27.86 | 1.3158 | 784714 | 0.0048 | 1225 | 3.995E-6 | 7.762 | 6.986 |
| 1293 | 27.99 | 1.3205 | 785837 | 0.0047 | 1111 | 4.310E-6 | 7.916 | 7.125 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^0.5) | deltaK |
|--------------|-------|-----------|--------|------------|------|-------------------|-----------------------|--------|
| 1316 | 28.12 | 1.3254 | 786904 | 0.0047 | 1016 | 4.642E-6 | 8.074 | 7.267 |
| 1337 | 28.25 | 1.3300 | 787854 | 0.0047 | 950 | 4.961E-6 | 8.234 | 7.411 |
| 1359 | 28.37 | 1.3345 | 788750 | 0.0047 | 890 | 5.306E-6 | 8.396 | 7.556 |
| 1382 | 28.50 | 1.3392 | 789604 | 0.0047 | 828 | 5.691E-6 | 8.560 | 7.704 |
| 1405 | 28.64 | 1.3439 | 790415 | 0.0047 | 772 | 6.124E-6 | 8.733 | 7.860 |
| 1430 | 28.77 | 1.3488 | 791179 | 0.0047 | 727 | 6.564E-6 | 8.907 | 8.017 |
| 1454 | 28.90 | 1.3535 | 791870 | 0.0047 | 686 | 6.980E-6 | 9.086 | 8.177 |
| 1478 | 29.03 | 1.3581 | 792483 | 0.0048 | 647 | 7.371E-6 | 9.268 | 8.341 |
| 1503 | 29.17 | 1.3628 | 793114 | 0.0048 | 611 | 7.831E-6 | 9.452 | 8.507 |
| 1529 | 29.31 | 1.3676 | 793718 | 0.0048 | 573 | 8.304E-6 | 9.644 | 8.679 |
| 1555 | 29.44 | 1.3725 | 794294 | 0.0099 | 1125 | 8.837E-6 | 9.844 | 8.860 |
| 1583 | 29.59 | 1.3776 | 794843 | 0.0096 | 1014 | 9.505E-6 | 10.040 | 9.036 |
| | 29.72 | 1.3821 | 795308 | | | | | |
| | 29.77 | 1.3836 | 795836 | | | | | |
| 1627 | 29.88 | 1.3875 | 796251 | 0.0105 | 1074 | 9.792E-6 | 10.425 | 9.382 |
| 1643 | 30.08 | 1.3941 | 796910 | 0.0158 | 1558 | 1.014E-5 | 10.568 | 9.511 |
| 1664 | 30.35 | 1.4033 | 797809 | 0.0189 | 1803 | 1.048E-5 | 10.747 | 9.672 |
| 1687 | 30.64 | 1.4130 | 798713 | 0.0090 | 816 | 1.106E-5 | 10.958 | 9.862 |
| 1710 | 30.94 | 1.4228 | 799594 | 0.0095 | 827 | 1.150E-5 | 11.176 | 10.059 |
| 1734 | 31.23 | 1.4323 | 800388 | 0.0095 | 793 | 1.202E-5 | 11.400 | 10.260 |
| 1757 | 31.53 | 1.4417 | 801149 | 0.0095 | 757 | 1.258E-5 | 11.623 | 10.461 |
| 1781 | 31.82 | 1.4511 | 801874 | 0.0095 | 720 | 1.318E-5 | 11.851 | 10.666 |
| 1804 | 32.12 | 1.4604 | 802565 | 0.0095 | 690 | 1.372E-5 | 12.086 | 10.877 |
| 1829 | 32.43 | 1.4701 | 803256 | 0.0095 | 663 | 1.432E-5 | 12.327 | 11.094 |
| 1855 | 32.75 | 1.4799 | 803913 | 0.0095 | 639 | 1.492E-5 | 12.572 | 11.314 |
| 1880 | 33.05 | 1.4891 | 804526 | 0.0096 | 615 | 1.552E-5 | 12.827 | 11.545 |
| 1906 | 33.37 | 1.4988 | 805129 | 0.0095 | 587 | 1.621E-5 | 13.078 | 11.770 |
| 1931 | 33.69 | 1.5082 | 805706 | 0.0095 | 562 | 1.686E-5 | 13.340 | 12.006 |
| 1957 | 34.02 | 1.5178 | 806254 | 0.0096 | 540 | 1.765E-5 | 13.604 | 12.243 |
| 1984 | 34.35 | 1.5273 | 806776 | 0.0095 | 516 | 1.847E-5 | 13.873 | 12.486 |
| 2011 | 34.67 | 1.5367 | 807285 | 0.0096 | 493 | 1.942E-5 | 14.152 | 12.736 |
| 2039 | 35.02 | 1.5465 | 807766 | 0.0095 | 467 | 2.039E-5 | 14.432 | 12.989 |
| 2066 | 35.36 | 1.5560 | 808224 | 0.0095 | 445 | 2.146E-5 | 14.724 | 13.251 |
| 2094 | 35.71 | 1.5657 | 808661 | 0.0096 | 422 | 2.264E-5 | 15.011 | 13.510 |
| 2122 | 36.05 | 1.5748 | 809054 | 0.0095 | 398 | 2.384E-5 | 15.311 | 13.780 |
| 2150 | 36.40 | 1.5844 | 809445 | 0.0095 | 377 | 2.520E-5 | 15.610 | 14.049 |
| 2179 | 36.76 | 1.5940 | 809818 | 0.0095 | 357 | 2.671E-5 | 15.918 | 14.326 |
| 2208 | 37.12 | 1.6034 | 810156 | 0.0095 | 339 | 2.820E-5 | 16.236 | 14.613 |
| 2238 | 37.49 | 1.6130 | 810487 | 0.0095 | 321 | 2.971E-5 | 16.558 | 14.903 |
| 2269 | 37.87 | 1.6227 | 810800 | 0.0095 | 306 | 3.123E-5 | 16.882 | 15.194 |
| 2298 | 38.23 | 1.6319 | 811085 | 0.0097 | 295 | 3.271E-5 | 17.217 | 15.495 |
| 2328 | 38.60 | 1.6414 | 811369 | 0.0097 | 280 | 3.438E-5 | 17.559 | 15.803 |
| 2360 | 39.01 | 1.6513 | 811654 | 0.0096 | 263 | 3.642E-5 | 17.913 | 16.122 |
| 2393 | 39.42 | 1.6614 | 811924 | 0.0096 | 251 | 3.857E-5 | 18.277 | 16.449 |
| 2425 | 39.81 | 1.6709 | 812164 | 0.0097 | 239 | 4.088E-5 | 18.644 | 16.780 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in]^0.5) |
|--------------|-------|-----------|--------|------------|-----|-------------------|--------|-------------------------|
| 2457 | 40.21 | 1.6803 | 812379 | 0.0096 | 223 | 4.303E-5 | 19.009 | 17.108 |
| 2488 | 40.59 | 1.6894 | 812590 | 0.0095 | 209 | 4.540E-5 | 19.389 | 17.451 |
| 2522 | 41.02 | 1.6994 | 812800 | 0.0095 | 198 | 4.801E-5 | 19.759 | 17.783 |
| 2554 | 41.42 | 1.7086 | 812992 | 0.0096 | 189 | 5.068E-5 | 20.159 | 18.143 |
| 2588 | 41.85 | 1.7183 | 813175 | 0.0096 | 180 | 5.363E-5 | 20.551 | 18.496 |
| 2622 | 42.28 | 1.7280 | 813349 | 0.0095 | 168 | 5.673E-5 | 20.965 | 18.869 |
| 2658 | 42.72 | 1.7377 | 813515 | 0.0096 | 160 | 6.010E-5 | 21.376 | 19.239 |
| 2692 | 43.15 | 1.7471 | 813668 | 0.0096 | 152 | 6.337E-5 | 21.800 | 19.620 |
| 2726 | 43.58 | 1.7564 | 813809 | 0.0096 | 144 | 6.649E-5 | 22.229 | 20.006 |
| 2762 | 44.04 | 1.7661 | 813950 | 0.0096 | 137 | 7.005E-5 | 22.665 | 20.399 |
| 2798 | 44.50 | 1.7758 | 814084 | 0.0097 | 130 | 7.413E-5 | 23.114 | 20.803 |
| 2834 | 44.96 | 1.7853 | 814212 | 0.0097 | 124 | 7.824E-5 | 23.577 | 21.220 |
| 2871 | 45.44 | 1.7951 | 814334 | 0.0097 | 118 | 8.238E-5 | 24.053 | 21.648 |
| 2910 | 45.94 | 1.8053 | 814450 | 0.0096 | 112 | 8.678E-5 | 24.531 | 22.078 |
| 2947 | 46.42 | 1.8147 | 814555 | 0.0188 | 207 | 9.063E-5 | 25.022 | 22.521 |
| 2984 | 46.89 | 1.8240 | 814657 | 0.0189 | 199 | 9.509E-5 | 25.511 | 22.960 |
| | 47.39 | 1.8336 | 814754 | | | | | |
| | 47.94 | 1.8445 | 814876 | | | | | |
| 2975 | 48.38 | 1.8532 | 814967 | 0.0188 | 194 | 9.695E-5 | 25.976 | 23.378 |
| 2975 | 48.90 | 1.8633 | 815070 | 0.0202 | 205 | 9.839E-5 | 26.152 | 23.537 |
| 2975 | 49.42 | 1.8734 | 815172 | 0.0205 | 208 | 9.868E-5 | 26.347 | 23.712 |
| 2975 | 49.98 | 1.8838 | 815278 | 0.0101 | 103 | 9.856E-5 | 26.545 | 23.890 |
| 2975 | 50.54 | 1.8943 | 815383 | 0.0101 | 102 | 9.900E-5 | 26.743 | 24.069 |
| 2975 | 51.08 | 1.9043 | 815485 | 0.0101 | 101 | 9.977E-5 | 26.942 | 24.248 |
| 2975 | 51.61 | 1.9140 | 815583 | 0.0101 | 100 | 1.008E-4 | 27.142 | 24.427 |
| 2975 | 52.17 | 1.9241 | 815680 | 0.0100 | 98 | 1.022E-4 | 27.341 | 24.607 |
| 2975 | 52.75 | 1.9342 | 815778 | 0.0100 | 96 | 1.040E-4 | 27.546 | 24.792 |
| 2975 | 53.33 | 1.9443 | 815875 | 0.0101 | 96 | 1.057E-4 | 27.755 | 24.980 |
| 2975 | 53.91 | 1.9543 | 815969 | 0.0101 | 94 | 1.073E-4 | 27.966 | 25.169 |
| 2975 | 54.51 | 1.9644 | 816062 | 0.0101 | 93 | 1.091E-4 | 28.182 | 25.364 |
| 2975 | 55.14 | 1.9748 | 816156 | 0.0102 | 92 | 1.111E-4 | 28.399 | 25.559 |
| 2975 | 55.75 | 1.9849 | 816245 | 0.0102 | 90 | 1.126E-4 | 28.622 | 25.760 |
| 2975 | 56.38 | 1.9951 | 816335 | 0.0102 | 89 | 1.144E-4 | 28.846 | 25.961 |
| 2975 | 57.03 | 2.0053 | 816424 | 0.0102 | 87 | 1.164E-4 | 29.072 | 26.165 |
| 2975 | 57.67 | 2.0154 | 816510 | 0.0102 | 86 | 1.186E-4 | 29.303 | 26.372 |
| 2975 | 58.34 | 2.0256 | 816595 | 0.0101 | 83 | 1.214E-4 | 29.537 | 26.583 |
| 2975 | 59.02 | 2.0360 | 816680 | 0.0101 | 81 | 1.245E-4 | 29.772 | 26.795 |
| 2975 | 59.69 | 2.0461 | 816758 | 0.0101 | 79 | 1.277E-4 | 30.010 | 27.009 |
| 2975 | 60.36 | 2.0559 | 816834 | 0.0101 | 76 | 1.313E-4 | 30.249 | 27.224 |
| 2975 | 61.06 | 2.0660 | 816910 | 0.0101 | 74 | 1.355E-4 | 30.489 | 27.440 |
| 2975 | 61.77 | 2.0761 | 816983 | 0.0101 | 72 | 1.397E-4 | 30.734 | 27.660 |
| 2975 | 62.48 | 2.0860 | 817053 | 0.0101 | 70 | 1.448E-4 | 30.989 | 27.889 |
| 2975 | 63.23 | 2.0964 | 817124 | 0.0102 | 67 | 1.513E-4 | 31.242 | 28.117 |
| 2975 | 63.98 | 2.1066 | 817190 | 0.0102 | 65 | 1.576E-4 | 31.503 | 28.352 |
| 2975 | 64.73 | 2.1167 | 817252 | 0.0102 | 63 | 1.634E-4 | 31.768 | 28.591 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in]^0.5) |
|--------------|--------|-----------|--------|------------|----|-------------------|--------|-------------------------|
| 2975 | 65.52 | 2.1270 | 817312 | 0.0102 | 60 | 1.694E-4 | 32.033 | 28.829 |
| 2975 | 66.31 | 2.1372 | 817371 | 0.0102 | 58 | 1.758E-4 | 32.303 | 29.072 |
| 2975 | 67.09 | 2.1472 | 817428 | 0.0102 | 56 | 1.826E-4 | 32.582 | 29.323 * |
| 2975 | 67.93 | 2.1577 | 817485 | 0.0102 | 54 | 1.885E-4 | 32.855 | 29.569 * |
| 2975 | 68.74 | 2.1677 | 817535 | 0.0102 | 52 | 1.954E-4 | 33.146 | 29.831 * |
| 2975 | 69.61 | 2.1781 | 817586 | 0.0102 | 50 | 2.049E-4 | 33.427 | 30.084 * |
| 2975 | 70.44 | 2.1880 | 817637 | 0.0101 | 46 | 2.184E-4 | 33.725 | 30.352 * |
| 2975 | 71.33 | 2.1984 | 817684 | 0.0101 | 44 | 2.328E-4 | 34.015 | 30.613 * |
| 2975 | 72.21 | 2.2085 | 817725 | 0.0100 | 41 | 2.481E-4 | 34.310 | 30.878 * |
| 2975 | 73.06 | 2.2181 | 817760 | 0.0101 | 38 | 2.638E-4 | 34.610 | 31.148 * |
| 2975 | 73.96 | 2.2281 | 817798 | 0.0100 | 36 | 2.771E-4 | 34.907 | 31.415 * |
| 2975 | 74.88 | 2.2381 | 817833 | 0.0101 | 35 | 2.878E-4 | 35.222 | 31.699 * |
| 2975 | 75.85 | 2.2485 | 817867 | 0.0102 | 34 | 3.001E-4 | 35.536 | 31.982 * |
| 2975 | 76.81 | 2.2587 | 817902 | 0.0102 | 32 | 3.184E-4 | 35.868 | 32.280 * |
| 2975 | 77.82 | 2.2691 | 817935 | 0.0101 | 30 | 3.382E-4 | 36.197 | 32.576 * |
| 2975 | 78.84 | 2.2794 | 817963 | 0.0101 | 28 | 3.657E-4 | 36.529 | 32.874 * |
| 2975 | 79.82 | 2.2892 | 817989 | 0.0102 | 26 | 3.999E-4 | 36.860 | 33.171 * |
| 2975 | 80.81 | 2.2988 | 818014 | 0.0101 | 23 | 4.380E-4 | 37.203 | 33.481 * |
| 2975 | 81.90 | 2.3094 | 818036 | 0.0101 | 22 | 4.763E-4 | 37.549 | 33.791 * |
| 2975 | 83.01 | 2.3199 | 818057 | 0.0102 | 20 | 5.209E-4 | 37.902 | 34.107 * |
| 2975 | 84.06 | 2.3296 | 818075 | 0.0102 | 18 | 5.681E-4 | 38.273 | 34.442 * |
| 2975 | 85.21 | 2.3400 | 818093 | 0.0101 | 17 | 6.235E-4 | 38.630 | 34.762 * |
| 2974 | 86.35 | 2.3502 | 818109 | 0.0100 | 15 | 6.847E-4 | 39.008 | 35.102 * |
| 2974 | 87.51 | 2.3603 | 818123 | 0.0101 | 14 | 7.532E-4 | 39.371 | 35.428 * |
| 2974 | 88.61 | 2.3698 | 818135 | 0.0101 | 13 | 8.124E-4 | 39.752 | 35.769 * |
| 2974 | 89.81 | 2.3800 | 818147 | 0.0102 | 12 | 8.799E-4 | 40.137 | 36.117 * |
| 2974 | 91.07 | 2.3904 | 818158 | 0.0106 | 11 | 9.708E-4 | 40.531 | 36.467 * |
| 2974 | 92.35 | 2.4007 | 818169 | 0.0103 | 10 | 1.072E-3 | 40.948 | 36.844 * |
| 2973 | 93.69 | 2.4114 | 818179 | 0.0104 | 9 | 1.228E-3 | 41.405 | 37.245 * |
| 2973 | 95.29 | 2.4238 | 818188 | 0.0105 | 8 | 1.521E-3 | 41.715 | 37.519 * |
| 2964 | 96.28 | 2.4313 | 818194 | 0.0109 | 6 | 1.970E-3 | 42.203 | 37.944 * |
| 2964 | 97.75 | 2.4424 | 818200 | 0.0110 | 5 | 2.460E-3 | 42.543 | 38.241 * |
| 2965 | 99.26 | 2.4534 | 818204 | 0.0239 | 7 | 3.416E-3 | 42.984 | 38.616 * |
| 2954 | 101.07 | 2.4663 | 818207 | 0.0239 | 7 | 3.419E-3 | 43.391 | 38.960 * |
| | 102.64 | 2.4773 | 818211 | | | | | |

Automated Fatigue Crack
Growth Rate Analysis

| | | | |
|-----------------|--------------|---------------|------|
| Test ID | 5086-FCG-2 | Geometry | C(T) |
| Contract | SSC 10624-01 | Orientation | T-L |
| Material | 5086-H116 | Yield (ksi) | 27.0 |
| Temperature (F) | 75 | Modulus (Msi) | 10.8 |
| Environment | RH = 40% | | |

Specimen Dimensions (in)

| | | | |
|---------------|-------|-------------|-------|
| Thickness | 0.496 | Height | 2.400 |
| Net Thickness | 0.496 | Notch Depth | 1.000 |
| Width | 4.000 | Gage Length | 0.500 |

Precrack Parameters

| | | | |
|--------------|-------|--------------------|------|
| Pmax (lbs) | 779.0 | Stress Ratio | 0.10 |
| Final a (in) | 1.050 | Kmax (ksi sqr[in]) | 4.00 |

Test Parameters

| EvBP | Freq | Pmax | R | Ai | Kmaxi | C | DKi |
|--------|-------|------|------|-------|-------|------|------|
| 23.356 | 10.00 | 0 | 0.10 | 1.130 | 3.00 | 4.00 | 0.00 |
| 31.296 | 10.00 | 0 | 0.10 | 1.446 | 10.60 | 2.00 | 0.00 |
| 49.484 | 5.00 | 2840 | 0.10 | 0.000 | 0.00 | 0.00 | 0.00 |

| K Coeff | C Coeff |
|---------|----------|
| .886 | 1.00098 |
| 4.64 | -4.66951 |
| -13.32 | 18.4601 |
| 14.72 | -236.825 |
| -5.6 | 1214.88 |
| . | -2143.57 |

Visual Observations

| EvB/P | Crack(EvB/P) | Crack(visual) | Error | CAF |
|---------|--------------|---------------|--------|-------|
| 20.433 | 0.988 | 1.001 | 0.013 | 1.013 |
| 21.842 | 1.061 | 1.060 | -0.001 | 1.009 |
| 23.496 | 1.139 | 1.135 | -0.004 | 1.005 |
| 27.422 | 1.302 | 1.300 | -0.002 | 0.997 |
| 31.212 | 1.434 | 1.430 | -0.004 | 0.990 |
| 41.599 | 1.716 | 1.710 | -0.006 | 0.976 |
| 49.143 | 1.870 | 1.870 | 0.000 | 0.968 |
| 103.926 | 2.466 | 2.470 | 0.004 | 0.939 |

Comments

Date of test: 8/21/2006
Waveform Type Sine

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in]^0.5) |
|--------------|-------|-----------|---------|------------|--------|-------------------|-------|-------------------------|
| | 23.36 | 1.1330 | 49863 | | | | | |
| 558 | 23.46 | 1.1378 | 135356 | 0.0089 | 154118 | 5.807E-8 | 3.031 | 2.728 |
| 566 | 23.55 | 1.1419 | 203981 | 0.0088 | 139929 | 6.284E-8 | 3.092 | 2.783 |
| 576 | 23.66 | 1.1466 | 275285 | 0.0048 | 68985 | 6.983E-8 | 3.153 | 2.838 |
| 586 | 23.77 | 1.1518 | 345898 | 0.0048 | 64956 | 7.576E-8 | 3.215 | 2.894 |
| 596 | 23.88 | 1.1565 | 403283 | 0.0050 | 63113 | 7.933E-8 | 3.285 | 2.957 |
| 607 | 23.99 | 1.1616 | 463772 | 0.0050 | 59559 | 8.343E-8 | 3.354 | 3.019 |
| 618 | 24.11 | 1.1669 | 525094 | 0.0049 | 55679 | 8.730E-8 | 3.424 | 3.082 |
| 629 | 24.22 | 1.1716 | 582657 | 0.0050 | 53373 | 9.266E-8 | 3.497 | 3.147 |
| 639 | 24.33 | 1.1765 | 632641 | 0.0049 | 49918 | 9.866E-8 | 3.566 | 3.209 |
| 650 | 24.44 | 1.1812 | 679974 | 0.0048 | 46008 | 1.058E-7 | 3.641 | 3.277 |
| 662 | 24.56 | 1.1863 | 723519 | 0.0047 | 42284 | 1.130E-7 | 3.712 | 3.341 |
| 673 | 24.66 | 1.1908 | 763279 | 0.0047 | 40012 | 1.187E-7 | 3.788 | 3.410 |
| 684 | 24.77 | 1.1955 | 801144 | 0.0047 | 37930 | 1.247E-7 | 3.862 | 3.476 |
| 695 | 24.88 | 1.2000 | 836361 | 0.0047 | 35722 | 1.300E-7 | 3.939 | 3.545 |
| 707 | 24.99 | 1.2048 | 872715 | 0.0047 | 33791 | 1.380E-7 | 4.018 | 3.616 |
| 719 | 25.11 | 1.2097 | 907554 | 0.0048 | 32126 | 1.485E-7 | 4.096 | 3.687 |
| 731 | 25.21 | 1.2142 | 937848 | 0.0048 | 30296 | 1.605E-7 | 4.180 | 3.762 |
| 743 | 25.33 | 1.2190 | 966024 | 0.0047 | 27670 | 1.734E-7 | 4.265 | 3.839 |
| 757 | 25.45 | 1.2241 | 993897 | 0.0046 | 25096 | 1.885E-7 | 4.351 | 3.916 |
| 770 | 25.57 | 1.2288 | 1018135 | 0.0047 | 23440 | 2.042E-7 | 4.437 | 3.994 |
| 782 | 25.67 | 1.2331 | 1038737 | 0.0048 | 21653 | 2.222E-7 | 4.523 | 4.071 |
| 794 | 25.78 | 1.2375 | 1058127 | 0.0047 | 19430 | 2.446E-7 | 4.613 | 4.152 |
| 808 | 25.90 | 1.2426 | 1078487 | 0.0048 | 17588 | 2.773E-7 | 4.704 | 4.233 |
| 822 | 26.03 | 1.2476 | 1095939 | 0.0048 | 15989 | 3.137E-7 | 4.803 | 4.323 |
| 837 | 26.15 | 1.2524 | 1110479 | 0.0047 | 14433 | 3.475E-7 | 4.902 | 4.412 |
| 851 | 26.27 | 1.2573 | 1123661 | 0.0046 | 12513 | 3.842E-7 | 4.999 | 4.499 |
| 865 | 26.38 | 1.2617 | 1134673 | 0.0046 | 11061 | 4.287E-7 | 5.095 | 4.586 |
| 878 | 26.49 | 1.2659 | 1144724 | 0.0047 | 9962 | 4.813E-7 | 5.191 | 4.672 |
| 892 | 26.60 | 1.2702 | 1153563 | 0.0046 | 8838 | 5.366E-7 | 5.294 | 4.765 |
| 908 | 26.73 | 1.2754 | 1162305 | 0.0046 | 7945 | 6.083E-7 | 5.400 | 4.860 |
| 925 | 26.86 | 1.2805 | 1170252 | 0.0048 | 7201 | 6.878E-7 | 5.509 | 4.958 |
| 939 | 26.98 | 1.2849 | 1176687 | 0.0049 | 6575 | 7.713E-7 | 5.622 | 5.059 |
| 955 | 27.09 | 1.2895 | 1182340 | 0.0049 | 5737 | 8.771E-7 | 5.734 | 5.161 |
| 972 | 27.23 | 1.2945 | 1187929 | 0.0047 | 5002 | 9.908E-7 | 5.852 | 5.267 |
| 990 | 27.36 | 1.2997 | 1193010 | 0.0048 | 4526 | 1.108E-6 | 5.974 | 5.376 |
| 1007 | 27.49 | 1.3045 | 1196725 | 0.0048 | 4131 | 1.199E-6 | 6.093 | 5.483 |
| 1022 | 27.60 | 1.3087 | 1200264 | 0.0048 | 3677 | 1.311E-6 | 6.216 | 5.594 |
| 1040 | 27.73 | 1.3135 | 1203842 | 0.0046 | 3229 | 1.443E-6 | 6.336 | 5.703 |
| 1058 | 27.86 | 1.3182 | 1207126 | 0.0047 | 3026 | 1.599E-6 | 6.464 | 5.817 |
| 1076 | 27.99 | 1.3232 | 1209988 | 0.0048 | 2784 | 1.781E-6 | 6.593 | 5.933 |
| 1093 | 28.11 | 1.3276 | 1212383 | 0.0047 | 2483 | 1.960E-6 | 6.729 | 6.056 |
| 1113 | 28.25 | 1.3327 | 1214883 | 0.0047 | 2213 | 2.193E-6 | 6.861 | 6.175 |
| 1132 | 28.38 | 1.3374 | 1216966 | 0.0047 | 2014 | 2.405E-6 | 6.998 | 6.298 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in]^0.5) |
|--------------|-------|-----------|---------|------------|------|-------------------|--------|-------------------------|
| 1149 | 28.50 | 1.3418 | 1218737 | 0.0049 | 1851 | 2.688E-6 | 7.138 | 6.424 |
| 1169 | 28.63 | 1.3466 | 1220404 | 0.0047 | 1632 | 2.975E-6 | 7.276 | 6.549 |
| 1189 | 28.77 | 1.3514 | 1222071 | 0.0047 | 1483 | 3.272E-6 | 7.431 | 6.688 |
| 1211 | 28.92 | 1.3568 | 1223487 | 0.0048 | 1366 | 3.580E-6 | 7.576 | 6.819 |
| 1231 | 29.04 | 1.3611 | 1224674 | 0.0048 | 1253 | 3.874E-6 | 7.733 | 6.960 |
| 1251 | 29.17 | 1.3656 | 1225864 | 0.0048 | 1139 | 4.201E-6 | 7.885 | 7.097 |
| 1272 | 29.31 | 1.3705 | 1226932 | 0.0047 | 1053 | 4.530E-6 | 8.038 | 7.234 |
| 1294 | 29.44 | 1.3751 | 1227924 | 0.0048 | 983 | 4.928E-6 | 8.205 | 7.385 |
| 1317 | 29.59 | 1.3801 | 1228906 | 0.0047 | 905 | 5.286E-6 | 8.372 | 7.535 |
| 1340 | 29.73 | 1.3851 | 1229802 | 0.0047 | 848 | 5.649E-6 | 8.542 | 7.688 |
| 1362 | 29.87 | 1.3898 | 1230570 | 0.0048 | 798 | 6.025E-6 | 8.707 | 7.837 |
| 1383 | 29.99 | 1.3939 | 1231292 | 0.0047 | 743 | 6.375E-6 | 8.883 | 7.995 |
| 1407 | 30.14 | 1.3989 | 1232017 | 0.0047 | 696 | 6.713E-6 | 9.055 | 8.150 |
| 1432 | 30.28 | 1.4038 | 1232709 | 0.0046 | 660 | 7.085E-6 | 9.236 | 8.312 |
| 1455 | 30.42 | 1.4085 | 1233365 | 0.0047 | 628 | 7.477E-6 | 9.425 | 8.483 |
| 1480 | 30.56 | 1.4131 | 1233978 | 0.0047 | 602 | 7.883E-6 | 9.606 | 8.645 |
| 1503 | 30.70 | 1.4177 | 1234527 | 0.0048 | 574 | 8.342E-6 | 9.795 | 8.815 |
| 1528 | 30.83 | 1.4221 | 1235058 | 0.0097 | 1099 | 8.808E-6 | 9.996 | 8.996 |
| 1556 | 30.99 | 1.4273 | 1235626 | 0.0104 | 1092 | 9.484E-6 | 10.199 | 9.179 |
| | 31.15 | 1.4325 | 1236150 | | | | | |
| | 31.30 | 1.4372 | 1236656 | | | | | |
| 1618 | 31.51 | 1.4440 | 1237333 | 0.0166 | 1602 | 1.036E-5 | 10.746 | 9.671 |
| 1640 | 31.82 | 1.4538 | 1238258 | 0.0191 | 1806 | 1.057E-5 | 10.930 | 9.837 |
| 1662 | 32.11 | 1.4631 | 1239139 | 0.0186 | 1711 | 1.087E-5 | 11.145 | 10.031 |
| 1683 | 32.41 | 1.4724 | 1239969 | 0.0096 | 819 | 1.170E-5 | 11.371 | 10.234 |
| 1708 | 32.74 | 1.4825 | 1240798 | 0.0095 | 780 | 1.230E-5 | 11.595 | 10.435 |
| 1731 | 33.06 | 1.4923 | 1241558 | 0.0096 | 743 | 1.294E-5 | 11.831 | 10.648 |
| 1755 | 33.37 | 1.5016 | 1242249 | 0.0096 | 707 | 1.356E-5 | 12.065 | 10.859 |
| 1778 | 33.69 | 1.5110 | 1242940 | 0.0095 | 665 | 1.423E-5 | 12.304 | 11.073 |
| 1802 | 34.01 | 1.5206 | 1243597 | 0.0095 | 634 | 1.491E-5 | 12.546 | 11.292 |
| 1827 | 34.34 | 1.5300 | 1244209 | 0.0095 | 610 | 1.564E-5 | 12.793 | 11.513 |
| 1851 | 34.67 | 1.5394 | 1244786 | 0.0095 | 580 | 1.636E-5 | 13.048 | 11.743 |
| 1876 | 35.01 | 1.5490 | 1245362 | 0.0095 | 558 | 1.708E-5 | 13.308 | 11.977 |
| 1902 | 35.36 | 1.5588 | 1245911 | 0.0095 | 536 | 1.777E-5 | 13.569 | 12.212 |
| 1927 | 35.69 | 1.5679 | 1246420 | 0.0095 | 513 | 1.851E-5 | 13.846 | 12.462 |
| 1954 | 36.05 | 1.5778 | 1246944 | 0.0095 | 490 | 1.944E-5 | 14.116 | 12.704 |
| 1980 | 36.40 | 1.5873 | 1247425 | 0.0095 | 467 | 2.045E-5 | 14.396 | 12.957 |
| 2006 | 36.75 | 1.5966 | 1247862 | 0.0096 | 445 | 2.158E-5 | 14.683 | 13.215 |
| 2033 | 37.11 | 1.6063 | 1248299 | 0.0096 | 420 | 2.285E-5 | 14.971 | 13.474 |
| 2060 | 37.49 | 1.6160 | 1248714 | 0.0096 | 399 | 2.407E-5 | 15.270 | 13.743 |
| 2088 | 37.86 | 1.6254 | 1249089 | 0.0096 | 379 | 2.530E-5 | 15.579 | 14.021 |
| 2117 | 38.24 | 1.6352 | 1249462 | 0.0095 | 358 | 2.654E-5 | 15.886 | 14.298 |
| 2145 | 38.62 | 1.6447 | 1249818 | 0.0096 | 341 | 2.800E-5 | 16.202 | 14.582 |
| 2173 | 38.99 | 1.6540 | 1250134 | 0.0096 | 328 | 2.933E-5 | 16.515 | 14.863 |
| 2201 | 39.37 | 1.6632 | 1250447 | 0.0096 | 311 | 3.091E-5 | 16.851 | 15.166 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^0.5) | deltaK |
|--------------|-------|-----------|---------|------------|-----|-------------------|-----------------------|--------|
| 2232 | 39.79 | 1.6734 | 1250760 | 0.0096 | 294 | 3.264E-5 | 17.182 | 15.464 |
| 2262 | 40.20 | 1.6832 | 1251059 | 0.0096 | 280 | 3.437E-5 | 17.535 | 15.782 |
| 2292 | 40.61 | 1.6929 | 1251329 | 0.0097 | 266 | 3.642E-5 | 17.885 | 16.097 |
| 2322 | 41.01 | 1.7022 | 1251580 | 0.0096 | 251 | 3.849E-5 | 18.234 | 16.411 |
| 2352 | 41.41 | 1.7115 | 1251815 | 0.0096 | 237 | 4.070E-5 | 18.595 | 16.736 |
| 2383 | 41.85 | 1.7212 | 1252042 | 0.0096 | 224 | 4.291E-5 | 18.962 | 17.066 |
| 2415 | 42.28 | 1.7311 | 1252265 | 0.0096 | 212 | 4.524E-5 | 19.344 | 17.410 |
| 2447 | 42.73 | 1.7409 | 1252478 | 0.0096 | 202 | 4.757E-5 | 19.732 | 17.759 |
| 2479 | 43.16 | 1.7503 | 1252670 | 0.0096 | 192 | 5.022E-5 | 20.122 | 18.110 |
| 2511 | 43.60 | 1.7597 | 1252853 | 0.0097 | 181 | 5.337E-5 | 20.514 | 18.463 |
| 2543 | 44.04 | 1.7691 | 1253027 | 0.0096 | 170 | 5.657E-5 | 20.924 | 18.832 |
| 2577 | 44.51 | 1.7790 | 1253193 | 0.0096 | 161 | 6.015E-5 | 21.342 | 19.208 |
| 2612 | 44.99 | 1.7891 | 1253353 | 0.0096 | 151 | 6.409E-5 | 21.766 | 19.590 |
| 2645 | 45.45 | 1.7984 | 1253498 | 0.0097 | 143 | 6.808E-5 | 22.209 | 19.988 |
| 2679 | 45.93 | 1.8080 | 1253633 | 0.0096 | 134 | 7.165E-5 | 22.640 | 20.376 |
| 2714 | 46.41 | 1.8176 | 1253761 | 0.0095 | 126 | 7.550E-5 | 23.090 | 20.781 |
| 2749 | 46.90 | 1.8272 | 1253883 | 0.0096 | 120 | 7.974E-5 | 23.535 | 21.182 |
| 2782 | 47.37 | 1.8364 | 1253999 | 0.0096 | 113 | 8.427E-5 | 24.001 | 21.601 |
| 2818 | 47.87 | 1.8460 | 1254110 | 0.0194 | 218 | 8.922E-5 | 24.471 | 22.024 |
| 2855 | 48.40 | 1.8559 | 1254217 | 0.0195 | 203 | 9.599E-5 | 24.953 | 22.458 |
| | 48.91 | 1.8655 | 1254313 | | | | | |
| | 49.48 | 1.8760 | 1254424 | | | | | |
| 2840 | 49.97 | 1.8847 | 1254526 | 0.0184 | 213 | 8.662E-5 | 25.363 | 22.827 |
| 2840 | 50.51 | 1.8944 | 1254637 | 0.0193 | 217 | 8.887E-5 | 25.533 | 22.979 |
| 2840 | 51.05 | 1.9040 | 1254743 | 0.0193 | 209 | 9.225E-5 | 25.715 | 23.144 |
| 2840 | 51.61 | 1.9137 | 1254846 | 0.0097 | 104 | 9.313E-5 | 25.900 | 23.310 |
| 2840 | 52.19 | 1.9236 | 1254948 | 0.0096 | 101 | 9.494E-5 | 26.086 | 23.478 |
| 2840 | 52.77 | 1.9333 | 1255051 | 0.0097 | 99 | 9.694E-5 | 26.274 | 23.647 |
| 2840 | 53.33 | 1.9427 | 1255149 | 0.0097 | 98 | 9.885E-5 | 26.463 | 23.816 |
| 2840 | 53.91 | 1.9522 | 1255243 | 0.0097 | 96 | 1.009E-4 | 26.655 | 23.990 |
| 2840 | 54.53 | 1.9621 | 1255338 | 0.0097 | 93 | 1.039E-4 | 26.850 | 24.165 |
| 2840 | 55.14 | 1.9719 | 1255432 | 0.0097 | 91 | 1.068E-4 | 27.050 | 24.345 |
| 2840 | 55.76 | 1.9816 | 1255522 | 0.0098 | 90 | 1.092E-4 | 27.251 | 24.526 |
| 2840 | 56.39 | 1.9913 | 1255608 | 0.0097 | 87 | 1.113E-4 | 27.455 | 24.709 |
| 2840 | 57.03 | 2.0011 | 1255694 | 0.0097 | 85 | 1.142E-4 | 27.662 | 24.896 |
| 2840 | 57.69 | 2.0110 | 1255780 | 0.0097 | 83 | 1.166E-4 | 27.868 | 25.081 |
| 2840 | 58.33 | 2.0204 | 1255862 | 0.0097 | 81 | 1.193E-4 | 28.082 | 25.274 |
| 2840 | 59.00 | 2.0303 | 1255940 | 0.0097 | 79 | 1.227E-4 | 28.288 | 25.459 |
| 2840 | 59.65 | 2.0396 | 1256017 | 0.0097 | 76 | 1.265E-4 | 28.508 | 25.657 |
| 2840 | 60.36 | 2.0495 | 1256094 | 0.0097 | 74 | 1.307E-4 | 28.726 | 25.853 |
| 2840 | 61.07 | 2.0595 | 1256168 | 0.0097 | 73 | 1.340E-4 | 28.948 | 26.053 |
| 2840 | 61.77 | 2.0690 | 1256238 | 0.0098 | 72 | 1.372E-4 | 29.175 | 26.257 |
| 2840 | 62.49 | 2.0787 | 1256306 | 0.0098 | 70 | 1.401E-4 | 29.402 | 26.461 |
| 2840 | 63.23 | 2.0886 | 1256376 | 0.0098 | 67 | 1.438E-4 | 29.637 | 26.673 |
| 2840 | 64.00 | 2.0986 | 1256448 | 0.0098 | 65 | 1.492E-4 | 29.870 | 26.883 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^0.5) | deltaK |
|--------------|--------|-----------|---------|------------|----|-------------------|-----------------------|----------|
| 2840 | 64.75 | 2.1083 | 1256511 | 0.0099 | 64 | 1.553E-4 | 30.113 | 27.101 |
| 2840 | 65.52 | 2.1180 | 1256571 | 0.0098 | 61 | 1.616E-4 | 30.350 | 27.314 |
| 2840 | 66.29 | 2.1276 | 1256628 | 0.0097 | 58 | 1.688E-4 | 30.603 | 27.542 |
| 2840 | 67.14 | 2.1380 | 1256688 | 0.0098 | 55 | 1.765E-4 | 30.841 | 27.757 |
| 2840 | 67.90 | 2.1472 | 1256741 | 0.0097 | 53 | 1.836E-4 | 31.102 | 27.991 |
| 2840 | 68.73 | 2.1571 | 1256793 | 0.0098 | 52 | 1.901E-4 | 31.349 | 28.214 |
| 2840 | 69.57 | 2.1668 | 1256841 | 0.0097 | 50 | 1.967E-4 | 31.601 | 28.440 |
| 2840 | 70.37 | 2.1760 | 1256886 | 0.0097 | 48 | 2.017E-4 | 31.868 | 28.680 |
| 2840 | 71.27 | 2.1861 | 1256937 | 0.0097 | 47 | 2.058E-4 | 32.130 | 28.916 |
| 2840 | 72.17 | 2.1962 | 1256985 | 0.0098 | 46 | 2.098E-4 | 32.400 | 29.159 * |
| 2840 | 73.04 | 2.2056 | 1257030 | 0.0099 | 45 | 2.171E-4 | 32.680 | 29.411 * |
| 2840 | 73.96 | 2.2155 | 1257076 | 0.0098 | 43 | 2.274E-4 | 32.953 | 29.657 * |
| 2840 | 74.89 | 2.2253 | 1257118 | 0.0097 | 41 | 2.386E-4 | 33.239 | 29.915 * |
| 2840 | 75.85 | 2.2353 | 1257157 | 0.0098 | 39 | 2.508E-4 | 33.523 | 30.170 * |
| 2840 | 76.79 | 2.2449 | 1257195 | 0.0099 | 37 | 2.673E-4 | 33.816 | 30.434 * |
| 2840 | 77.77 | 2.2547 | 1257231 | 0.0099 | 35 | 2.830E-4 | 34.111 | 30.699 * |
| 2840 | 78.78 | 2.2646 | 1257266 | 0.0099 | 33 | 2.992E-4 | 34.421 | 30.978 * |
| 2840 | 79.87 | 2.2752 | 1257298 | 0.0099 | 32 | 3.142E-4 | 34.721 | 31.247 * |
| 2840 | 80.85 | 2.2845 | 1257327 | 0.0099 | 30 | 3.275E-4 | 35.046 | 31.540 * |
| 2840 | 81.94 | 2.2946 | 1257357 | 0.0098 | 29 | 3.408E-4 | 35.349 | 31.812 * |
| 2840 | 82.98 | 2.3041 | 1257385 | 0.0098 | 27 | 3.564E-4 | 35.677 | 32.107 * |
| 2840 | 84.10 | 2.3142 | 1257413 | 0.0099 | 26 | 3.815E-4 | 35.991 | 32.390 * |
| 2840 | 85.17 | 2.3237 | 1257438 | 0.0098 | 24 | 4.116E-4 | 36.327 | 32.692 * |
| 2840 | 86.32 | 2.3337 | 1257461 | 0.0099 | 23 | 4.476E-4 | 36.656 | 32.989 * |
| 2840 | 87.49 | 2.3436 | 1257482 | 0.0100 | 21 | 4.849E-4 | 37.002 | 33.299 * |
| 2840 | 88.68 | 2.3536 | 1257502 | 0.0099 | 20 | 5.150E-4 | 37.350 | 33.612 * |
| 2840 | 89.89 | 2.3635 | 1257520 | 0.0099 | 18 | 5.440E-4 | 37.715 | 33.941 * |
| 2840 | 91.19 | 2.3740 | 1257538 | 0.0098 | 17 | 5.778E-4 | 38.061 | 34.251 * |
| 2839 | 92.36 | 2.3832 | 1257555 | 0.0098 | 16 | 6.087E-4 | 38.432 | 34.584 * |
| 2839 | 93.61 | 2.3929 | 1257570 | 0.0098 | 15 | 6.389E-4 | 38.787 | 34.904 * |
| 2839 | 94.90 | 2.4026 | 1257584 | 0.0097 | 14 | 6.857E-4 | 39.160 | 35.238 * |
| 2839 | 96.23 | 2.4126 | 1257599 | 0.0098 | 13 | 7.498E-4 | 39.533 | 35.573 * |
| 2839 | 97.54 | 2.4221 | 1257612 | 0.0099 | 12 | 8.137E-4 | 39.924 | 35.923 * |
| 2838 | 98.95 | 2.4322 | 1257623 | 0.0098 | 11 | 8.917E-4 | 40.317 | 36.277 * |
| 2839 | 100.38 | 2.4423 | 1257634 | 0.0103 | 11 | 9.812E-4 | 40.716 | 36.633 * |
| 2838 | 101.81 | 2.4521 | 1257644 | 0.0101 | 10 | 1.055E-3 | 41.118 | 36.994 * |
| 2838 | 103.19 | 2.4614 | 1257652 | 0.0102 | 9 | 1.150E-3 | 41.594 | 37.418 * |
| 2837 | 105.14 | 2.4746 | 1257663 | 0.0105 | 8 | 1.442E-3 | 41.890 | 37.671 * |
| 2828 | 106.32 | 2.4825 | 1257670 | 0.0107 | 7 | 1.894E-3 | 42.358 | 38.078 * |
| 2821 | 107.95 | 2.4932 | 1257676 | 0.0109 | 6 | 2.505E-3 | 42.725 | 38.392 * |
| 2821 | 109.84 | 2.5053 | 1257680 | 0.0103 | 4 | 2.960E-3 | 43.172 | 38.778 * |
| 2822 | 111.60 | 2.5163 | 1257683 | 0.0215 | 6 | 3.584E-3 | 43.668 | 39.215 * |
| 2819 | 113.31 | 2.5268 | 1257686 | 0.0202 | 6 | 3.370E-3 | 44.020 | 39.503 * |
| | 114.94 | 2.5365 | 1257689 | | | | | |

Automated Fatigue Crack
Growth Rate Analysis

| | | | |
|-----------------|--------------|---------------|------|
| Test ID | 5086-FCG-3 | Geometry | C(T) |
| Contract | SSC 10624-01 | Orientation | T-L |
| Material | 5086-H116 | Yield (ksi) | 27.0 |
| Temperature (F) | 75 | Modulus (Msi) | 10.5 |
| Environment | Sea Water | | |

Specimen Dimensions (in)

| | | | |
|---------------|-------|-------------|-------|
| Thickness | 0.496 | Height | 2.400 |
| Net Thickness | 0.496 | Notch Depth | 1.000 |
| Width | 4.001 | Gage Length | 0.500 |

Precrack Parameters

| | | | |
|--------------|-------|--------------------|------|
| Pmax (lbs) | 877.0 | Stress Ratio | 0.10 |
| Final a (in) | 1.050 | Kmax (ksi sqr[in]) | 4.50 |

Test Parameters

| EvBP | Freq | Pmax | R | Ai | Kmaxi | C | DKi |
|--------|------|------|------|-------|-------|------|------|
| 24.592 | 5.00 | 0 | 0.10 | 1.185 | 2.90 | 4.00 | 0.00 |
| 32.530 | 5.00 | 0 | 0.10 | 1.489 | 9.65 | 2.00 | 0.00 |
| 53.965 | 5.00 | 2630 | 0.10 | 0.000 | 0.00 | 0.00 | 0.00 |

| K Coeff | C Coeff |
|---------|----------|
| .886 | 1.00098 |
| 4.64 | -4.66951 |
| -13.32 | 18.4601 |
| 14.72 | -236.825 |
| -5.6 | 1214.88 |
| . | -2143.57 |

Visual Observations

| EvB/P | Crack(EvB/P) | Crack(visual) | Error | CAF |
|---------|--------------|---------------|--------|-------|
| 20.713 | 1.016 | 1.002 | -0.014 | 1.024 |
| 21.842 | 1.074 | 1.050 | -0.024 | 1.021 |
| 23.158 | 1.137 | 1.150 | 0.013 | 1.017 |
| 23.897 | 1.170 | 1.200 | 0.030 | 1.015 |
| 28.441 | 1.352 | 1.340 | -0.012 | 1.006 |
| 32.409 | 1.484 | 1.500 | 0.016 | 0.999 |
| 44.737 | 1.794 | 1.790 | -0.004 | 0.982 |
| 53.608 | 1.957 | 1.950 | -0.007 | 0.974 |
| 107.893 | 2.499 | 2.500 | 0.001 | 0.947 |

Comments

Date of test: 8/26/2006
Waveform Type Sine

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in]^0.5) |
|--------------|-------|-----------|--------|------------|-------|-------------------|-------|-------------------------|
| | 24.59 | 1.2004 | 6238 | | | | | |
| 521 | 24.64 | 1.2024 | 25700 | 0.0069 | 58740 | 1.173E-7 | 2.973 | 2.676 |
| 530 | 24.75 | 1.2073 | 64978 | 0.0098 | 82088 | 1.189E-7 | 3.016 | 2.714 |
| 539 | 24.87 | 1.2121 | 107788 | 0.0044 | 34574 | 1.285E-7 | 3.078 | 2.770 |
| 548 | 24.98 | 1.2169 | 145913 | 0.0048 | 36526 | 1.316E-7 | 3.140 | 2.826 |
| 558 | 25.09 | 1.2217 | 177197 | 0.0048 | 33598 | 1.436E-7 | 3.205 | 2.884 |
| 567 | 25.21 | 1.2266 | 213681 | 0.0048 | 30599 | 1.602E-7 | 3.267 | 2.940 |
| 576 | 25.32 | 1.2312 | 244856 | 0.0048 | 28381 | 1.739E-7 | 3.337 | 3.003 |
| 587 | 25.44 | 1.2363 | 266568 | 0.0048 | 27206 | 1.809E-7 | 3.401 | 3.061 |
| 597 | 25.56 | 1.2410 | 291381 | 0.0047 | 25004 | 1.909E-7 | 3.472 | 3.125 |
| 607 | 25.67 | 1.2457 | 316197 | 0.0048 | 23524 | 1.984E-7 | 3.542 | 3.188 |
| 617 | 25.79 | 1.2504 | 340435 | 0.0047 | 23461 | 1.989E-7 | 3.610 | 3.249 |
| 627 | 25.90 | 1.2549 | 363703 | 0.0048 | 22395 | 2.115E-7 | 3.684 | 3.316 |
| 638 | 26.02 | 1.2598 | 386002 | 0.0048 | 21006 | 2.281E-7 | 3.755 | 3.379 |
| 649 | 26.14 | 1.2645 | 407331 | 0.0047 | 19422 | 2.490E-7 | 3.836 | 3.452 |
| 661 | 26.27 | 1.2697 | 425752 | 0.0047 | 17844 | 2.718E-7 | 3.911 | 3.520 |
| 672 | 26.39 | 1.2742 | 442231 | 0.0047 | 16403 | 2.926E-7 | 3.990 | 3.591 |
| 682 | 26.50 | 1.2786 | 456964 | 0.0047 | 15019 | 3.127E-7 | 4.069 | 3.662 |
| 694 | 26.62 | 1.2833 | 470767 | 0.0046 | 14017 | 3.302E-7 | 4.146 | 3.731 |
| 705 | 26.74 | 1.2879 | 484417 | 0.0046 | 13132 | 3.533E-7 | 4.229 | 3.806 |
| 717 | 26.86 | 1.2926 | 497446 | 0.0047 | 12331 | 3.815E-7 | 4.312 | 3.881 |
| 729 | 26.98 | 1.2973 | 509854 | 0.0047 | 11603 | 4.150E-7 | 4.398 | 3.958 |
| 742 | 27.10 | 1.3021 | 521022 | 0.0048 | 10735 | 4.554E-7 | 4.488 | 4.039 |
| 755 | 27.23 | 1.3070 | 530950 | 0.0048 | 9888 | 4.942E-7 | 4.579 | 4.121 |
| 768 | 27.36 | 1.3118 | 540382 | 0.0048 | 9078 | 5.322E-7 | 4.674 | 4.206 |
| 781 | 27.49 | 1.3166 | 548824 | 0.0047 | 8289 | 5.714E-7 | 4.767 | 4.291 |
| 794 | 27.61 | 1.3212 | 556771 | 0.0047 | 7703 | 6.117E-7 | 4.863 | 4.377 |
| 807 | 27.73 | 1.3258 | 564321 | 0.0047 | 7148 | 6.591E-7 | 4.957 | 4.461 |
| 820 | 27.86 | 1.3303 | 570755 | 0.0046 | 6588 | 7.085E-7 | 5.056 | 4.551 |
| 834 | 27.98 | 1.3350 | 577170 | 0.0047 | 6152 | 7.734E-7 | 5.155 | 4.639 |
| 849 | 28.11 | 1.3399 | 583268 | 0.0046 | 5826 | 8.108E-7 | 5.256 | 4.730 |
| 862 | 28.24 | 1.3443 | 588349 | 0.0047 | 5601 | 8.475E-7 | 5.367 | 4.830 |
| 878 | 28.38 | 1.3495 | 593684 | 0.0048 | 5251 | 9.017E-7 | 5.465 | 4.919 |
| 892 | 28.50 | 1.3537 | 599276 | 0.0048 | 4845 | 9.785E-7 | 5.584 | 5.025 |
| 907 | 28.64 | 1.3588 | 604359 | 0.0048 | 4513 | 1.093E-6 | 5.694 | 5.125 |
| 924 | 28.78 | 1.3638 | 608677 | 0.0047 | 4106 | 1.242E-6 | 5.811 | 5.230 |
| 939 | 28.91 | 1.3686 | 612336 | 0.0048 | 3629 | 1.397E-6 | 5.930 | 5.337 |
| 955 | 29.04 | 1.3731 | 615425 | 0.0047 | 3194 | 1.532E-6 | 6.048 | 5.443 |
| 971 | 29.18 | 1.3778 | 618320 | 0.0047 | 2861 | 1.680E-6 | 6.169 | 5.553 |
| 988 | 29.31 | 1.3826 | 621051 | 0.0047 | 2598 | 1.833E-6 | 6.290 | 5.661 |
| 1004 | 29.45 | 1.3872 | 623523 | 0.0047 | 2406 | 1.973E-6 | 6.421 | 5.779 |
| 1022 | 29.59 | 1.3921 | 625840 | 0.0048 | 2243 | 2.139E-6 | 6.544 | 5.890 |
| 1039 | 29.72 | 1.3967 | 627923 | 0.0047 | 2066 | 2.318E-6 | 6.675 | 6.008 |
| 1056 | 29.85 | 1.4012 | 629861 | 0.0047 | 1890 | 2.519E-6 | 6.813 | 6.131 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^0.5) | deltaK |
|--------------|-------|-----------|--------|------------|------|-------------------|-----------------------|--------|
| 1075 | 30.00 | 1.4063 | 631777 | 0.0047 | 1728 | 2.758E-6 | 6.946 | 6.251 |
| 1093 | 30.14 | 1.4111 | 633444 | 0.0047 | 1593 | 3.036E-6 | 7.086 | 6.378 |
| 1110 | 30.28 | 1.4155 | 634865 | 0.0047 | 1459 | 3.315E-6 | 7.226 | 6.503 |
| 1129 | 30.41 | 1.4201 | 636206 | 0.0047 | 1327 | 3.596E-6 | 7.369 | 6.632 |
| 1148 | 30.56 | 1.4250 | 637480 | 0.0047 | 1218 | 3.941E-6 | 7.512 | 6.761 |
| 1167 | 30.70 | 1.4296 | 638617 | 0.0048 | 1116 | 4.325E-6 | 7.668 | 6.901 |
| 1188 | 30.85 | 1.4345 | 639738 | 0.0047 | 1026 | 4.720E-6 | 7.823 | 7.041 |
| 1209 | 31.01 | 1.4395 | 640752 | 0.0047 | 940 | 5.166E-6 | 7.981 | 7.183 |
| 1229 | 31.15 | 1.4441 | 641563 | 0.0048 | 866 | 5.608E-6 | 8.140 | 7.326 |
| 1249 | 31.28 | 1.4485 | 642361 | 0.0047 | 789 | 6.080E-6 | 8.303 | 7.473 |
| 1270 | 31.44 | 1.4534 | 643122 | 0.0047 | 717 | 6.584E-6 | 8.466 | 7.619 |
| 1292 | 31.59 | 1.4582 | 643812 | 0.0047 | 673 | 7.114E-6 | 8.636 | 7.773 |
| 1313 | 31.74 | 1.4629 | 644469 | 0.0048 | 627 | 7.674E-6 | 8.811 | 7.930 |
| 1336 | 31.89 | 1.4676 | 645054 | 0.0047 | 582 | 8.176E-6 | 8.988 | 8.089 |
| 1359 | 32.04 | 1.4724 | 645603 | 0.0094 | 1071 | 8.773E-6 | 9.165 | 8.249 |
| 1381 | 32.19 | 1.4770 | 646125 | 0.0093 | 1009 | 9.186E-6 | 9.348 | 8.413 |
| | 32.33 | 1.4817 | 646612 | | | | | |
| | 32.53 | 1.4877 | 647008 | | | | | |
| 1427 | 32.73 | 1.4937 | 647606 | 0.0151 | 1479 | 1.021E-5 | 9.816 | 8.835 |
| 1445 | 33.03 | 1.5028 | 648487 | 0.0188 | 1702 | 1.107E-5 | 9.954 | 8.959 |
| 1465 | 33.35 | 1.5125 | 649308 | 0.0195 | 1617 | 1.206E-5 | 10.150 | 9.135 |
| 1486 | 33.68 | 1.5223 | 650104 | 0.0095 | 787 | 1.208E-5 | 10.353 | 9.318 |
| 1506 | 34.01 | 1.5318 | 650927 | 0.0097 | 754 | 1.274E-5 | 10.561 | 9.505 |
| 1526 | 34.34 | 1.5413 | 651668 | 0.0095 | 727 | 1.314E-5 | 10.773 | 9.695 |
| 1547 | 34.67 | 1.5510 | 652327 | 0.0095 | 691 | 1.373E-5 | 10.990 | 9.891 |
| 1569 | 35.02 | 1.5607 | 653013 | 0.0095 | 654 | 1.452E-5 | 11.200 | 10.080 |
| 1588 | 35.34 | 1.5695 | 653671 | 0.0096 | 636 | 1.505E-5 | 11.426 | 10.283 |
| 1609 | 35.68 | 1.5791 | 654248 | 0.0096 | 617 | 1.548E-5 | 11.651 | 10.486 |
| 1633 | 36.05 | 1.5891 | 654851 | 0.0095 | 588 | 1.615E-5 | 11.884 | 10.695 |
| 1655 | 36.41 | 1.5988 | 655482 | 0.0096 | 562 | 1.692E-5 | 12.126 | 10.913 |
| 1677 | 36.77 | 1.6084 | 656031 | 0.0096 | 546 | 1.750E-5 | 12.369 | 11.132 |
| 1700 | 37.13 | 1.6177 | 656540 | 0.0095 | 526 | 1.818E-5 | 12.612 | 11.351 |
| 1722 | 37.49 | 1.6271 | 657043 | 0.0095 | 497 | 1.901E-5 | 12.860 | 11.574 |
| 1745 | 37.86 | 1.6365 | 657523 | 0.0095 | 478 | 1.975E-5 | 13.114 | 11.803 |
| 1768 | 38.23 | 1.6460 | 658004 | 0.0095 | 466 | 2.042E-5 | 13.371 | 12.034 |
| 1792 | 38.61 | 1.6555 | 658463 | 0.0096 | 448 | 2.129E-5 | 13.641 | 12.277 |
| 1816 | 39.01 | 1.6654 | 658900 | 0.0095 | 430 | 2.213E-5 | 13.909 | 12.518 |
| 1840 | 39.40 | 1.6748 | 659337 | 0.0095 | 412 | 2.306E-5 | 14.192 | 12.773 |
| 1865 | 39.80 | 1.6846 | 659730 | 0.0096 | 397 | 2.403E-5 | 14.466 | 13.019 |
| 1889 | 40.18 | 1.6935 | 660100 | 0.0095 | 384 | 2.489E-5 | 14.753 | 13.277 |
| 1913 | 40.58 | 1.7029 | 660474 | 0.0095 | 364 | 2.595E-5 | 15.047 | 13.543 |
| 1940 | 41.02 | 1.7130 | 660847 | 0.0095 | 351 | 2.701E-5 | 15.343 | 13.808 |
| 1966 | 41.43 | 1.7226 | 661203 | 0.0096 | 339 | 2.838E-5 | 15.654 | 14.088 |
| 1991 | 41.84 | 1.7319 | 661520 | 0.0096 | 324 | 2.976E-5 | 15.964 | 14.367 |
| 2018 | 42.27 | 1.7415 | 661833 | 0.0096 | 307 | 3.127E-5 | 16.281 | 14.653 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in]^0.5) |
|--------------|-------|-----------|--------|------------|-----|-------------------|--------|-------------------------|
| 2045 | 42.72 | 1.7512 | 662132 | 0.0095 | 289 | 3.283E-5 | 16.603 | 14.943 |
| 2071 | 43.16 | 1.7608 | 662416 | 0.0096 | 279 | 3.430E-5 | 16.936 | 15.242 |
| 2098 | 43.60 | 1.7704 | 662686 | 0.0097 | 267 | 3.626E-5 | 17.265 | 15.538 |
| 2125 | 44.03 | 1.7795 | 662937 | 0.0096 | 252 | 3.800E-5 | 17.613 | 15.852 |
| 2154 | 44.50 | 1.7894 | 663195 | 0.0096 | 240 | 4.014E-5 | 17.969 | 16.172 |
| 2183 | 45.01 | 1.7998 | 663432 | 0.0096 | 228 | 4.226E-5 | 18.321 | 16.488 |
| 2210 | 45.44 | 1.8086 | 663643 | 0.0096 | 218 | 4.413E-5 | 18.699 | 16.829 |
| 2239 | 45.92 | 1.8183 | 663853 | 0.0095 | 206 | 4.610E-5 | 19.057 | 17.152 |
| 2268 | 46.40 | 1.8278 | 664054 | 0.0094 | 197 | 4.800E-5 | 19.430 | 17.487 |
| 2296 | 46.88 | 1.8371 | 664246 | 0.0096 | 191 | 5.029E-5 | 19.811 | 17.830 |
| 2325 | 47.37 | 1.8466 | 664429 | 0.0096 | 182 | 5.279E-5 | 20.201 | 18.181 |
| 2355 | 47.89 | 1.8564 | 664612 | 0.0096 | 173 | 5.567E-5 | 20.604 | 18.544 |
| 2386 | 48.41 | 1.8663 | 664786 | 0.0096 | 164 | 5.882E-5 | 21.024 | 18.922 |
| 2418 | 48.95 | 1.8762 | 664945 | 0.0096 | 156 | 6.207E-5 | 21.436 | 19.293 |
| 2447 | 49.44 | 1.8863 | 665089 | 0.0097 | 147 | 6.571E-5 | 21.869 | 19.682 |
| 2478 | 49.97 | 1.8948 | 665231 | 0.0096 | 138 | 6.975E-5 | 22.288 | 20.059 |
| 2509 | 50.51 | 1.9044 | 665365 | 0.0096 | 130 | 7.371E-5 | 22.737 | 20.463 |
| 2542 | 51.08 | 1.9143 | 665493 | 0.0096 | 125 | 7.763E-5 | 23.191 | 20.872 |
| 2575 | 51.65 | 1.9242 | 665615 | 0.0097 | 118 | 8.206E-5 | 23.650 | 21.285 |
| 2606 | 52.20 | 1.9335 | 665726 | 0.0189 | 223 | 8.491E-5 | 24.126 | 21.713 |
| 2639 | 52.77 | 1.9431 | 665838 | 0.0195 | 214 | 9.113E-5 | 24.601 | 22.140 |
| | 53.37 | 1.9530 | 665940 | | | | | |
| | 53.96 | 1.9627 | 666037 | | | | | |
| 2630 | 54.52 | 1.9716 | 666147 | 0.0188 | 224 | 8.411E-5 | 25.064 | 22.558 |
| 2630 | 55.15 | 1.9816 | 666261 | 0.0197 | 219 | 8.989E-5 | 25.233 | 22.710 |
| 2630 | 55.77 | 1.9913 | 666366 | 0.0193 | 207 | 9.315E-5 | 25.422 | 22.880 |
| 2630 | 56.39 | 2.0009 | 666468 | 0.0097 | 104 | 9.339E-5 | 25.611 | 23.050 |
| 2630 | 57.02 | 2.0105 | 666570 | 0.0097 | 102 | 9.519E-5 | 25.800 | 23.220 |
| 2630 | 57.65 | 2.0199 | 666667 | 0.0096 | 100 | 9.623E-5 | 25.995 | 23.395 |
| 2630 | 58.32 | 2.0298 | 666769 | 0.0096 | 98 | 9.778E-5 | 26.192 | 23.572 |
| 2630 | 59.01 | 2.0397 | 666871 | 0.0097 | 97 | 9.971E-5 | 26.390 | 23.750 |
| 2630 | 59.66 | 2.0490 | 666964 | 0.0098 | 96 | 1.015E-4 | 26.594 | 23.935 |
| 2630 | 60.36 | 2.0588 | 667057 | 0.0097 | 94 | 1.038E-4 | 26.797 | 24.117 |
| 2630 | 61.07 | 2.0686 | 667151 | 0.0097 | 90 | 1.067E-4 | 27.009 | 24.308 |
| 2630 | 61.80 | 2.0787 | 667245 | 0.0098 | 89 | 1.095E-4 | 27.219 | 24.497 |
| 2630 | 62.51 | 2.0882 | 667330 | 0.0097 | 87 | 1.120E-4 | 27.433 | 24.690 |
| 2630 | 63.23 | 2.0976 | 667411 | 0.0097 | 84 | 1.149E-4 | 27.650 | 24.885 |
| 2630 | 63.99 | 2.1076 | 667497 | 0.0097 | 82 | 1.184E-4 | 27.865 | 25.078 |
| 2630 | 64.75 | 2.1172 | 667578 | 0.0097 | 79 | 1.213E-4 | 28.086 | 25.277 |
| 2630 | 65.49 | 2.1266 | 667654 | 0.0096 | 78 | 1.239E-4 | 28.315 | 25.483 |
| 2630 | 66.31 | 2.1367 | 667734 | 0.0097 | 75 | 1.281E-4 | 28.537 | 25.684 |
| 2630 | 67.09 | 2.1462 | 667806 | 0.0097 | 72 | 1.333E-4 | 28.767 | 25.889 |
| 2630 | 67.86 | 2.1554 | 667877 | 0.0097 | 70 | 1.388E-4 | 29.003 | 26.103 |
| 2630 | 68.70 | 2.1655 | 667947 | 0.0097 | 67 | 1.447E-4 | 29.236 | 26.312 |
| 2630 | 69.56 | 2.1754 | 668011 | 0.0098 | 66 | 1.500E-4 | 29.477 | 26.529 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^1.5) | deltaK |
|--------------|--------|-----------|--------|------------|----|-------------------|-----------------------|----------|
| 2630 | 70.38 | 2.1848 | 668072 | 0.0099 | 64 | 1.554E-4 | 29.727 | 26.754 |
| 2630 | 71.27 | 2.1947 | 668136 | 0.0098 | 61 | 1.600E-4 | 29.979 | 26.981 |
| 2630 | 72.20 | 2.2051 | 668200 | 0.0098 | 59 | 1.648E-4 | 30.235 | 27.211 |
| 2630 | 73.10 | 2.2149 | 668258 | 0.0098 | 58 | 1.705E-4 | 30.496 | 27.447 |
| 2630 | 74.00 | 2.2245 | 668313 | 0.0098 | 55 | 1.773E-4 | 30.757 | 27.681 |
| 2630 | 74.93 | 2.2342 | 668367 | 0.0097 | 52 | 1.850E-4 | 31.016 | 27.914 |
| 2630 | 75.85 | 2.2437 | 668417 | 0.0097 | 50 | 1.926E-4 | 31.282 | 28.153 |
| 2630 | 76.81 | 2.2534 | 668466 | 0.0097 | 48 | 2.004E-4 | 31.550 | 28.394 |
| 2630 | 77.78 | 2.2631 | 668513 | 0.0097 | 46 | 2.088E-4 | 31.825 | 28.642 * |
| 2630 | 78.79 | 2.2729 | 668559 | 0.0098 | 45 | 2.189E-4 | 32.103 | 28.892 * |
| 2630 | 79.79 | 2.2826 | 668603 | 0.0098 | 43 | 2.306E-4 | 32.389 | 29.150 * |
| 2630 | 80.83 | 2.2924 | 668645 | 0.0098 | 41 | 2.425E-4 | 32.683 | 29.414 * |
| 2630 | 81.93 | 2.3027 | 668685 | 0.0098 | 39 | 2.547E-4 | 32.976 | 29.678 * |
| 2630 | 82.99 | 2.3123 | 668721 | 0.0098 | 37 | 2.668E-4 | 33.276 | 29.948 * |
| 2630 | 84.05 | 2.3218 | 668756 | 0.0098 | 35 | 2.794E-4 | 33.582 | 30.223 * |
| 2630 | 85.20 | 2.3319 | 668792 | 0.0098 | 33 | 2.936E-4 | 33.883 | 30.493 * |
| 2630 | 86.32 | 2.3415 | 668824 | 0.0098 | 32 | 3.093E-4 | 34.203 | 30.781 * |
| 2630 | 87.49 | 2.3514 | 668855 | 0.0098 | 30 | 3.278E-4 | 34.523 | 31.069 * |
| 2630 | 88.70 | 2.3615 | 668885 | 0.0098 | 28 | 3.501E-4 | 34.848 | 31.362 * |
| 2630 | 89.90 | 2.3713 | 668912 | 0.0099 | 27 | 3.740E-4 | 35.170 | 31.651 * |
| 2630 | 91.04 | 2.3804 | 668936 | 0.0098 | 25 | 3.964E-4 | 35.513 | 31.960 * |
| 2630 | 92.36 | 2.3908 | 668961 | 0.0098 | 23 | 4.216E-4 | 35.841 | 32.255 * |
| 2630 | 93.64 | 2.4007 | 668983 | 0.0098 | 22 | 4.449E-4 | 36.189 | 32.568 * |
| 2630 | 94.89 | 2.4101 | 669004 | 0.0099 | 21 | 4.660E-4 | 36.544 | 32.888 * |
| 2630 | 96.25 | 2.4202 | 669025 | 0.0099 | 20 | 4.857E-4 | 36.901 | 33.208 * |
| 2630 | 97.64 | 2.4303 | 669045 | 0.0099 | 19 | 5.084E-4 | 37.259 | 33.530 * |
| 2630 | 98.95 | 2.4396 | 669063 | 0.0099 | 18 | 5.388E-4 | 37.645 | 33.877 * |
| 2630 | 100.44 | 2.4501 | 669083 | 0.0098 | 17 | 5.870E-4 | 38.008 | 34.204 * |
| 2630 | 101.87 | 2.4598 | 669099 | 0.0097 | 16 | 6.443E-4 | 38.396 | 34.552 * |
| 2630 | 103.28 | 2.4693 | 669113 | 0.0098 | 14 | 7.180E-4 | 38.775 | 34.893 * |
| 2629 | 104.74 | 2.4789 | 669126 | 0.0099 | 13 | 7.870E-4 | 39.165 | 35.243 * |
| 2629 | 106.27 | 2.4887 | 669138 | 0.0100 | 12 | 8.697E-4 | 39.555 | 35.592 * |
| 2630 | 107.78 | 2.4983 | 669148 | 0.0108 | 11 | 1.000E-3 | 39.991 | 35.985 * |
| 2629 | 109.53 | 2.5095 | 669160 | 0.0102 | 10 | 1.120E-3 | 40.402 | 36.350 * |
| 2628 | 111.17 | 2.5197 | 669169 | 0.0104 | 9 | 1.227E-3 | 40.961 | 36.854 * |
| 2630 | 113.47 | 2.5338 | 669177 | 0.0108 | 8 | 1.377E-3 | 41.283 | 37.137 * |
| 2626 | 114.53 | 2.5401 | 669184 | 0.0175 | 14 | 1.251E-3 | 41.844 | 37.637 * |
| 2623 | 116.43 | 2.5513 | 669191 | 0.0230 | 13 | 1.770E-3 | 42.190 | 37.938 * |
| | 118.50 | 2.5631 | 669197 | | | | | |

Automated Fatigue Crack
Growth Rate Analysis

| | | | |
|-----------------|--------------|---------------|------|
| Test ID | 5086-FCG-45 | Geometry | C(T) |
| Contract | SSC 10624-01 | Orientation | T-L |
| Material | 5383-H116 | Yield (ksi) | 35.4 |
| Temperature (F) | 75 | Modulus (Msi) | 10.5 |
| Environment | RH = 40% | | |

Specimen Dimensions (in)

| | | | |
|---------------|-------|-------------|-------|
| Thickness | 0.496 | Height | 2.400 |
| Net Thickness | 0.496 | Notch Depth | 1.000 |
| Width | 4.000 | Gage Length | 0.500 |

Precrack Parameters

| | | | |
|--------------|-------|--------------------|------|
| Pmax (lbs) | 859.0 | Stress Ratio | 0.10 |
| Final a (in) | 1.050 | Kmax (ksi sqr[in]) | 4.41 |

Test Parameters

| EvBP | Freq | Pmax | R | Ai | Kmaxi | C | DKi |
|--------|------|------|------|-------|-------|------|------|
| 23.716 | 5.00 | 0 | 0.10 | 1.140 | 2.80 | 4.00 | 0.00 |
| 33.922 | 5.00 | 0 | 0.10 | 1.451 | 9.69 | 2.00 | 0.00 |
| 52.247 | 5.00 | 2750 | 0.10 | 0.000 | 0.00 | 0.00 | 0.00 |

| K Coeff | C Coeff |
|---------|----------|
| .886 | 1.00098 |
| 4.64 | -4.66951 |
| -13.32 | 18.4601 |
| 14.72 | -236.825 |
| -5.6 | 1214.88 |
| . | -2143.57 |

Visual Observations

| EvB/P | Crack(EvB/P) | Crack(visual) | Error | CAF |
|---------|--------------|---------------|--------|-------|
| 20.753 | 0.983 | 1.002 | 0.019 | 0.993 |
| 21.841 | 1.040 | 1.040 | 0.000 | 0.992 |
| 23.480 | 1.121 | 1.100 | -0.021 | 0.990 |
| 23.760 | 1.134 | 1.170 | 0.036 | 0.989 |
| 26.667 | 1.260 | 1.260 | 0.000 | 0.987 |
| 27.531 | 1.294 | 1.280 | -0.014 | 0.986 |
| 30.339 | 1.397 | 1.380 | -0.017 | 0.983 |
| 34.274 | 1.524 | 1.490 | -0.034 | 0.981 |
| 48.661 | 1.865 | 1.880 | 0.015 | 0.973 |
| 59.300 | 2.043 | 2.080 | 0.037 | 0.969 |
| 66.619 | 2.142 | 2.120 | -0.022 | 0.967 |
| 101.006 | 2.462 | 2.460 | -0.002 | 0.960 |

Comments

Date of test: 9/9/2006

| Waveform Type | | Sine | | | | | | |
|---------------------|-------|-----------|--------|------------|--------|-------------------|-----------------------|--------|
| Test ID 5086-FCG-45 | | Page 1 | | | | | | |
| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^0.5) | deltaK |
| | 23.78 | 1.1354 | 33353 | | | | | |
| 535 | 23.89 | 1.1402 | 83477 | 0.0093 | 107030 | 8.711E-8 | 2.916 | 2.625 |
| 544 | 23.99 | 1.1447 | 140383 | 0.0099 | 105802 | 9.340E-8 | 2.977 | 2.680 |
| 554 | 24.10 | 1.1501 | 189279 | 0.0050 | 45981 | 1.085E-7 | 3.037 | 2.734 |
| 564 | 24.22 | 1.1554 | 233480 | 0.0050 | 42879 | 1.212E-7 | 3.098 | 2.788 |
| 572 | 24.32 | 1.1599 | 277489 | 0.0050 | 39050 | 1.328E-7 | 3.165 | 2.849 |
| 582 | 24.44 | 1.1652 | 309241 | 0.0050 | 35546 | 1.427E-7 | 3.227 | 2.904 |
| 593 | 24.55 | 1.1701 | 340750 | 0.0049 | 32421 | 1.535E-7 | 3.293 | 2.963 |
| 602 | 24.66 | 1.1750 | 374683 | 0.0049 | 29126 | 1.674E-7 | 3.360 | 3.024 |
| 613 | 24.77 | 1.1800 | 402556 | 0.0048 | 27752 | 1.767E-7 | 3.425 | 3.083 |
| 622 | 24.87 | 1.1846 | 428006 | 0.0048 | 26217 | 1.880E-7 | 3.495 | 3.145 |
| 633 | 24.99 | 1.1895 | 452244 | 0.0050 | 23955 | 2.059E-7 | 3.563 | 3.207 |
| 644 | 25.10 | 1.1943 | 475755 | 0.0049 | 22380 | 2.211E-7 | 3.634 | 3.270 |
| 654 | 25.21 | 1.1991 | 498053 | 0.0049 | 20594 | 2.426E-7 | 3.713 | 3.342 |
| 667 | 25.34 | 1.2048 | 518413 | 0.0048 | 19165 | 2.607E-7 | 3.784 | 3.406 |
| 678 | 25.45 | 1.2094 | 536833 | 0.0050 | 17832 | 2.840E-7 | 3.866 | 3.479 |
| 689 | 25.56 | 1.2142 | 551568 | 0.0050 | 16287 | 3.041E-7 | 3.938 | 3.544 |
| 700 | 25.66 | 1.2186 | 567233 | 0.0049 | 14958 | 3.305E-7 | 4.022 | 3.620 |
| 713 | 25.79 | 1.2242 | 582744 | 0.0049 | 13629 | 3.635E-7 | 4.098 | 3.689 |
| 725 | 25.91 | 1.2288 | 595772 | 0.0049 | 12911 | 3.919E-7 | 4.187 | 3.769 |
| 737 | 26.03 | 1.2340 | 607561 | 0.0049 | 11872 | 4.203E-7 | 4.271 | 3.844 |
| 750 | 26.15 | 1.2388 | 618605 | 0.0048 | 10760 | 4.508E-7 | 4.356 | 3.920 |
| 762 | 26.26 | 1.2436 | 629031 | 0.0048 | 10112 | 4.779E-7 | 4.441 | 3.997 |
| 774 | 26.37 | 1.2481 | 638463 | 0.0048 | 9538 | 5.086E-7 | 4.530 | 4.077 |
| 788 | 26.49 | 1.2531 | 647302 | 0.0048 | 8875 | 5.444E-7 | 4.616 | 4.155 |
| 800 | 26.61 | 1.2578 | 656441 | 0.0049 | 8355 | 5.857E-7 | 4.714 | 4.242 |
| 815 | 26.74 | 1.2631 | 664786 | 0.0050 | 7894 | 6.358E-7 | 4.805 | 4.325 |
| 828 | 26.85 | 1.2677 | 671855 | 0.0049 | 7406 | 6.798E-7 | 4.907 | 4.416 |
| 843 | 26.98 | 1.2727 | 679160 | 0.0050 | 6772 | 7.370E-7 | 5.007 | 4.506 |
| 858 | 27.12 | 1.2781 | 685829 | 0.0048 | 6101 | 8.065E-7 | 5.108 | 4.597 |
| 872 | 27.23 | 1.2827 | 691736 | 0.0094 | 11243 | 8.360E-7 | 5.212 | 4.691 |
| 886 | 27.35 | 1.2875 | 697072 | 0.0094 | 9654 | 9.755E-7 | 5.314 | 4.782 |
| 901 | 27.47 | 1.2922 | 701390 | 0.0390 | 29392 | 1.326E-6 | 0.000 | 0.000 |
| 1014 | 28.37 | 1.3265 | 726464 | 0.0392 | 27605 | 1.418E-6 | 0.000 | 0.000 |
| 1031 | 28.50 | 1.3313 | 728995 | 0.0099 | 4844 | 2.034E-6 | 6.358 | 5.723 |
| 1048 | 28.64 | 1.3363 | 731308 | 0.0099 | 4387 | 2.256E-6 | 6.485 | 5.836 |
| 1066 | 28.77 | 1.3412 | 733382 | 0.0099 | 3989 | 2.477E-6 | 6.617 | 5.955 |
| 1084 | 28.90 | 1.3462 | 735297 | 0.0049 | 1820 | 2.783E-6 | 6.748 | 6.073 |
| 1102 | 29.04 | 1.3510 | 736972 | 0.0049 | 1657 | 3.053E-6 | 6.885 | 6.196 |
| 1121 | 29.17 | 1.3559 | 738453 | 0.0049 | 1501 | 3.346E-6 | 7.023 | 6.321 |
| 1140 | 29.31 | 1.3609 | 739913 | 0.0049 | 1352 | 3.702E-6 | 7.166 | 6.450 |
| 1160 | 29.45 | 1.3659 | 741247 | 0.0049 | 1233 | 4.075E-6 | 7.311 | 6.580 |
| 1179 | 29.58 | 1.3708 | 742390 | 0.0049 | 1137 | 4.436E-6 | 7.460 | 6.714 |
| 1199 | 29.72 | 1.3757 | 743407 | 0.0049 | 1036 | 4.797E-6 | 7.607 | 6.846 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in]^0.5) |
|--------------|-------|-----------|--------|------------|------|-------------------|--------|-------------------------|
| 1219 | 29.86 | 1.3805 | 744372 | 0.0049 | 943 | 5.188E-6 | 7.760 | 6.984 |
| 1240 | 29.99 | 1.3853 | 745277 | 0.0049 | 873 | 5.596E-6 | 7.914 | 7.122 |
| 1260 | 30.13 | 1.3902 | 746130 | 0.0049 | 817 | 6.049E-6 | 8.072 | 7.265 |
| 1281 | 30.27 | 1.3950 | 746903 | 0.0049 | 759 | 6.551E-6 | 8.235 | 7.411 |
| 1304 | 30.42 | 1.4000 | 747626 | 0.0049 | 706 | 7.078E-6 | 8.401 | 7.561 |
| 1326 | 30.56 | 1.4050 | 748309 | 0.0050 | 656 | 7.632E-6 | 8.572 | 7.715 |
| 1348 | 30.71 | 1.4099 | 748927 | 0.0050 | 611 | 8.185E-6 | 8.748 | 7.873 |
| 1372 | 30.85 | 1.4149 | 749510 | 0.0049 | 568 | 8.750E-6 | 8.926 | 8.033 |
| 1395 | 31.00 | 1.4199 | 750065 | 0.0099 | 1057 | 9.386E-6 | 9.106 | 8.195 |
| 1419 | 31.15 | 1.4248 | 750567 | 0.0097 | 969 | 9.969E-6 | 9.291 | 8.361 |
| | 31.29 | 1.4295 | 751034 | | | | | |
| | 35.34 | 1.5548 | 2545 | | | | | |
| 1744 | 35.68 | 1.5642 | 3058 | 0.0193 | 1039 | 1.858E-5 | 12.504 | 11.253 |
| 1767 | 36.03 | 1.5741 | 3584 | 0.0197 | 1040 | 1.889E-5 | 12.749 | 11.474 |
| 1791 | 36.38 | 1.5839 | 4098 | 0.0199 | 1004 | 1.981E-5 | 13.006 | 11.706 |
| 1815 | 36.74 | 1.5939 | 4588 | 0.0099 | 482 | 2.060E-5 | 13.266 | 11.939 |
| 1840 | 37.11 | 1.6038 | 5054 | 0.0099 | 463 | 2.143E-5 | 13.533 | 12.180 |
| 1864 | 37.48 | 1.6137 | 5507 | 0.0099 | 441 | 2.235E-5 | 13.809 | 12.428 |
| 1890 | 37.86 | 1.6239 | 5951 | 0.0098 | 423 | 2.323E-5 | 14.084 | 12.675 |
| 1915 | 38.24 | 1.6337 | 6364 | 0.0098 | 406 | 2.419E-5 | 14.367 | 12.930 |
| 1940 | 38.61 | 1.6433 | 6746 | 0.0098 | 389 | 2.521E-5 | 14.651 | 13.186 |
| 1965 | 38.99 | 1.6529 | 7127 | 0.0098 | 371 | 2.639E-5 | 14.941 | 13.447 |
| 1991 | 39.38 | 1.6628 | 7492 | 0.0098 | 355 | 2.764E-5 | 15.238 | 13.714 |
| 2018 | 39.78 | 1.6727 | 7841 | 0.0099 | 341 | 2.895E-5 | 15.546 | 13.991 |
| 2045 | 40.18 | 1.6827 | 8174 | 0.0099 | 327 | 3.033E-5 | 15.857 | 14.272 |
| 2072 | 40.59 | 1.6926 | 8492 | 0.0099 | 313 | 3.171E-5 | 16.177 | 14.560 |
| 2099 | 41.01 | 1.7025 | 8794 | 0.0099 | 298 | 3.311E-5 | 16.506 | 14.856 |
| 2128 | 41.43 | 1.7125 | 9091 | 0.0099 | 285 | 3.466E-5 | 16.839 | 15.155 |
| 2156 | 41.86 | 1.7225 | 9372 | 0.0099 | 273 | 3.625E-5 | 17.176 | 15.458 |
| 2184 | 42.27 | 1.7320 | 9629 | 0.0099 | 259 | 3.799E-5 | 17.524 | 15.772 |
| 2213 | 42.71 | 1.7421 | 9885 | 0.0098 | 246 | 3.992E-5 | 17.868 | 16.081 |
| 2242 | 43.15 | 1.7519 | 10128 | 0.0099 | 236 | 4.184E-5 | 18.228 | 16.405 |
| 2271 | 43.59 | 1.7616 | 10349 | 0.0099 | 228 | 4.367E-5 | 18.588 | 16.729 |
| 2300 | 44.03 | 1.7713 | 10564 | 0.0098 | 214 | 4.574E-5 | 18.970 | 17.073 |
| 2332 | 44.52 | 1.7817 | 10790 | 0.0099 | 201 | 4.888E-5 | 19.347 | 17.413 |
| 2362 | 44.99 | 1.7917 | 10995 | 0.0100 | 191 | 5.261E-5 | 19.736 | 17.762 |
| 2391 | 45.43 | 1.8010 | 11168 | 0.0099 | 181 | 5.575E-5 | 20.134 | 18.121 |
| 2423 | 45.91 | 1.8110 | 11332 | 0.0098 | 169 | 5.868E-5 | 20.539 | 18.485 |
| 2456 | 46.43 | 1.8215 | 11497 | 0.0098 | 160 | 6.157E-5 | 20.943 | 18.848 |
| 2486 | 46.89 | 1.8309 | 11652 | 0.0098 | 153 | 6.371E-5 | 21.376 | 19.238 |
| 2518 | 47.39 | 1.8407 | 11806 | 0.0099 | 148 | 6.613E-5 | 21.793 | 19.614 |
| 2551 | 47.89 | 1.8506 | 11952 | 0.0098 | 141 | 6.956E-5 | 22.218 | 19.997 |
| 2581 | 48.38 | 1.8600 | 12086 | 0.0100 | 135 | 7.377E-5 | 22.669 | 20.402 |
| 2615 | 48.91 | 1.8702 | 12219 | 0.0099 | 127 | 7.821E-5 | 23.119 | 20.807 |
| 2649 | 49.46 | 1.8805 | 12345 | 0.0099 | 120 | 8.301E-5 | 23.597 | 21.237 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^1.5) | deltaK |
|--------------|-------|-----------|-------|------------|-----|-------------------|-----------------------|--------|
| 2685 | 50.01 | 1.8906 | 12462 | 0.0100 | 114 | 8.825E-5 | 24.066 | 21.660 |
| 2717 | 50.53 | 1.9001 | 12569 | 0.0194 | 210 | 9.254E-5 | 24.557 | 22.101 |
| 2751 | 51.08 | 1.9100 | 12672 | 0.0201 | 200 | 1.004E-4 | 25.042 | 22.538 |
| | 51.65 | 1.9201 | 12769 | | | | | |
| | 52.25 | 1.9306 | 12875 | | | | | |
| 2750 | 52.76 | 1.9394 | 12970 | 0.0188 | 201 | 9.340E-5 | 25.587 | 23.028 |
| 2750 | 53.34 | 1.9494 | 13076 | 0.0197 | 209 | 9.430E-5 | 25.765 | 23.188 |
| 2750 | 53.92 | 1.9591 | 13179 | 0.0197 | 205 | 9.589E-5 | 25.959 | 23.363 |
| 2750 | 54.52 | 1.9690 | 13281 | 0.0099 | 101 | 9.807E-5 | 26.152 | 23.537 |
| 2750 | 55.13 | 1.9790 | 13380 | 0.0099 | 99 | 9.979E-5 | 26.351 | 23.716 |
| 2750 | 55.76 | 1.9889 | 13478 | 0.0100 | 98 | 1.017E-4 | 26.553 | 23.897 |
| 2750 | 56.39 | 1.9990 | 13577 | 0.0100 | 96 | 1.037E-4 | 26.755 | 24.079 |
| 2750 | 57.02 | 2.0088 | 13671 | 0.0100 | 94 | 1.060E-4 | 26.963 | 24.267 |
| 2750 | 57.68 | 2.0189 | 13765 | 0.0099 | 92 | 1.085E-4 | 27.172 | 24.454 |
| 2750 | 58.35 | 2.0289 | 13855 | 0.0099 | 89 | 1.107E-4 | 27.384 | 24.645 |
| 2750 | 59.01 | 2.0388 | 13942 | 0.0100 | 88 | 1.127E-4 | 27.597 | 24.837 |
| 2750 | 59.68 | 2.0486 | 14027 | 0.0099 | 86 | 1.148E-4 | 27.810 | 25.029 |
| 2750 | 60.35 | 2.0583 | 14113 | 0.0099 | 84 | 1.171E-4 | 28.032 | 25.228 |
| 2750 | 61.07 | 2.0685 | 14200 | 0.0100 | 82 | 1.210E-4 | 28.250 | 25.425 |
| 2750 | 61.78 | 2.0784 | 14281 | 0.0099 | 80 | 1.252E-4 | 28.478 | 25.630 |
| 2750 | 62.50 | 2.0882 | 14357 | 0.0100 | 77 | 1.294E-4 | 28.711 | 25.840 |
| 2750 | 63.26 | 2.0986 | 14433 | 0.0100 | 75 | 1.335E-4 | 28.938 | 26.044 |
| 2750 | 63.99 | 2.1083 | 14504 | 0.0100 | 73 | 1.370E-4 | 29.178 | 26.260 |
| 2750 | 64.75 | 2.1182 | 14577 | 0.0099 | 70 | 1.401E-4 | 29.414 | 26.473 |
| 2750 | 65.53 | 2.1283 | 14648 | 0.0201 | 139 | 1.445E-4 | 29.656 | 26.691 |
| 2750 | 66.32 | 2.1383 | 14716 | 0.0195 | 131 | 1.492E-4 | 29.898 | 26.908 |
| 2750 | 67.08 | 2.1478 | 14779 | 0.1002 | 567 | 1.767E-4 | 0.000 | 0.000 |
| 2750 | 74.99 | 2.2385 | 15283 | 0.0999 | 543 | 1.839E-4 | 0.000 | 0.000 |
| 2750 | 75.86 | 2.2477 | 15322 | 0.0193 | 81 | 2.388E-4 | 32.857 | 29.570 |
| 2750 | 76.84 | 2.2578 | 15364 | 0.0202 | 81 | 2.488E-4 | 33.139 | 29.824 |
| 2750 | 77.83 | 2.2678 | 15403 | 0.0195 | 75 | 2.596E-4 | 33.430 | 30.086 |
| 2750 | 78.77 | 2.2773 | 15439 | 0.0100 | 36 | 2.789E-4 | 33.727 | 30.354 |
| 2750 | 79.75 | 2.2869 | 15472 | 0.0099 | 34 | 2.936E-4 | 34.029 | 30.625 |
| 2750 | 80.81 | 2.2971 | 15505 | 0.0099 | 32 | 3.103E-4 | 34.340 | 30.904 |
| 2750 | 81.90 | 2.3074 | 15537 | 0.0100 | 30 | 3.280E-4 | 34.655 | 31.189 |
| 2750 | 82.95 | 2.3172 | 15567 | 0.0099 | 29 | 3.467E-4 | 34.983 | 31.484 |
| 2750 | 84.05 | 2.3273 | 15595 | 0.0100 | 28 | 3.643E-4 | 35.302 | 31.771 |
| 2750 | 85.15 | 2.3371 | 15621 | 0.0100 | 27 | 3.804E-4 | 35.627 | 32.063 |
| 2750 | 86.22 | 2.3465 | 15644 | 0.0101 | 25 | 3.980E-4 | 35.973 | 32.374 |
| 2750 | 87.47 | 2.3573 | 15671 | 0.0100 | 24 | 4.198E-4 | 36.312 | 32.679 |
| 2750 | 88.67 | 2.3675 | 15696 | 0.0100 | 22 | 4.482E-4 | 36.675 | 33.005 |
| 2750 | 89.90 | 2.3777 | 15718 | 0.0101 | 21 | 4.872E-4 | 37.028 | 33.323 |
| 2750 | 91.09 | 2.3873 | 15737 | 0.0101 | 19 | 5.320E-4 | 37.385 | 33.644 |
| 2750 | 92.31 | 2.3971 | 15755 | 0.0100 | 17 | 5.862E-4 | 37.745 | 33.967 |
| 2750 | 93.57 | 2.4070 | 15771 | 0.0099 | 16 | 6.385E-4 | 38.122 | 34.306 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^-.5) | deltaK |
|--------------|--------|-----------|-------|------------|----|-------------------|-----------------------|----------|
| 2750 | 94.95 | 2.4176 | 15787 | 0.0100 | 15 | 7.072E-4 | 38.492 | 34.637 |
| 2750 | 96.23 | 2.4273 | 15800 | 0.0100 | 13 | 7.746E-4 | 38.889 | 34.994 |
| 2749 | 97.60 | 2.4374 | 15813 | 0.0101 | 12 | 8.391E-4 | 39.274 | 35.339 * |
| 2749 | 98.99 | 2.4475 | 15824 | 0.0101 | 11 | 9.128E-4 | 39.668 | 35.694 * |
| 2749 | 100.36 | 2.4572 | 15834 | 0.0108 | 10 | 1.053E-3 | 40.081 | 36.064 * |
| 2749 | 101.85 | 2.4677 | 15845 | 0.0103 | 9 | 1.205E-3 | 40.496 | 36.437 * |
| 2749 | 103.38 | 2.4782 | 15854 | 0.0105 | 8 | 1.473E-3 | 41.004 | 36.887 * |
| 2749 | 105.40 | 2.4919 | 15861 | 0.0106 | 7 | 1.871E-3 | 41.314 | 37.159 * |
| 2740 | 106.49 | 2.4990 | 15867 | 0.0106 | 5 | 2.398E-3 | 41.849 | 37.631 * |
| 2739 | 108.22 | 2.5103 | 15871 | 0.0104 | 4 | 2.988E-3 | 42.162 | 37.901 * |
| 2737 | 109.87 | 2.5208 | 15874 | 0.0211 | 6 | 3.514E-3 | 42.588 | 38.268 * |
| 2730 | 111.59 | 2.5314 | 15877 | 0.0199 | 5 | 3.987E-3 | 42.968 | 38.595 * |
| | 113.12 | 2.5407 | 15879 | | | | | |

Automated Fatigue Crack
Growth Rate Analysis

| | | | |
|-----------------|---------------|---------------|------|
| Test ID | 5086-FCG-4pt5 | Geometry | C(T) |
| Contract | SSC 10624-01 | Orientation | T-L |
| Material | 5383-H116 | Yield (ksi) | 35.4 |
| Temperature (F) | 75 | Modulus (Msi) | 10.5 |
| Environment | RH = 40% | | |

Specimen Dimensions (in)

| | | | |
|---------------|-------|-------------|-------|
| Thickness | 0.496 | Height | 2.400 |
| Net Thickness | 0.496 | Notch Depth | 1.000 |
| Width | 4.000 | Gage Length | 0.500 |

Precrack Parameters

| | | | |
|--------------|-------|--------------------|------|
| Pmax (lbs) | 859.0 | Stress Ratio | 0.10 |
| Final a (in) | 1.050 | Kmax (ksi sqr[in]) | 4.41 |

Test Parameters

| EvBP | Freq | Pmax | R | Ai | Kmaxi | C | DKi |
|--------|------|------|------|-------|-------|------|------|
| 23.720 | 0.50 | 0 | 0.10 | 1.140 | 2.80 | 4.00 | 0.00 |
| 31.406 | 0.50 | 0 | 0.10 | 1.451 | 9.69 | 2.00 | 0.00 |
| 52.250 | 0.50 | 2750 | 0.10 | 0.000 | 0.00 | 0.00 | 0.00 |

| K Coeff | C Coeff |
|---------|----------|
| .886 | 1.00098 |
| 4.64 | -4.66951 |
| -13.32 | 18.4601 |
| 14.72 | -236.825 |
| -5.6 | 1214.88 |
| . | -2143.57 |

Visual Observations

| EvB/P | Crack(EvB/P) | Crack(visual) | Error | CAF |
|---------|--------------|---------------|--------|-------|
| 20.753 | 0.983 | 1.002 | 0.019 | 0.993 |
| 21.841 | 1.040 | 1.040 | 0.000 | 0.992 |
| 23.480 | 1.121 | 1.100 | -0.021 | 0.990 |
| 23.760 | 1.134 | 1.170 | 0.036 | 0.989 |
| 26.667 | 1.260 | 1.260 | 0.000 | 0.987 |
| 27.531 | 1.294 | 1.280 | -0.014 | 0.986 |
| 30.339 | 1.397 | 1.380 | -0.017 | 0.983 |
| 34.274 | 1.524 | 1.490 | -0.034 | 0.981 |
| 48.661 | 1.865 | 1.880 | 0.015 | 0.973 |
| 59.300 | 2.043 | 2.080 | 0.037 | 0.969 |
| 66.619 | 2.142 | 2.120 | -0.022 | 0.967 |
| 101.006 | 2.462 | 2.460 | -0.002 | 0.960 |

Comments

Date of test: 9/9/2006

Waveform Type

Sine

Test ID 5086-FCG-4pt5

Page 1

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^0.5) | deltaK |
|--------------|-------|-----------|--------|------------|---------|-------------------|-----------------------|--------|
| | 27.62 | 1.2978 | 704348 | | | | | |
| 925 | 27.66 | 1.2994 | 705872 | 0.0035 | 3329 | 1.056E-6 | 5.588 | 5.029 |
| 930 | 27.71 | 1.3013 | 707677 | 0.0039 | 3583 | 1.077E-6 | 5.630 | 5.067 |
| 937 | 27.76 | 1.3033 | 709455 | 0.0019 | 1698 | 1.121E-6 | 5.673 | 5.106 |
| 943 | 27.81 | 1.3053 | 711233 | 0.0019 | 1698 | 1.143E-6 | 5.720 | 5.148 |
| 950 | 27.87 | 1.3073 | 712947 | 0.0020 | 1641 | 1.182E-6 | 5.765 | 5.189 |
| 956 | 27.92 | 1.3092 | 714536 | 0.0020 | 1588 | 1.226E-6 | 5.811 | 5.230 |
| 962 | 27.96 | 1.3111 | 716061 | 0.0020 | 1535 | 1.276E-6 | 5.856 | 5.271 |
| 968 | 28.01 | 1.3130 | 717521 | 0.0023 | 1793 | 1.384E-6 | 5.903 | 5.313 |
| 975 | 28.07 | 1.3150 | 718982 | 0.0029 | 1988 | 1.480E-6 | 5.951 | 5.355 |
| 982 | 28.12 | 1.3171 | 720442 | 0.0034 | 2156 | 1.530E-6 | 6.028 | 5.425 |
| 996 | 28.23 | 1.3213 | 723707 | 0.0039 | 2298 | 1.686E-6 | 6.116 | 5.504 |
| 1014 | 28.37 | 1.3265 | 726464 | 0.0100 | 5288 | 1.887E-6 | 6.230 | 5.607 |
| 1031 | 28.50 | 1.3313 | 728995 | 0.0099 | 4844 | 2.034E-6 | 6.358 | 5.723 |
| 1048 | 28.64 | 1.3363 | 731308 | 0.1073 | 22660 | 4.737E-6 | 0.000 | 0.000 |
| 1467 | 31.56 | 1.4387 | 751655 | 0.1041 | 20492 | 5.082E-6 | 0.000 | 0.000 |
| 1471 | 31.62 | 1.4405 | 751800 | 0.0037 | 324 | 1.132E-5 | 9.731 | 8.758 |
| 1475 | 31.68 | 1.4423 | 751979 | 0.0040 | 359 | 1.115E-5 | 9.770 | 8.793 |
| 1479 | 31.74 | 1.4445 | 752159 | 0.0040 | 338 | 1.183E-5 | 9.807 | 8.826 |
| 1483 | 31.80 | 1.4463 | 752317 | 0.0020 | 173 | 1.133E-5 | 9.847 | 8.863 |
| 1487 | 31.86 | 1.4482 | 752496 | 0.0020 | 172 | 1.145E-5 | 9.886 | 8.897 |
| 1491 | 31.92 | 1.4503 | 752674 | 0.0020 | 172 | 1.147E-5 | 9.925 | 8.932 |
| 1495 | 31.98 | 1.4522 | 752839 | 0.0020 | 173 | 1.148E-5 | 9.965 | 8.969 |
| 1499 | 32.04 | 1.4542 | 753011 | 0.0020 | 170 | 1.158E-5 | 10.006 | 9.005 |
| 1504 | 32.10 | 1.4562 | 753189 | 0.0020 | 167 | 1.168E-5 | 10.046 | 9.041 |
| 1508 | 32.17 | 1.4582 | 753354 | 0.0020 | 167 | 1.169E-5 | 10.085 | 9.077 |
| 1512 | 32.22 | 1.4601 | 753513 | 0.0020 | 165 | 1.179E-5 | 10.126 | 9.113 |
| 1516 | 32.28 | 1.4621 | 753678 | 0.0019 | 161 | 1.201E-5 | 10.164 | 9.148 |
| 1520 | 32.34 | 1.4640 | 753843 | 0.0019 | 160 | 1.217E-5 | 10.205 | 9.185 |
| 1524 | 32.41 | 1.4660 | 754002 | 0.0020 | 159 | 1.233E-5 | 10.246 | 9.221 |
| 1528 | 32.47 | 1.4679 | 754154 | 0.0019 | 153 | 1.255E-5 | 10.286 | 9.258 |
| 1532 | 32.53 | 1.4699 | 754312 | 0.0019 | 150 | 1.286E-5 | 10.327 | 9.294 |
| 1536 | 32.59 | 1.4718 | 754464 | 0.0020 | 152 | 1.310E-5 | 10.367 | 9.330 |
| 1540 | 32.65 | 1.4736 | 754596 | 0.0038 | 281 | 1.365E-5 | 10.408 | 9.367 |
| 1544 | 32.71 | 1.4756 | 754745 | 0.0042 | 318 | 1.328E-5 | 10.451 | 9.405 |
| 1549 | 32.78 | 1.4779 | 754914 | 0.6776 | -739922 | -9.158E-7 | 0.000 | 0.000 |
| 2745 | 67.52 | 2.1533 | 14823 | 0.6773 | -740078 | -9.152E-7 | 0.000 | 0.000 |
| 2750 | 67.68 | 2.1552 | 14836 | 0.0038 | 26 | 1.469E-4 | 30.299 | 27.249 |
| 2750 | 67.83 | 2.1571 | 14849 | 0.0040 | 26 | 1.540E-4 | 30.377 | 27.338 |
| 2750 | 68.00 | 2.1592 | 14862 | 0.0040 | 26 | 1.536E-4 | 30.426 | 27.384 |
| 2750 | 68.16 | 2.1611 | 14875 | 0.0020 | 13 | 1.519E-4 | 30.479 | 27.431 |
| 2750 | 68.33 | 2.1631 | 14888 | 0.0020 | 13 | 1.511E-4 | 30.530 | 27.477 |
| 2750 | 68.49 | 2.1651 | 14901 | 0.0020 | 13 | 1.503E-4 | 30.581 | 27.523 |
| 2750 | 68.66 | 2.1671 | 14915 | 0.0020 | 13 | 1.518E-4 | 30.633 | 27.570 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in]^0.5) |
|--------------|-------|-----------|-------|------------|----|-------------------|--------|-------------------------|
| 2750 | 68.82 | 2.1691 | 14928 | 0.0020 | 13 | 1.534E-4 | 30.683 | 27.614 |
| 2750 | 68.98 | 2.1709 | 14940 | 0.0020 | 13 | 1.551E-4 | 30.735 | 27.662 |
| 2750 | 69.16 | 2.1730 | 14953 | 0.0020 | 13 | 1.591E-4 | 30.787 | 27.708 |
| 2750 | 69.33 | 2.1751 | 14966 | 0.0020 | 12 | 1.615E-4 | 30.839 | 27.755 |
| 2750 | 69.49 | 2.1770 | 14978 | 0.0020 | 12 | 1.640E-4 | 30.893 | 27.803 |
| 2750 | 69.67 | 2.1790 | 14990 | 0.0020 | 12 | 1.671E-4 | 30.944 | 27.849 |
| 2750 | 69.84 | 2.1810 | 15002 | 0.0020 | 12 | 1.713E-4 | 30.997 | 27.898 |
| 2750 | 70.00 | 2.1830 | 15013 | 0.0020 | 11 | 1.748E-4 | 31.048 | 27.943 |
| 2750 | 70.17 | 2.1849 | 15024 | 0.0020 | 11 | 1.768E-4 | 31.101 | 27.991 |
| 2750 | 70.34 | 2.1869 | 15035 | 0.0020 | 11 | 1.789E-4 | 31.153 | 28.038 |
| 2750 | 70.52 | 2.1889 | 15046 | 0.0020 | 11 | 1.789E-4 | 31.207 | 28.086 |
| 2750 | 70.69 | 2.1910 | 15058 | 0.0020 | 11 | 1.794E-4 | 31.261 | 28.135 |
| 2750 | 70.87 | 2.1930 | 15069 | 0.0020 | 11 | 1.787E-4 | 31.315 | 28.183 |
| 2750 | 71.04 | 2.1950 | 15080 | 0.0020 | 12 | 1.781E-4 | 31.369 | 28.232 |
| 2750 | 71.22 | 2.1970 | 15091 | 0.0041 | 23 | 1.768E-4 | 31.423 | 28.281 |
| 2750 | 71.40 | 2.1990 | 15103 | 0.0042 | 24 | 1.738E-4 | 31.479 | 28.331 |
| | 71.58 | 2.2011 | 15115 | | | | | |

Automated Fatigue Crack
Growth Rate Analysis

| | | | |
|-----------------|----------------|---------------|------|
| Test ID | 5086-FCG-4pt05 | Geometry | C(T) |
| Contract | SSC 10624-01 | Orientation | T-L |
| Material | 5086-H116 | Yield (ksi) | 27.0 |
| Temperature (F) | 75 | Modulus (Msi) | 10.5 |
| Environment | Sea Water | | |

Specimen Dimensions (in)

| | | | |
|---------------|-------|-------------|-------|
| Thickness | 0.496 | Height | 2.400 |
| Net Thickness | 0.496 | Notch Depth | 1.000 |
| Width | 4.000 | Gage Length | 0.500 |

Precrack Parameters

| | | | |
|--------------|-------|--------------------|------|
| Pmax (lbs) | 779.0 | Stress Ratio | 0.10 |
| Final a (in) | 1.050 | Kmax (ksi sqr[in]) | 4.00 |

Test Parameters

| EvBP | Freq | Pmax | R | Ai | Kmaxi | C | DKi |
|--------|------|------|------|-------|-------|------|------|
| 31.406 | 0.05 | 0 | 0.10 | 1.451 | 9.69 | 2.00 | 0.00 |
| 52.247 | 0.05 | 2750 | 0.10 | 0.000 | 0.00 | 0.00 | 0.00 |

| K Coeff | C Coeff |
|---------|----------|
| .886 | 1.00098 |
| 4.64 | -4.66951 |
| -13.32 | 18.4601 |
| 14.72 | -236.825 |
| -5.6 | 1214.88 |
| . | -2143.57 |

Visual Observations

| EvB/P | Crack(EvB/P) | Crack(visual) | Error | CAF |
|--------|--------------|---------------|--------|-------|
| 20.726 | 1.014 | 1.001 | -0.013 | 1.021 |
| 21.845 | 1.073 | 1.070 | -0.003 | 1.020 |
| 22.606 | 1.111 | 1.120 | 0.009 | 1.019 |
| 23.443 | 1.151 | 1.160 | 0.009 | 1.018 |
| 23.654 | 1.161 | 1.190 | 0.029 | 1.018 |
| 27.959 | 1.341 | 1.330 | -0.011 | 1.013 |
| 31.354 | 1.461 | 1.460 | -0.001 | 1.010 |
| 35.099 | 1.576 | 1.550 | -0.026 | 1.007 |
| 43.347 | 1.783 | 1.790 | 0.007 | 1.002 |
| 51.894 | 1.949 | 1.920 | -0.029 | 0.998 |
| 67.433 | 2.175 | 2.200 | 0.025 | 0.993 |

Comments

Date of test: 9/10/2006
Waveform Type Sine

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^-.5) | deltaK |
|--------------|-------|-----------|--------|------------|---------|-------------------|-----------------------|----------|
| | 32.94 | 1.5115 | 755158 | | | | | |
| 1562 | 32.97 | 1.5126 | 755226 | 0.0027 | 231 | 1.169E-5 | 10.821 | 9.737 |
| 1566 | 33.02 | 1.5142 | 755389 | 0.0038 | 351 | 1.078E-5 | 10.864 | 9.777 |
| 1570 | 33.09 | 1.5164 | 755577 | 0.0018 | 163 | 1.173E-5 | 10.904 | 9.814 |
| 1574 | 33.15 | 1.5183 | 755755 | 0.0019 | 182 | 1.071E-5 | 10.950 | 9.855 |
| 1579 | 33.22 | 1.5203 | 755947 | 0.0020 | 183 | 1.062E-5 | 10.994 | 9.894 |
| 1583 | 33.29 | 1.5223 | 756138 | 0.0019 | 182 | 1.058E-5 | 11.037 | 9.933 |
| 1587 | 33.35 | 1.5242 | 756316 | 0.0019 | 183 | 1.062E-5 | 11.081 | 9.973 |
| 1591 | 33.41 | 1.5260 | 756488 | 0.0019 | 177 | 1.074E-5 | 11.124 | 10.011 |
| 1595 | 33.47 | 1.5279 | 756667 | 0.0019 | 173 | 1.084E-5 | 11.168 | 10.051 |
| 1600 | 33.54 | 1.5299 | 756852 | 0.0019 | 173 | 1.101E-5 | 11.210 | 10.089 |
| 1604 | 33.60 | 1.5318 | 757010 | 0.0019 | 174 | 1.115E-5 | 11.254 | 10.128 |
| 1608 | 33.66 | 1.5335 | 757175 | 0.0020 | 172 | 1.136E-5 | 11.298 | 10.168 |
| 1612 | 33.72 | 1.5356 | 757354 | 0.0041 | 357 | 1.156E-5 | 11.343 | 10.208 |
| 1617 | 33.79 | 1.5377 | 757532 | 0.0041 | 343 | 1.190E-5 | 11.389 | 10.250 |
| 1621 | 33.86 | 1.5397 | 757697 | 0.6901 | -742402 | -9.296E-7 | 0.000 | 0.000 |
| 2750 | 71.93 | 2.2278 | 15130 | 0.6900 | -742558 | -9.292E-7 | 0.000 | 0.000 |
| 2750 | 72.09 | 2.2296 | 15139 | 0.0037 | 18 | 2.034E-4 | 32.322 | 29.095 * |
| 2750 | 72.25 | 2.2315 | 15148 | 0.0041 | 21 | 1.935E-4 | 32.382 | 29.144 * |
| 2750 | 72.45 | 2.2337 | 15160 | 0.0042 | 22 | 1.899E-4 | 32.436 | 29.192 * |
| 2750 | 72.63 | 2.2356 | 15170 | 0.0020 | 10 | 2.051E-4 | 32.497 | 29.247 * |
| 2750 | 72.81 | 2.2376 | 15179 | 0.0021 | 10 | 2.094E-4 | 32.556 | 29.300 * |
| 2750 | 73.00 | 2.2398 | 15189 | 0.0020 | 9 | 2.150E-4 | 32.613 | 29.352 * |
| 2750 | 73.18 | 2.2418 | 15198 | 0.0020 | 9 | 2.168E-4 | 32.673 | 29.405 * |
| 2750 | 73.36 | 2.2438 | 15207 | 0.0020 | 9 | 2.158E-4 | 32.729 | 29.457 * |
| 2750 | 73.53 | 2.2457 | 15216 | 0.0020 | 9 | 2.173E-4 | 32.788 | 29.509 * |
| 2750 | 73.72 | 2.2477 | 15226 | 0.0041 | 19 | 2.166E-4 | 32.845 | 29.561 * |
| 2750 | 73.91 | 2.2498 | 15235 | 0.0041 | 18 | 2.278E-4 | 32.905 | 29.615 * |
| | 74.10 | 2.2518 | 15244 | | | | | |

Automated Fatigue Crack
Growth Rate Analysis

| | | |
|-----------------|-------------------------|---------------|
| Test ID | 5086-FCG-4Cpt05Geometry | C(T) |
| Contract | SSC 10624-01 | Orientation |
| Material | 5086-H116 | Yield (ksi) |
| Temperature (F) | 75 | Modulus (Msi) |
| Environment | Sea Water | |

Specimen Dimensions (in)

| | | | |
|---------------|-------|-------------|-------|
| Thickness | 0.496 | Height | 2.400 |
| Net Thickness | 0.496 | Notch Depth | 1.000 |
| Width | 4.000 | Gage Length | 0.500 |

Precrack Parameters

| | | | |
|--------------|-------|--------------------|------|
| Pmax (lbs) | 779.0 | Stress Ratio | 0.10 |
| Final a (in) | 1.050 | Kmax (ksi sqr[in]) | 4.00 |

Test Parameters

| | | | | | | | |
|--------|------|------|------|-------|-------|------|------|
| EvBP | Freq | Pmax | R | Ai | Kmaxi | C | DKi |
| 31.406 | 0.05 | 0 | 0.10 | 1.451 | 9.69 | 2.00 | 0.00 |

| | |
|---------|----------|
| K Coeff | C Coeff |
| .886 | 1.00098 |
| 4.64 | -4.66951 |
| -13.32 | 18.4601 |
| 14.72 | -236.825 |
| -5.6 | 1214.88 |
| . | -2143.57 |

Visual Observations

| EvB/P | Crack(EvB/P) | Crack(visual) | Error | CAF |
|--------|--------------|---------------|--------|-------|
| 20.726 | 1.014 | 1.001 | -0.013 | 1.021 |
| 21.845 | 1.073 | 1.070 | -0.003 | 1.020 |
| 22.606 | 1.111 | 1.120 | 0.009 | 1.019 |
| 23.443 | 1.151 | 1.160 | 0.009 | 1.018 |
| 23.654 | 1.161 | 1.190 | 0.029 | 1.018 |
| 27.959 | 1.341 | 1.330 | -0.011 | 1.013 |
| 31.354 | 1.461 | 1.460 | -0.001 | 1.010 |
| 35.099 | 1.576 | 1.550 | -0.026 | 1.007 |
| 43.347 | 1.783 | 1.790 | 0.007 | 1.002 |
| 51.894 | 1.949 | 1.920 | -0.029 | 0.998 |
| 67.433 | 2.175 | 2.200 | 0.025 | 0.993 |

Comments

Date of test: 9/10/2006
Waveform Type Sine

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in]^0.5) |
|--------------|-------|-----------|------|------------|-----|-------------------|--------|-------------------------|
| | 33.92 | 1.5415 | 89 | | | | | |
| 1630 | 33.98 | 1.5433 | 190 | 0.0037 | 223 | 1.659E-5 | 11.524 | 10.372 |
| 1634 | 34.05 | 1.5452 | 312 | 0.0042 | 267 | 1.572E-5 | 11.570 | 10.413 |
| 1639 | 34.12 | 1.5475 | 457 | 0.0020 | 123 | 1.587E-5 | 11.617 | 10.455 |
| 1644 | 34.19 | 1.5494 | 583 | 0.0020 | 127 | 1.558E-5 | 11.665 | 10.499 |
| 1648 | 34.25 | 1.5513 | 705 | 0.0020 | 128 | 1.559E-5 | 11.712 | 10.541 |
| 1652 | 34.32 | 1.5533 | 827 | 0.0019 | 123 | 1.572E-5 | 11.757 | 10.582 |
| 1657 | 34.38 | 1.5552 | 953 | 0.0019 | 121 | 1.589E-5 | 11.806 | 10.626 |
| 1661 | 34.45 | 1.5572 | 1079 | 0.0020 | 121 | 1.602E-5 | 11.851 | 10.666 |
| 1666 | 34.51 | 1.5590 | 1192 | 0.0019 | 119 | 1.608E-5 | 11.899 | 10.709 |
| 1670 | 34.58 | 1.5610 | 1310 | 0.0019 | 117 | 1.644E-5 | 11.944 | 10.750 |
| 1675 | 34.65 | 1.5630 | 1431 | 0.0019 | 115 | 1.669E-5 | 11.991 | 10.792 |
| 1679 | 34.71 | 1.5648 | 1540 | 0.0019 | 113 | 1.699E-5 | 12.040 | 10.836 |
| 1684 | 34.78 | 1.5669 | 1657 | 0.0019 | 114 | 1.708E-5 | 12.085 | 10.876 |
| 1688 | 34.85 | 1.5687 | 1766 | 0.0020 | 112 | 1.747E-5 | 12.135 | 10.922 |
| 1693 | 34.91 | 1.5707 | 1870 | 0.0038 | 226 | 1.696E-5 | 12.180 | 10.962 |
| 1697 | 34.98 | 1.5725 | 1992 | 0.0041 | 235 | 1.762E-5 | 12.233 | 11.010 |
| | 35.06 | 1.5748 | 2105 | | | | | |

Automated Fatigue Crack
Growth Rate Analysis

| | | | |
|-----------------|--------------|---------------|------|
| Test ID | 5086-FCG-5 | Geometry | C(T) |
| Contract | SSC 10624-01 | Orientation | T-L |
| Material | 5086-H116 | Yield (ksi) | 27.0 |
| Temperature (F) | 75 | Modulus (Msi) | 10.5 |
| Environment | RH = 40% | | |

Specimen Dimensions (in)

| | | | |
|---------------|-------|-------------|-------|
| Thickness | 0.497 | Height | 2.400 |
| Net Thickness | 0.497 | Notch Depth | 1.000 |
| Width | 4.000 | Gage Length | 0.500 |

Precrack Parameters

| | | | |
|--------------|-------|--------------------------------|------|
| Pmax (lbs) | 962.0 | Stress Ratio | 0.10 |
| Final a (in) | 1.070 | Kmax (ksi $\sqrt{\text{in}}$) | 5.00 |

Test Parameters

| | | | | | | | |
|--------|-------|------|------|-------|-------|-------|------|
| EvBP | Freq | Pmax | R | Ai | Kmaxi | C | DKi |
| 22.290 | 24.00 | 0 | 0.10 | 1.070 | 5.00 | -4.00 | 0.00 |
| 24.852 | 24.00 | 0 | 0.10 | 1.190 | 3.40 | 4.00 | 0.00 |

| | | |
|---------|----------|------------------------------|
| K Coeff | C Coeff | da/dN Fit Parameters (DKapp) |
| .886 | 1.00098 | Upper da/dN limit |
| 4.64 | -4.66951 | Lower da/dN limit |
| -13.32 | 18.4601 | da/dN intercept (C) |
| 14.72 | -236.825 | da/dN slope (m) |
| -5.6 | 1214.88 | da/dN for delta K |
| . | -2143.57 | delta K |

Visual Observations

| | | | | |
|--------|--------------|---------------|--------|-------|
| EvB/P | Crack(EvB/P) | Crack(visual) | Error | CAF |
| 20.547 | 0.990 | 1.000 | 0.011 | 1.009 |
| 22.223 | 1.089 | 1.070 | -0.019 | 1.016 |
| 24.200 | 1.194 | 1.190 | -0.004 | 1.024 |
| 24.485 | 1.208 | 1.220 | 0.012 | 1.025 |
| 25.589 | 1.242 | 1.250 | 0.008 | 1.011 |
| 28.155 | 1.334 | 1.325 | -0.009 | 0.999 |
| 31.334 | 1.435 | 1.430 | -0.005 | 0.987 |
| 36.192 | 1.569 | 1.575 | 0.006 | 0.971 |

Comments

Date of test: 9/19/2006
Waveform Type Sine

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in]^0.5) |
|--------------|-------|-----------|---------|------------|----------|-------------------|-------|-------------------------|
| | 22.29 | 1.0928 | 9610 | | | | | |
| 928 | 22.37 | 1.0972 | 21809 | 0.0099 | 29163 | 3.389E-7 | 4.905 | 4.414 |
| 907 | 22.47 | 1.1026 | 38773 | 0.0107 | 35479 | 3.005E-7 | 4.820 | 4.338 |
| 887 | 22.57 | 1.1079 | 57288 | 0.0053 | 20154 | 2.987E-7 | 4.724 | 4.252 |
| 866 | 22.67 | 1.1135 | 79640 | 0.0055 | 22614 | 2.590E-7 | 4.632 | 4.169 |
| 845 | 22.77 | 1.1193 | 105089 | 0.0055 | 24474 | 2.334E-7 | 4.542 | 4.088 |
| 826 | 22.87 | 1.1245 | 130533 | 0.0055 | 25268 | 2.154E-7 | 4.449 | 4.004 |
| 807 | 22.98 | 1.1302 | 157491 | 0.0053 | 27199 | 2.021E-7 | 4.364 | 3.928 |
| 788 | 23.08 | 1.1357 | 185617 | 0.0053 | 30028 | 1.920E-7 | 4.282 | 3.854 |
| 772 | 23.17 | 1.1407 | 208893 | 0.0055 | 33464 | 1.847E-7 | 4.198 | 3.779 |
| 755 | 23.26 | 1.1452 | 242836 | 0.0054 | 37154 | 1.675E-7 | 4.123 | 3.711 |
| 738 | 23.37 | 1.1511 | 285255 | 0.0055 | 39032 | 1.447E-7 | 4.029 | 3.626 |
| 715 | 23.49 | 1.1575 | 331318 | 0.0054 | 43992 | 1.292E-7 | 3.962 | 3.566 |
| 703 | 23.58 | 1.1624 | 380414 | 0.0056 | 50772 | 1.200E-7 | 3.866 | 3.479 |
| 684 | 23.70 | 1.1686 | 419811 | 0.0055 | 58616 | 1.138E-7 | 3.805 | 3.424 |
| 670 | 23.79 | 1.1732 | 472844 | 0.0052 | 67607 | 1.020E-7 | 3.726 | 3.353 |
| 655 | 23.90 | 1.1785 | 547467 | 0.0048 | 76435 | 8.309E-8 | 3.656 | 3.290 |
| 640 | 24.01 | 1.1842 | 636950 | 0.0041 | 86511 | 5.617E-8 | 3.591 | 3.232 |
| 628 | 24.09 | 1.1885 | 736959 | 0.0035 | 94315 | 3.915E-8 | 3.537 | 3.183 |
| 620 | 24.14 | 1.1911 | 839022 | 0.0027 | 98521 | 2.634E-8 | 3.495 | 3.146 |
| 615 | 24.18 | 1.1931 | 938878 | 0.0019 | 100250 | 1.747E-8 | 3.472 | 3.124 |
| 612 | 24.20 | 1.1939 | 1038734 | 0.0014 | 100838 | 1.289E-8 | 3.456 | 3.110 |
| 611 | 24.21 | 1.1946 | 1138591 | 0.0012 | 100470 | 1.112E-8 | 3.442 | 3.098 |
| 608 | 24.23 | 1.1956 | 1238447 | 0.0011 | 100470 | 1.080E-8 | 3.430 | 3.087 |
| 604 | 24.26 | 1.1970 | 1341989 | 0.0011 | 100471 | 1.125E-8 | 3.416 | 3.074 |
| 601 | 24.29 | 1.1983 | 1441844 | 0.0011 | 100471 | 1.095E-8 | 3.398 | 3.058 |
| 598 | 24.31 | 1.1995 | 1541700 | 0.0009 | 100468 | 9.168E-9 | 3.386 | 3.048 |
| 596 | 24.33 | 1.2003 | 1641557 | 0.0006 | 99854 | 6.044E-9 | 3.373 | 3.036 |
| 594 | 24.34 | 1.2009 | 1741414 | 0.0005 | 99854 | 4.054E-9 | 3.363 | 3.026 |
| 592 | 24.34 | 1.2009 | 1841257 | -0.0005 | 199697 | -2.307E-9 | 3.357 | 3.021 |
| 592 | 24.33 | 1.2005 | 1941111 | 0.0003 | 199710 | 1.530E-9 | 3.351 | 3.016 |
| 592 | 24.34 | 1.2012 | 2040967 | 0.0745 | -1011432 | -7.369E-8 | 0.000 | 0.000 |
| 783 | 26.49 | 1.2750 | 929679 | 0.0779 | -1091165 | -7.140E-8 | 0.000 | 0.000 |
| 796 | 26.60 | 1.2792 | 949802 | 0.0086 | 38114 | 2.256E-7 | 4.741 | 4.267 |
| 809 | 26.72 | 1.2836 | 967793 | 0.0088 | 33336 | 2.634E-7 | 4.833 | 4.349 |
| 823 | 26.84 | 1.2879 | 983138 | 0.0087 | 28228 | 3.089E-7 | 4.929 | 4.436 |
| 837 | 26.97 | 1.2923 | 996021 | 0.0044 | 13200 | 3.453E-7 | 5.024 | 4.522 |
| 850 | 27.08 | 1.2966 | 1007541 | 0.0044 | 11575 | 3.871E-7 | 5.122 | 4.610 |
| 864 | 27.20 | 1.3007 | 1018820 | 0.0044 | 10181 | 4.427E-7 | 5.225 | 4.702 |
| 880 | 27.34 | 1.3055 | 1029002 | 0.0044 | 9069 | 5.114E-7 | 5.326 | 4.793 |
| 895 | 27.46 | 1.3098 | 1037242 | 0.0044 | 8132 | 5.856E-7 | 5.434 | 4.891 |
| 910 | 27.59 | 1.3142 | 1044225 | 0.0045 | 7091 | 6.629E-7 | 5.541 | 4.987 |
| 925 | 27.71 | 1.3185 | 1050435 | 0.0044 | 6131 | 7.452E-7 | 5.651 | 5.086 |
| 941 | 27.84 | 1.3231 | 1056334 | 0.0044 | 5454 | 8.287E-7 | 5.763 | 5.187 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in]^-.5) |
|--------------|-------|-----------|---------|------------|------|-------------------|-------|-------------------------|
| 957 | 27.97 | 1.3274 | 1061365 | 0.0044 | 4952 | 9.127E-7 | 5.879 | 5.291 |
| 973 | 28.10 | 1.3318 | 1065787 | 0.0045 | 4514 | 1.007E-6 | 5.992 | 5.393 |
| 989 | 28.22 | 1.3360 | 1069963 | 0.0044 | 4008 | 1.123E-6 | 6.113 | 5.502 |
| 1006 | 28.35 | 1.3406 | 1073939 | 0.0044 | 3594 | 1.260E-6 | 6.233 | 5.610 |
| 1024 | 28.49 | 1.3452 | 1077518 | 0.0044 | 3259 | 1.421E-6 | 6.359 | 5.723 |
| 1041 | 28.62 | 1.3496 | 1080382 | 0.0045 | 2923 | 1.594E-6 | 6.485 | 5.837 |
| 1058 | 28.75 | 1.3538 | 1082926 | 0.0044 | 2565 | 1.791E-6 | 6.613 | 5.951 |
| 1076 | 28.88 | 1.3582 | 1085340 | 0.0044 | 2239 | 2.019E-6 | 6.744 | 6.069 |
| 1095 | 29.02 | 1.3627 | 1087499 | 0.0044 | 2006 | 2.296E-6 | 6.876 | 6.188 |
| 1113 | 29.15 | 1.3672 | 1089328 | 0.0044 | 1799 | 2.589E-6 | 7.014 | 6.313 |
| 1132 | 29.29 | 1.3715 | 1090954 | 0.0044 | 1592 | 2.904E-6 | 7.154 | 6.439 |
| 1151 | 29.43 | 1.3760 | 1092418 | 0.0044 | 1406 | 3.255E-6 | 7.295 | 6.565 |
| 1171 | 29.56 | 1.3804 | 1093719 | 0.0044 | 1258 | 3.654E-6 | 7.440 | 6.696 |
| 1190 | 29.70 | 1.3848 | 1094889 | 0.0044 | 1126 | 4.054E-6 | 7.588 | 6.829 |
| 1211 | 29.84 | 1.3892 | 1095933 | 0.0044 | 1014 | 4.454E-6 | 7.739 | 6.966 |
| 1232 | 29.98 | 1.3938 | 1096876 | 0.0044 | 921 | 4.882E-6 | 7.891 | 7.102 |
| 1252 | 30.11 | 1.3979 | 1097711 | 0.0044 | 844 | 5.257E-6 | 8.046 | 7.241 |
| 1272 | 30.25 | 1.4023 | 1098502 | 0.0044 | 781 | 5.641E-6 | 8.205 | 7.384 |
| 1294 | 30.40 | 1.4068 | 1099246 | 0.0044 | 725 | 6.091E-6 | 8.361 | 7.525 |
| 1316 | 30.53 | 1.4110 | 1099951 | 0.0044 | 675 | 6.571E-6 | 8.531 | 7.678 |
| 1338 | 30.68 | 1.4155 | 1100621 | 0.0044 | 633 | 7.067E-6 | 8.699 | 7.829 |
| 1361 | 30.83 | 1.4202 | 1101225 | 0.0044 | 595 | 7.573E-6 | 8.869 | 7.982 |
| 1383 | 30.97 | 1.4243 | 1101763 | 0.0087 | 1077 | 8.052E-6 | 9.049 | 8.144 |
| 1407 | 31.11 | 1.4288 | 1102302 | 0.0091 | 1051 | 8.619E-6 | 9.226 | 8.304 |
| | 31.27 | 1.4334 | 1102814 | | | | | |

Automated Fatigue Crack
Growth Rate Analysis

| | | | |
|-----------------|--------------|---------------|------|
| Test ID | 5383-FCG-1 | Geometry | C(T) |
| Contract | SSC 10624-01 | Orientation | T-L |
| Material | 5383-H116 | Yield (ksi) | 35.4 |
| Temperature (F) | 75 | Modulus (Msi) | 10.5 |
| Environment | RH = 40% | | |

Specimen Dimensions (in)

| | | | |
|---------------|-------|-------------|-------|
| Thickness | 0.488 | Height | 2.400 |
| Net Thickness | 0.488 | Notch Depth | 1.000 |
| Width | 4.000 | Gage Length | 0.500 |

Precrack Parameters

| | | | |
|--------------|-------|--------------------|------|
| Pmax (lbs) | 861.0 | Stress Ratio | 0.10 |
| Final a (in) | 1.050 | Kmax (ksi sqr[in]) | 4.50 |

Test Parameters

| EvBP | Freq | Pmax | R | Ai | Kmaxi | C | DKi |
|--------|-------|------|------|-------|-------|------|------|
| 24.226 | 10.00 | 0 | 0.10 | 1.170 | 3.00 | 2.00 | 0.00 |
| 32.427 | 10.00 | 0 | 0.10 | 1.486 | 10.58 | 2.00 | 0.00 |
| 51.111 | 5.00 | 2675 | 0.10 | 0.000 | 0.00 | 0.00 | 0.00 |

| K Coeff | C Coeff |
|---------|----------|
| .886 | 1.00098 |
| 4.64 | -4.66951 |
| -13.32 | 18.4601 |
| 14.72 | -236.825 |
| -5.6 | 1214.88 |
| . | -2143.57 |

Visual Observations

| EvB/P | Crack(EvB/P) | Crack(visual) | Error | CAF |
|--------|--------------|---------------|--------|-------|
| 20.829 | 0.994 | 1.001 | 0.007 | 0.999 |
| 21.843 | 1.046 | 1.045 | -0.001 | 0.996 |
| 24.198 | 1.157 | 1.160 | 0.003 | 0.991 |
| 24.815 | 1.184 | 1.185 | 0.001 | 0.990 |
| 26.085 | 1.237 | 1.235 | -0.002 | 0.988 |
| 28.304 | 1.322 | 1.315 | -0.007 | 0.984 |
| 32.405 | 1.461 | 1.455 | -0.006 | 0.977 |
| 43.793 | 1.755 | 1.760 | 0.005 | 0.965 |
| 50.785 | 1.892 | 1.890 | -0.002 | 0.959 |
| 98.246 | 2.423 | 2.425 | 0.002 | 0.937 |

Comments

Date of test: 8/24/2006
Waveform Type Sine

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in]^0.5) |
|--------------|-------|-----------|---------|------------|--------|-------------------|-------|-------------------------|
| | 24.23 | 1.1583 | 21299 | | | | | |
| 534 | 24.31 | 1.1621 | 84307 | 0.0088 | 141260 | 6.236E-8 | 3.014 | 2.712 |
| 544 | 24.43 | 1.1671 | 162559 | 0.0097 | 149583 | 6.490E-8 | 3.068 | 2.761 |
| 553 | 24.53 | 1.1718 | 233890 | 0.0047 | 66040 | 7.106E-8 | 3.131 | 2.818 |
| 562 | 24.64 | 1.1765 | 297453 | 0.0049 | 64780 | 7.560E-8 | 3.193 | 2.874 |
| 572 | 24.75 | 1.1813 | 356275 | 0.0048 | 59979 | 8.078E-8 | 3.258 | 2.932 |
| 582 | 24.87 | 1.1863 | 417537 | 0.0048 | 55917 | 8.680E-8 | 3.324 | 2.992 |
| 592 | 24.99 | 1.1912 | 472986 | 0.0048 | 52897 | 9.193E-8 | 3.392 | 3.053 |
| 602 | 25.10 | 1.1960 | 522431 | 0.0049 | 50414 | 9.707E-8 | 3.461 | 3.115 |
| 612 | 25.21 | 1.2008 | 569390 | 0.0048 | 47020 | 1.027E-7 | 3.529 | 3.176 |
| 622 | 25.32 | 1.2055 | 614832 | 0.0048 | 44090 | 1.084E-7 | 3.601 | 3.241 |
| 633 | 25.44 | 1.2104 | 658759 | 0.0048 | 41908 | 1.148E-7 | 3.673 | 3.305 |
| 644 | 25.56 | 1.2152 | 699657 | 0.0048 | 39888 | 1.214E-7 | 3.747 | 3.372 |
| 654 | 25.67 | 1.2200 | 737525 | 0.0048 | 37616 | 1.285E-7 | 3.824 | 3.441 |
| 666 | 25.79 | 1.2249 | 773879 | 0.0048 | 35596 | 1.352E-7 | 3.900 | 3.510 |
| 677 | 25.91 | 1.2297 | 808718 | 0.0048 | 33829 | 1.418E-7 | 3.979 | 3.581 |
| 688 | 26.02 | 1.2344 | 840527 | 0.0048 | 32012 | 1.485E-7 | 4.059 | 3.653 |
| 700 | 26.14 | 1.2392 | 872337 | 0.0047 | 30396 | 1.560E-7 | 4.139 | 3.725 |
| 712 | 26.26 | 1.2440 | 902631 | 0.0047 | 28831 | 1.643E-7 | 4.222 | 3.800 |
| 724 | 26.38 | 1.2486 | 929595 | 0.0047 | 27368 | 1.734E-7 | 4.306 | 3.876 |
| 736 | 26.50 | 1.2533 | 956256 | 0.0047 | 25661 | 1.851E-7 | 4.391 | 3.952 |
| 748 | 26.62 | 1.2581 | 981706 | 0.0048 | 24005 | 1.987E-7 | 4.478 | 4.030 |
| 761 | 26.74 | 1.2628 | 1004732 | 0.0048 | 22582 | 2.139E-7 | 4.569 | 4.112 |
| 774 | 26.86 | 1.2676 | 1026304 | 0.0048 | 20885 | 2.322E-7 | 4.660 | 4.194 |
| 787 | 26.98 | 1.2725 | 1046663 | 0.0048 | 19099 | 2.562E-7 | 4.755 | 4.279 |
| 800 | 27.11 | 1.2773 | 1065085 | 0.0048 | 17251 | 2.870E-7 | 4.850 | 4.365 |
| 814 | 27.23 | 1.2821 | 1081564 | 0.0048 | 15310 | 3.290E-7 | 4.950 | 4.455 |
| 828 | 27.36 | 1.2871 | 1096297 | 0.0048 | 13407 | 3.827E-7 | 5.048 | 4.544 |
| 842 | 27.48 | 1.2917 | 1108239 | 0.0048 | 11594 | 4.467E-7 | 5.150 | 4.635 |
| 856 | 27.61 | 1.2964 | 1118166 | 0.0048 | 9920 | 5.241E-7 | 5.252 | 4.727 |
| 870 | 27.73 | 1.3011 | 1127103 | 0.0047 | 8365 | 6.138E-7 | 5.357 | 4.821 |
| 885 | 27.86 | 1.3059 | 1134650 | 0.0047 | 7179 | 7.125E-7 | 5.465 | 4.919 |
| 901 | 27.99 | 1.3109 | 1141085 | 0.0048 | 6278 | 8.166E-7 | 5.574 | 5.016 |
| 916 | 28.12 | 1.3155 | 1146484 | 0.0048 | 5433 | 9.261E-7 | 5.686 | 5.118 |
| 931 | 28.24 | 1.3201 | 1151311 | 0.0047 | 4744 | 1.040E-6 | 5.800 | 5.220 |
| 947 | 28.38 | 1.3250 | 1155836 | 0.0048 | 4240 | 1.162E-6 | 5.914 | 5.323 |
| 963 | 28.51 | 1.3298 | 1159698 | 0.0048 | 3828 | 1.302E-6 | 6.033 | 5.430 |
| 979 | 28.63 | 1.3344 | 1163113 | 0.0048 | 3414 | 1.460E-6 | 6.156 | 5.541 |
| 996 | 28.77 | 1.3394 | 1166527 | 0.0048 | 3007 | 1.655E-6 | 6.281 | 5.653 |
| 1013 | 28.91 | 1.3445 | 1169454 | 0.0048 | 2711 | 1.852E-6 | 6.409 | 5.768 |
| 1030 | 29.04 | 1.3492 | 1171795 | 0.0049 | 2471 | 2.045E-6 | 6.537 | 5.883 |
| 1047 | 29.17 | 1.3537 | 1173878 | 0.0048 | 2184 | 2.246E-6 | 6.667 | 6.000 |
| 1065 | 29.31 | 1.3584 | 1175961 | 0.0047 | 1933 | 2.487E-6 | 6.801 | 6.121 |
| 1084 | 29.45 | 1.3636 | 1177940 | 0.0047 | 1766 | 2.751E-6 | 6.938 | 6.244 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in]^0.5) |
|--------------|-------|-----------|---------|------------|------|-------------------|--------|-------------------------|
| 1102 | 29.59 | 1.3683 | 1179628 | 0.0048 | 1631 | 3.031E-6 | 7.079 | 6.371 |
| 1121 | 29.72 | 1.3730 | 1181049 | 0.0048 | 1482 | 3.308E-6 | 7.218 | 6.496 |
| 1138 | 29.85 | 1.3775 | 1182390 | 0.0047 | 1339 | 3.582E-6 | 7.361 | 6.625 |
| 1158 | 29.99 | 1.3823 | 1183665 | 0.0047 | 1236 | 3.864E-6 | 7.506 | 6.756 |
| 1178 | 30.14 | 1.3872 | 1184855 | 0.0048 | 1159 | 4.135E-6 | 7.656 | 6.890 |
| 1197 | 30.28 | 1.3919 | 1185975 | 0.0048 | 1085 | 4.424E-6 | 7.812 | 7.031 |
| 1218 | 30.42 | 1.3968 | 1187042 | 0.0048 | 1022 | 4.721E-6 | 7.966 | 7.169 |
| 1238 | 30.56 | 1.4015 | 1188003 | 0.0048 | 959 | 5.032E-6 | 8.126 | 7.313 |
| 1259 | 30.70 | 1.4062 | 1188899 | 0.0048 | 899 | 5.358E-6 | 8.289 | 7.460 |
| 1281 | 30.85 | 1.4111 | 1189795 | 0.0048 | 842 | 5.725E-6 | 8.455 | 7.609 |
| 1302 | 31.00 | 1.4159 | 1190607 | 0.0048 | 797 | 6.063E-6 | 8.628 | 7.765 |
| 1325 | 31.14 | 1.4207 | 1191371 | 0.0048 | 758 | 6.408E-6 | 8.802 | 7.922 |
| 1347 | 31.29 | 1.4256 | 1192096 | 0.0048 | 710 | 6.784E-6 | 8.978 | 8.081 |
| 1370 | 31.44 | 1.4303 | 1192787 | 0.0048 | 671 | 7.132E-6 | 9.159 | 8.243 |
| 1393 | 31.59 | 1.4352 | 1193444 | 0.0048 | 635 | 7.498E-6 | 9.345 | 8.410 |
| 1417 | 31.74 | 1.4400 | 1194057 | 0.0047 | 601 | 7.903E-6 | 9.527 | 8.574 |
| 1440 | 31.88 | 1.4446 | 1194633 | 0.0048 | 567 | 8.384E-6 | 9.718 | 8.747 |
| 1464 | 32.03 | 1.4493 | 1195182 | 0.0095 | 1070 | 8.871E-6 | 9.907 | 8.916 |
| 1488 | 32.18 | 1.4541 | 1195703 | 0.0096 | 1008 | 9.554E-6 | 10.106 | 9.095 |
| | 32.33 | 1.4589 | 1196190 | | | | | |
| | 32.43 | 1.4618 | 1196914 | | | | | |
| 1545 | 32.72 | 1.4710 | 1197845 | 0.0190 | 1943 | 9.781E-6 | 10.615 | 9.553 |
| 1567 | 33.04 | 1.4808 | 1198857 | 0.0199 | 1945 | 1.022E-5 | 10.822 | 9.740 |
| 1589 | 33.37 | 1.4908 | 1199790 | 0.0193 | 1763 | 1.095E-5 | 11.035 | 9.932 |
| 1609 | 33.69 | 1.5001 | 1200620 | 0.0097 | 866 | 1.121E-5 | 11.257 | 10.131 |
| 1631 | 34.00 | 1.5095 | 1201449 | 0.0097 | 812 | 1.184E-5 | 11.480 | 10.332 |
| 1654 | 34.34 | 1.5194 | 1202278 | 0.0096 | 772 | 1.246E-5 | 11.707 | 10.536 |
| 1676 | 34.68 | 1.5292 | 1203038 | 0.0097 | 743 | 1.308E-5 | 11.944 | 10.750 |
| 1699 | 35.02 | 1.5389 | 1203730 | 0.0097 | 707 | 1.372E-5 | 12.182 | 10.964 |
| 1722 | 35.36 | 1.5485 | 1204420 | 0.0096 | 669 | 1.437E-5 | 12.425 | 11.183 |
| 1745 | 35.70 | 1.5581 | 1205077 | 0.0096 | 639 | 1.494E-5 | 12.672 | 11.405 |
| 1769 | 36.05 | 1.5676 | 1205690 | 0.0096 | 615 | 1.552E-5 | 12.923 | 11.631 |
| 1792 | 36.40 | 1.5772 | 1206293 | 0.0096 | 591 | 1.619E-5 | 13.176 | 11.859 |
| 1816 | 36.75 | 1.5865 | 1206870 | 0.0096 | 569 | 1.688E-5 | 13.439 | 12.095 |
| 1840 | 37.11 | 1.5963 | 1207418 | 0.0097 | 548 | 1.762E-5 | 13.702 | 12.332 |
| 1865 | 37.48 | 1.6060 | 1207967 | 0.0097 | 524 | 1.846E-5 | 13.980 | 12.582 |
| 1890 | 37.86 | 1.6158 | 1208489 | 0.0097 | 500 | 1.942E-5 | 14.263 | 12.837 |
| 1917 | 38.25 | 1.6257 | 1208976 | 0.0097 | 478 | 2.042E-5 | 14.546 | 13.092 |
| 1942 | 38.62 | 1.6351 | 1209435 | 0.0096 | 449 | 2.151E-5 | 14.843 | 13.359 |
| 1968 | 39.02 | 1.6450 | 1209872 | 0.0096 | 424 | 2.267E-5 | 15.135 | 13.622 |
| 1994 | 39.41 | 1.6547 | 1210287 | 0.0096 | 403 | 2.394E-5 | 15.431 | 13.888 |
| 2020 | 39.78 | 1.6638 | 1210661 | 0.0096 | 381 | 2.514E-5 | 15.740 | 14.166 |
| 2047 | 40.19 | 1.6735 | 1211035 | 0.0096 | 363 | 2.646E-5 | 16.048 | 14.443 |
| 2074 | 40.60 | 1.6834 | 1211391 | 0.0096 | 343 | 2.799E-5 | 16.362 | 14.726 |
| 2101 | 40.99 | 1.6926 | 1211721 | 0.0097 | 326 | 2.964E-5 | 16.695 | 15.026 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in] ^{0.5}) |
|--------------|-------|-----------|---------|------------|-----|-------------------|--------|-------------------------------------|
| 2129 | 41.42 | 1.7026 | 1212049 | 0.0096 | 308 | 3.148E-5 | 17.022 | 15.320 |
| 2157 | 41.85 | 1.7123 | 1212347 | 0.0096 | 291 | 3.336E-5 | 17.362 | 15.626 |
| 2185 | 42.27 | 1.7218 | 1212618 | 0.0097 | 275 | 3.534E-5 | 17.707 | 15.937 |
| 2214 | 42.70 | 1.7313 | 1212880 | 0.0097 | 256 | 3.764E-5 | 18.056 | 16.251 |
| 2243 | 43.14 | 1.7411 | 1213137 | 0.0097 | 242 | 4.015E-5 | 18.413 | 16.572 |
| 2272 | 43.58 | 1.7508 | 1213372 | 0.0098 | 230 | 4.273E-5 | 18.782 | 16.904 |
| 2302 | 44.04 | 1.7606 | 1213587 | 0.0097 | 216 | 4.549E-5 | 19.158 | 17.242 |
| 2333 | 44.50 | 1.7704 | 1213797 | 0.0097 | 202 | 4.841E-5 | 19.546 | 17.591 |
| 2364 | 44.98 | 1.7804 | 1213999 | 0.0098 | 190 | 5.172E-5 | 19.930 | 17.938 |
| 2393 | 45.44 | 1.7897 | 1214173 | 0.0098 | 179 | 5.492E-5 | 20.332 | 18.299 |
| 2424 | 45.91 | 1.7994 | 1214346 | 0.0097 | 165 | 5.909E-5 | 20.741 | 18.667 |
| 2458 | 46.43 | 1.8098 | 1214514 | 0.0097 | 153 | 6.392E-5 | 21.146 | 19.031 |
| 2488 | 46.90 | 1.8192 | 1214659 | 0.0097 | 144 | 6.854E-5 | 21.573 | 19.416 |
| 2519 | 47.38 | 1.8286 | 1214788 | 0.0097 | 134 | 7.319E-5 | 21.997 | 19.797 |
| 2552 | 47.89 | 1.8384 | 1214916 | 0.0097 | 124 | 7.856E-5 | 22.427 | 20.185 |
| 2585 | 48.41 | 1.8481 | 1215038 | 0.0097 | 117 | 8.371E-5 | 22.871 | 20.585 |
| 2617 | 48.91 | 1.8577 | 1215149 | 0.0098 | 111 | 8.849E-5 | 23.335 | 21.002 |
| 2652 | 49.46 | 1.8678 | 1215256 | 0.0198 | 209 | 9.473E-5 | 23.792 | 21.413 |
| 2685 | 49.99 | 1.8775 | 1215358 | 0.0194 | 198 | 9.810E-5 | 24.274 | 21.846 |
| | 50.54 | 1.8872 | 1215454 | | | | | |
| | 51.11 | 1.8974 | 1215566 | | | | | |
| 2675 | 51.61 | 1.9062 | 1215661 | 0.0185 | 197 | 9.368E-5 | 24.702 | 22.231 |
| 2675 | 52.17 | 1.9159 | 1215763 | 0.0199 | 200 | 9.952E-5 | 24.876 | 22.388 |
| 2675 | 52.78 | 1.9261 | 1215861 | 0.0200 | 187 | 1.071E-4 | 25.055 | 22.550 |
| 2675 | 53.36 | 1.9359 | 1215950 | 0.0099 | 91 | 1.087E-4 | 25.241 | 22.717 |
| 2675 | 53.95 | 1.9456 | 1216035 | 0.0099 | 87 | 1.126E-4 | 25.424 | 22.881 |
| 2675 | 54.53 | 1.9550 | 1216121 | 0.0098 | 85 | 1.156E-4 | 25.615 | 23.053 |
| 2675 | 55.17 | 1.9653 | 1216206 | 0.0097 | 83 | 1.176E-4 | 25.801 | 23.221 |
| 2675 | 55.79 | 1.9751 | 1216287 | 0.0097 | 81 | 1.197E-4 | 25.999 | 23.399 |
| 2675 | 56.42 | 1.9849 | 1216369 | 0.0098 | 79 | 1.229E-4 | 26.189 | 23.570 |
| 2675 | 57.03 | 1.9943 | 1216446 | 0.0097 | 76 | 1.269E-4 | 26.385 | 23.746 |
| 2675 | 57.67 | 2.0040 | 1216522 | 0.0097 | 73 | 1.326E-4 | 26.583 | 23.924 |
| 2675 | 58.34 | 2.0140 | 1216596 | 0.0097 | 70 | 1.391E-4 | 26.780 | 24.101 |
| 2675 | 58.98 | 2.0234 | 1216659 | 0.0098 | 69 | 1.432E-4 | 26.985 | 24.286 |
| 2675 | 59.65 | 2.0331 | 1216724 | 0.0098 | 67 | 1.471E-4 | 27.191 | 24.472 |
| 2675 | 60.36 | 2.0431 | 1216790 | 0.0098 | 65 | 1.506E-4 | 27.399 | 24.659 |
| 2675 | 61.06 | 2.0529 | 1216858 | 0.0099 | 64 | 1.530E-4 | 27.613 | 24.852 |
| 2675 | 61.76 | 2.0626 | 1216921 | 0.0099 | 64 | 1.559E-4 | 27.831 | 25.048 |
| 2675 | 62.50 | 2.0727 | 1216983 | 0.0098 | 62 | 1.591E-4 | 28.050 | 25.245 |
| 2675 | 63.24 | 2.0826 | 1217043 | 0.0098 | 60 | 1.634E-4 | 28.277 | 25.449 |
| 2675 | 64.00 | 2.0926 | 1217105 | 0.0098 | 58 | 1.688E-4 | 28.500 | 25.650 |
| 2675 | 64.74 | 2.1022 | 1217162 | 0.0098 | 55 | 1.764E-4 | 28.726 | 25.853 |
| 2675 | 65.49 | 2.1117 | 1217216 | 0.0098 | 53 | 1.847E-4 | 28.954 | 26.059 |
| 2675 | 66.27 | 2.1216 | 1217266 | 0.0097 | 51 | 1.935E-4 | 29.187 | 26.268 |
| 2675 | 67.09 | 2.1316 | 1217315 | 0.0099 | 48 | 2.041E-4 | 29.422 | 26.479 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^0.5) | deltaK |
|--------------|--------|-----------|---------|------------|----|-------------------|-----------------------|----------|
| 2675 | 67.87 | 2.1412 | 1217362 | 0.0099 | 46 | 2.158E-4 | 29.665 | 26.698 |
| 2675 | 68.69 | 2.1509 | 1217408 | 0.0099 | 43 | 2.303E-4 | 29.914 | 26.922 |
| 2675 | 69.59 | 2.1615 | 1217452 | 0.0098 | 41 | 2.442E-4 | 30.160 | 27.144 |
| 2675 | 70.44 | 2.1713 | 1217490 | 0.0099 | 39 | 2.544E-4 | 30.419 | 27.377 |
| 2675 | 71.29 | 2.1810 | 1217524 | 0.0099 | 38 | 2.635E-4 | 30.667 | 27.600 |
| 2675 | 72.13 | 2.1904 | 1217560 | 0.0097 | 35 | 2.727E-4 | 30.927 | 27.834 |
| 2675 | 73.04 | 2.2004 | 1217598 | 0.0099 | 34 | 2.836E-4 | 31.182 | 28.063 |
| 2675 | 73.95 | 2.2102 | 1217633 | 0.0098 | 34 | 2.919E-4 | 31.447 | 28.301 |
| 2675 | 74.85 | 2.2198 | 1217663 | 0.0099 | 33 | 3.009E-4 | 31.728 | 28.554 |
| 2675 | 75.87 | 2.2304 | 1217696 | 0.0099 | 32 | 3.121E-4 | 31.995 | 28.795 |
| 2675 | 76.81 | 2.2401 | 1217728 | 0.0100 | 31 | 3.223E-4 | 32.285 | 29.056 |
| 2675 | 77.79 | 2.2499 | 1217759 | 0.0100 | 30 | 3.334E-4 | 32.569 | 29.311 |
| 2675 | 78.81 | 2.2601 | 1217789 | 0.0099 | 28 | 3.537E-4 | 32.860 | 29.573 |
| 2675 | 79.85 | 2.2702 | 1217817 | 0.0099 | 27 | 3.780E-4 | 33.150 | 29.834 |
| 2675 | 80.84 | 2.2797 | 1217841 | 0.0099 | 25 | 4.005E-4 | 33.450 | 30.103 |
| 2675 | 81.89 | 2.2895 | 1217864 | 0.0099 | 23 | 4.287E-4 | 33.746 | 30.369 |
| 2675 | 82.97 | 2.2995 | 1217887 | 0.0098 | 21 | 4.615E-4 | 34.053 | 30.646 |
| 2675 | 84.08 | 2.3095 | 1217909 | 0.0100 | 20 | 5.041E-4 | 34.369 | 30.930 |
| 2675 | 85.22 | 2.3197 | 1217928 | 0.0100 | 19 | 5.473E-4 | 34.681 | 31.210 |
| 2675 | 86.32 | 2.3293 | 1217945 | 0.0099 | 17 | 5.970E-4 | 35.014 | 31.510 |
| 2675 | 87.53 | 2.3396 | 1217961 | 0.0099 | 16 | 6.399E-4 | 35.330 | 31.794 |
| 2675 | 88.68 | 2.3493 | 1217976 | 0.0099 | 15 | 6.795E-4 | 35.666 | 32.095 |
| 2675 | 89.85 | 2.3590 | 1217989 | 0.0099 | 14 | 7.162E-4 | 36.000 | 32.396 |
| 2675 | 91.08 | 2.3689 | 1218003 | 0.0098 | 13 | 7.557E-4 | 36.340 | 32.701 |
| 2675 | 92.34 | 2.3790 | 1218016 | 0.0099 | 12 | 8.065E-4 | 36.689 | 33.015 |
| 2674 | 93.62 | 2.3889 | 1218028 | 0.0100 | 12 | 8.658E-4 | 37.038 | 33.329 |
| 2674 | 94.87 | 2.3985 | 1218039 | 0.0103 | 11 | 9.432E-4 | 37.397 | 33.651 |
| 2674 | 96.19 | 2.4084 | 1218049 | 0.0100 | 10 | 1.002E-3 | 37.767 | 33.983 |
| 2674 | 97.63 | 2.4190 | 1218059 | 0.0101 | 10 | 1.071E-3 | 38.148 | 34.315 |
| 2670 | 99.24 | 2.4308 | 1218069 | 0.0103 | 9 | 1.148E-3 | 38.531 | 34.669 |
| 2673 | 100.38 | 2.4391 | 1218077 | 0.0105 | 9 | 1.207E-3 | 38.941 | 35.025 |
| 2674 | 101.83 | 2.4495 | 1218085 | 0.0105 | 8 | 1.277E-3 | 39.343 | 35.400 * |
| 2674 | 103.39 | 2.4604 | 1218093 | 0.0101 | 8 | 1.361E-3 | 39.768 | 35.778 * |
| 2673 | 104.97 | 2.4712 | 1218101 | 0.0105 | 7 | 1.472E-3 | 40.208 | 36.173 * |
| 2673 | 106.55 | 2.4818 | 1218108 | 0.0106 | 7 | 1.603E-3 | 40.631 | 36.551 * |
| 2673 | 108.05 | 2.4916 | 1218114 | 0.0105 | 6 | 1.738E-3 | 41.080 | 36.953 * |
| 2672 | 109.72 | 2.5023 | 1218120 | 0.0103 | 6 | 1.914E-3 | 41.508 | 37.330 * |
| 2671 | 111.39 | 2.5128 | 1218125 | 0.0103 | 5 | 2.091E-3 | 41.964 | 37.735 * |
| 2670 | 113.08 | 2.5232 | 1218130 | 0.0105 | 5 | 2.306E-3 | 42.416 | 38.138 * |
| 2672 | 114.68 | 2.5328 | 1218134 | 0.0104 | 4 | 2.425E-3 | 42.870 | 38.534 * |
| 2669 | 116.48 | 2.5434 | 1218138 | 0.0104 | 4 | 2.606E-3 | 43.374 | 38.990 * |
| 2669 | 118.47 | 2.5549 | 1218142 | 0.0103 | 4 | 2.799E-3 | 43.833 | 39.393 * |
| 2669 | 120.18 | 2.5645 | 1218146 | 0.0106 | 4 | 2.924E-3 | 44.352 | 39.854 * |
| 2667 | 122.12 | 2.5751 | 1218149 | 0.0108 | 4 | 3.068E-3 | 44.816 | 40.259 * |
| 2666 | 123.93 | 2.5849 | 1218152 | 0.0105 | 3 | 3.292E-3 | 45.352 | 40.729 * |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^0.5) | deltaK |
|--------------|--------|-----------|---------|------------|----|-------------------|-----------------------|----------|
| 2664 | 126.17 | 2.5966 | 1218156 | 0.0107 | 3 | 3.774E-3 | 45.830 | 41.135 * |
| 2657 | 128.45 | 2.6083 | 1218159 | 0.0107 | 3 | 4.345E-3 | 46.308 | 41.535 * |
| 2650 | 130.35 | 2.6178 | 1218161 | 0.0105 | 3 | 4.563E-3 | 46.804 | 41.944 * |
| 2645 | 132.55 | 2.6285 | 1218163 | 0.0218 | 4 | 5.453E-3 | 47.099 | 42.139 * |
| 2623 | 134.88 | 2.6396 | 1218165 | 0.0193 | 4 | 4.835E-3 | 47.459 | 42.385 * |
| | 136.66 | 2.6479 | 1218167 | | | | | |

Automated Fatigue Crack
Growth Rate Analysis

| | | | |
|-----------------|--------------|---------------|------|
| Test ID | 5383-FCG-2 | Geometry | C(T) |
| Contract | SSC 10624-01 | Orientation | T-L |
| Material | 5383-H116 | Yield (ksi) | 35.4 |
| Temperature (F) | 75 | Modulus (Msi) | 10.5 |
| Environment | RH = 40% | | |

Specimen Dimensions (in)

| | | | |
|---------------|-------|-------------|-------|
| Thickness | 0.487 | Height | 2.400 |
| Net Thickness | 0.487 | Notch Depth | 1.000 |
| Width | 4.001 | Gage Length | 0.500 |

Precrack Parameters

| | | | |
|--------------|-------|--------------------|------|
| Pmax (lbs) | 861.0 | Stress Ratio | 0.10 |
| Final a (in) | 1.050 | Kmax (ksi sqr[in]) | 4.50 |

Test Parameters

| EvBP | Freq | Pmax | R | Ai | Kmaxi | C | DKi |
|--------|-------|------|------|-------|-------|------|------|
| 24.663 | 10.00 | 0 | 0.10 | 1.180 | 3.00 | 4.00 | 0.00 |
| 32.708 | 10.00 | 0 | 0.10 | 1.495 | 10.56 | 2.00 | 0.00 |
| 50.476 | 5.00 | 2590 | 0.10 | 0.000 | 0.00 | 0.00 | 0.00 |

| K Coeff | C Coeff |
|---------|----------|
| .886 | 1.00098 |
| 4.64 | -4.66951 |
| -13.32 | 18.4601 |
| 14.72 | -236.825 |
| -5.6 | 1214.88 |
| . | -2143.57 |

Visual Observations

| EvB/P | Crack(EvB/P) | Crack(visual) | Error | CAF |
|---------|--------------|---------------|--------|-------|
| 20.552 | 0.994 | 1.000 | 0.006 | 1.013 |
| 21.843 | 1.061 | 1.060 | -0.001 | 1.009 |
| 23.970 | 1.160 | 1.160 | 0.000 | 1.003 |
| 24.563 | 1.186 | 1.185 | -0.001 | 1.001 |
| 27.161 | 1.290 | 1.285 | -0.005 | 0.995 |
| 28.537 | 1.341 | 1.340 | -0.001 | 0.992 |
| 32.684 | 1.478 | 1.475 | -0.003 | 0.985 |
| 50.171 | 1.884 | 1.890 | 0.006 | 0.963 |
| 102.347 | 2.451 | 2.450 | -0.001 | 0.933 |

Comments

Date of test: 8/30/2006
Waveform Type Sine

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^0.5) | deltaK |
|--------------|-------|-----------|--------|------------|--------|-------------------|-----------------------|--------|
| | 24.66 | 1.1898 | 17589 | | | | | |
| 547 | 24.73 | 1.1925 | 51634 | 0.0076 | 91844 | 8.322E-8 | 3.157 | 2.841 |
| 557 | 24.84 | 1.1974 | 109433 | 0.0096 | 109507 | 8.759E-8 | 3.206 | 2.886 |
| 566 | 24.95 | 1.2021 | 161141 | 0.0044 | 48565 | 9.160E-8 | 3.271 | 2.944 |
| 576 | 25.06 | 1.2067 | 211789 | 0.0048 | 50194 | 9.510E-8 | 3.339 | 3.005 |
| 586 | 25.18 | 1.2117 | 263538 | 0.0048 | 47751 | 1.003E-7 | 3.404 | 3.063 |
| 596 | 25.29 | 1.2164 | 308981 | 0.0048 | 45798 | 1.052E-7 | 3.476 | 3.128 |
| 606 | 25.42 | 1.2213 | 352797 | 0.0048 | 43416 | 1.108E-7 | 3.545 | 3.190 |
| 617 | 25.53 | 1.2262 | 395940 | 0.0048 | 40850 | 1.166E-7 | 3.617 | 3.256 |
| 627 | 25.65 | 1.2309 | 435931 | 0.0048 | 39335 | 1.219E-7 | 3.690 | 3.321 |
| 637 | 25.76 | 1.2355 | 472285 | 0.0048 | 37587 | 1.270E-7 | 3.764 | 3.387 |
| 648 | 25.88 | 1.2403 | 508639 | 0.0047 | 35445 | 1.330E-7 | 3.840 | 3.456 |
| 660 | 26.00 | 1.2452 | 544992 | 0.0047 | 34082 | 1.389E-7 | 3.917 | 3.526 |
| 671 | 26.12 | 1.2500 | 578316 | 0.0048 | 33072 | 1.439E-7 | 3.996 | 3.596 |
| 682 | 26.24 | 1.2545 | 608611 | 0.0047 | 31507 | 1.500E-7 | 4.077 | 3.669 |
| 694 | 26.36 | 1.2593 | 640421 | 0.0047 | 29690 | 1.571E-7 | 4.157 | 3.742 |
| 705 | 26.48 | 1.2641 | 670715 | 0.0047 | 28175 | 1.658E-7 | 4.242 | 3.818 |
| 718 | 26.60 | 1.2688 | 697679 | 0.0047 | 26964 | 1.755E-7 | 4.325 | 3.892 |
| 729 | 26.71 | 1.2733 | 723129 | 0.0047 | 25096 | 1.871E-7 | 4.413 | 3.971 |
| 742 | 26.84 | 1.2780 | 747366 | 0.0047 | 23278 | 2.016E-7 | 4.498 | 4.049 |
| 754 | 26.96 | 1.2828 | 770392 | 0.0047 | 21693 | 2.186E-7 | 4.588 | 4.129 |
| 767 | 27.08 | 1.2873 | 790994 | 0.0047 | 20036 | 2.379E-7 | 4.681 | 4.213 |
| 780 | 27.21 | 1.2922 | 810385 | 0.0047 | 18323 | 2.628E-7 | 4.773 | 4.296 |
| 793 | 27.33 | 1.2969 | 827836 | 0.0047 | 16450 | 2.940E-7 | 4.869 | 4.382 |
| 806 | 27.45 | 1.3015 | 843346 | 0.0047 | 14774 | 3.330E-7 | 4.967 | 4.470 |
| 820 | 27.58 | 1.3063 | 857303 | 0.0047 | 13032 | 3.804E-7 | 5.065 | 4.558 |
| 834 | 27.71 | 1.3109 | 869090 | 0.0047 | 11381 | 4.382E-7 | 5.169 | 4.652 |
| 848 | 27.84 | 1.3158 | 879639 | 0.0048 | 9922 | 5.106E-7 | 5.270 | 4.743 |
| 862 | 27.96 | 1.3203 | 888575 | 0.0048 | 8548 | 5.974E-7 | 5.377 | 4.839 |
| 877 | 28.09 | 1.3250 | 896122 | 0.0047 | 7346 | 6.988E-7 | 5.485 | 4.936 |
| 892 | 28.22 | 1.3300 | 902875 | 0.0047 | 6266 | 8.158E-7 | 5.596 | 5.036 |
| 908 | 28.36 | 1.3349 | 908591 | 0.0047 | 5420 | 9.424E-7 | 5.709 | 5.138 |
| 923 | 28.49 | 1.3394 | 913164 | 0.0047 | 4738 | 1.056E-6 | 5.823 | 5.240 |
| 938 | 28.61 | 1.3439 | 917232 | 0.0047 | 4127 | 1.180E-6 | 5.939 | 5.345 |
| 954 | 28.75 | 1.3488 | 921094 | 0.0047 | 3614 | 1.335E-6 | 6.055 | 5.449 |
| 970 | 28.88 | 1.3534 | 924549 | 0.0047 | 3238 | 1.507E-6 | 6.178 | 5.560 |
| 986 | 29.01 | 1.3582 | 927639 | 0.0047 | 2924 | 1.684E-6 | 6.303 | 5.673 |
| 1004 | 29.15 | 1.3630 | 930273 | 0.0047 | 2610 | 1.870E-6 | 6.428 | 5.785 |
| 1021 | 29.28 | 1.3676 | 932589 | 0.0047 | 2344 | 2.063E-6 | 6.556 | 5.901 |
| 1037 | 29.41 | 1.3721 | 934777 | 0.0047 | 2092 | 2.285E-6 | 6.686 | 6.017 |
| 1055 | 29.55 | 1.3769 | 936756 | 0.0047 | 1888 | 2.537E-6 | 6.818 | 6.137 |
| 1073 | 29.69 | 1.3817 | 938610 | 0.0047 | 1725 | 2.824E-6 | 6.954 | 6.259 |
| 1091 | 29.83 | 1.3864 | 940193 | 0.0047 | 1559 | 3.131E-6 | 7.095 | 6.386 |
| 1109 | 29.97 | 1.3911 | 941598 | 0.0048 | 1425 | 3.423E-6 | 7.236 | 6.513 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in]^0.5) |
|--------------|-------|-----------|--------|------------|------|-------------------|--------|-------------------------|
| 1128 | 30.11 | 1.3958 | 942940 | 0.0048 | 1294 | 3.733E-6 | 7.382 | 6.644 |
| 1147 | 30.25 | 1.4005 | 944130 | 0.0047 | 1181 | 4.028E-6 | 7.531 | 6.778 |
| 1167 | 30.39 | 1.4054 | 945304 | 0.0047 | 1096 | 4.351E-6 | 7.684 | 6.916 |
| 1187 | 30.54 | 1.4102 | 946371 | 0.0047 | 1022 | 4.684E-6 | 7.835 | 7.052 |
| 1206 | 30.67 | 1.4146 | 947278 | 0.0047 | 952 | 5.018E-6 | 7.992 | 7.193 |
| 1226 | 30.81 | 1.4193 | 948174 | 0.0047 | 876 | 5.384E-6 | 8.151 | 7.336 |
| 1248 | 30.97 | 1.4243 | 949070 | 0.0047 | 819 | 5.743E-6 | 8.312 | 7.481 |
| 1269 | 31.11 | 1.4290 | 949839 | 0.0047 | 783 | 6.082E-6 | 8.480 | 7.632 |
| 1290 | 31.25 | 1.4335 | 950560 | 0.0048 | 738 | 6.460E-6 | 8.647 | 7.782 |
| 1311 | 31.40 | 1.4382 | 951286 | 0.0047 | 685 | 6.868E-6 | 8.822 | 7.939 |
| 1334 | 31.55 | 1.4431 | 951977 | 0.0047 | 657 | 7.254E-6 | 8.996 | 8.097 |
| 1357 | 31.70 | 1.4479 | 952599 | 0.0048 | 628 | 7.663E-6 | 9.179 | 8.261 |
| 1380 | 31.85 | 1.4525 | 953177 | 0.0048 | 592 | 8.056E-6 | 9.366 | 8.429 |
| 1404 | 32.01 | 1.4574 | 953781 | 0.0047 | 564 | 8.404E-6 | 9.554 | 8.599 |
| 1428 | 32.16 | 1.4622 | 954330 | 0.0047 | 541 | 8.720E-6 | 9.747 | 8.773 |
| 1452 | 32.31 | 1.4668 | 954839 | 0.0093 | 1033 | 9.000E-6 | 9.944 | 8.950 |
| 1476 | 32.46 | 1.4715 | 955363 | 0.0094 | 1005 | 9.345E-6 | 10.139 | 9.125 |
| | 32.61 | 1.4762 | 955844 | | | | | |
| | 32.71 | 1.4791 | 956507 | | | | | |
| 1533 | 33.00 | 1.4880 | 957438 | 0.0189 | 1874 | 1.007E-5 | 10.658 | 9.591 |
| 1555 | 33.34 | 1.4979 | 958381 | 0.0193 | 1842 | 1.050E-5 | 10.859 | 9.773 |
| 1576 | 33.65 | 1.5073 | 959280 | 0.0190 | 1728 | 1.098E-5 | 11.078 | 9.970 |
| 1597 | 33.98 | 1.5169 | 960109 | 0.0095 | 831 | 1.144E-5 | 11.294 | 10.165 |
| 1618 | 34.30 | 1.5262 | 960904 | 0.0094 | 789 | 1.193E-5 | 11.519 | 10.367 |
| 1640 | 34.63 | 1.5357 | 961699 | 0.0095 | 754 | 1.256E-5 | 11.745 | 10.571 |
| 1662 | 34.97 | 1.5453 | 962424 | 0.0096 | 726 | 1.318E-5 | 11.974 | 10.776 |
| 1684 | 35.30 | 1.5544 | 963115 | 0.0096 | 691 | 1.385E-5 | 12.217 | 10.995 |
| 1708 | 35.66 | 1.5644 | 963806 | 0.0096 | 654 | 1.461E-5 | 12.460 | 11.214 |
| 1732 | 36.03 | 1.5743 | 964463 | 0.0096 | 625 | 1.537E-5 | 12.710 | 11.439 |
| 1754 | 36.37 | 1.5835 | 965048 | 0.0095 | 595 | 1.607E-5 | 12.969 | 11.672 |
| 1778 | 36.73 | 1.5931 | 965624 | 0.0095 | 567 | 1.677E-5 | 13.222 | 11.900 |
| 1802 | 37.09 | 1.6027 | 966173 | 0.0094 | 537 | 1.754E-5 | 13.481 | 12.133 |
| 1826 | 37.44 | 1.6117 | 966682 | 0.0095 | 516 | 1.825E-5 | 13.751 | 12.376 |
| 1851 | 37.82 | 1.6214 | 967207 | 0.0095 | 497 | 1.905E-5 | 14.018 | 12.617 |
| 1875 | 38.20 | 1.6310 | 967687 | 0.0095 | 478 | 1.988E-5 | 14.296 | 12.866 |
| 1900 | 38.57 | 1.6402 | 968146 | 0.0096 | 463 | 2.078E-5 | 14.581 | 13.123 |
| 1925 | 38.96 | 1.6499 | 968605 | 0.0096 | 438 | 2.178E-5 | 14.870 | 13.383 |
| 1952 | 39.36 | 1.6597 | 969042 | 0.0095 | 417 | 2.280E-5 | 15.170 | 13.653 |
| 1978 | 39.76 | 1.6695 | 969457 | 0.0096 | 400 | 2.403E-5 | 15.470 | 13.924 |
| 2004 | 40.15 | 1.6787 | 969832 | 0.0096 | 379 | 2.534E-5 | 15.774 | 14.197 |
| 2029 | 40.54 | 1.6879 | 970187 | 0.0095 | 357 | 2.671E-5 | 16.088 | 14.479 |
| 2057 | 40.97 | 1.6978 | 970543 | 0.0095 | 335 | 2.830E-5 | 16.405 | 14.764 |
| 2085 | 41.40 | 1.7076 | 970881 | 0.0095 | 320 | 2.997E-5 | 16.732 | 15.059 |
| 2112 | 41.81 | 1.7169 | 971183 | 0.0097 | 306 | 3.169E-5 | 17.065 | 15.358 |
| 2139 | 42.23 | 1.7263 | 971468 | 0.0096 | 287 | 3.355E-5 | 17.402 | 15.662 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in]^1.5) |
|--------------|-------|-----------|--------|------------|-----|-------------------|--------|-------------------------|
| 2168 | 42.67 | 1.7360 | 971752 | 0.0095 | 266 | 3.578E-5 | 17.750 | 15.975 |
| 2197 | 43.12 | 1.7460 | 972023 | 0.0095 | 253 | 3.804E-5 | 18.103 | 16.293 |
| 2226 | 43.56 | 1.7554 | 972263 | 0.0096 | 240 | 4.038E-5 | 18.461 | 16.615 |
| 2254 | 44.00 | 1.7646 | 972478 | 0.0096 | 223 | 4.303E-5 | 18.827 | 16.945 |
| 2284 | 44.45 | 1.7741 | 972698 | 0.0095 | 209 | 4.587E-5 | 19.195 | 17.276 |
| 2314 | 44.93 | 1.7840 | 972908 | 0.0096 | 198 | 4.865E-5 | 19.577 | 17.619 |
| 2344 | 45.40 | 1.7936 | 973091 | 0.0096 | 188 | 5.133E-5 | 19.969 | 17.972 |
| 2374 | 45.87 | 1.8032 | 973274 | 0.0097 | 177 | 5.468E-5 | 20.363 | 18.327 |
| 2405 | 46.35 | 1.8128 | 973448 | 0.0097 | 166 | 5.845E-5 | 20.763 | 18.687 |
| 2435 | 46.84 | 1.8222 | 973606 | 0.0097 | 156 | 6.243E-5 | 21.178 | 19.060 |
| 2467 | 47.35 | 1.8321 | 973758 | 0.0096 | 144 | 6.763E-5 | 21.608 | 19.447 |
| 2501 | 47.88 | 1.8423 | 973903 | 0.0096 | 133 | 7.383E-5 | 22.033 | 19.830 |
| 2532 | 48.37 | 1.8516 | 974027 | 0.0096 | 123 | 8.026E-5 | 22.478 | 20.230 |
| 2563 | 48.88 | 1.8609 | 974138 | 0.0190 | 217 | 8.759E-5 | 22.915 | 20.624 |
| 2596 | 49.40 | 1.8706 | 974244 | 0.0192 | 203 | 9.459E-5 | 23.359 | 21.024 |
| | 49.93 | 1.8801 | 974341 | | | | | |
| | 50.48 | 1.8898 | 974442 | | | | | |
| 2590 | 51.01 | 1.8991 | 974544 | 0.0191 | 212 | 9.010E-5 | 23.791 | 21.398 |
| 2590 | 51.57 | 1.9089 | 974654 | 0.0195 | 220 | 8.844E-5 | 23.969 | 21.572 |
| 2590 | 52.14 | 1.9186 | 974764 | 0.0193 | 211 | 9.164E-5 | 24.141 | 21.727 |
| 2590 | 52.71 | 1.9282 | 974865 | 0.0097 | 102 | 9.536E-5 | 24.315 | 21.884 |
| 2590 | 53.30 | 1.9380 | 974963 | 0.0097 | 100 | 9.786E-5 | 24.490 | 22.041 |
| 2590 | 53.88 | 1.9476 | 975056 | 0.0096 | 96 | 1.005E-4 | 24.668 | 22.201 |
| 2590 | 54.48 | 1.9572 | 975154 | 0.0096 | 93 | 1.028E-4 | 24.850 | 22.365 |
| 2590 | 55.11 | 1.9672 | 975252 | 0.0097 | 92 | 1.052E-4 | 25.028 | 22.525 |
| 2590 | 55.70 | 1.9765 | 975337 | 0.0097 | 90 | 1.073E-4 | 25.214 | 22.692 |
| 2590 | 56.32 | 1.9860 | 975422 | 0.0097 | 87 | 1.103E-4 | 25.399 | 22.859 |
| 2590 | 56.97 | 1.9959 | 975512 | 0.0096 | 84 | 1.138E-4 | 25.586 | 23.027 |
| 2590 | 57.62 | 2.0056 | 975597 | 0.0097 | 82 | 1.171E-4 | 25.778 | 23.200 |
| 2590 | 58.26 | 2.0152 | 975678 | 0.0097 | 80 | 1.215E-4 | 25.973 | 23.376 |
| 2590 | 58.94 | 2.0250 | 975756 | 0.0097 | 77 | 1.263E-4 | 26.167 | 23.550 |
| 2590 | 59.60 | 2.0345 | 975829 | 0.0097 | 75 | 1.301E-4 | 26.369 | 23.732 |
| 2590 | 60.31 | 2.0444 | 975902 | 0.0097 | 73 | 1.334E-4 | 26.570 | 23.913 |
| 2590 | 61.01 | 2.0543 | 975975 | 0.0097 | 71 | 1.362E-4 | 26.774 | 24.097 |
| 2590 | 61.71 | 2.0637 | 976045 | 0.0097 | 70 | 1.385E-4 | 26.985 | 24.286 |
| 2590 | 62.44 | 2.0736 | 976116 | 0.0097 | 68 | 1.422E-4 | 27.191 | 24.472 |
| 2590 | 63.17 | 2.0833 | 976182 | 0.0096 | 65 | 1.472E-4 | 27.403 | 24.663 |
| 2590 | 63.90 | 2.0928 | 976247 | 0.0097 | 63 | 1.533E-4 | 27.617 | 24.855 |
| 2590 | 64.64 | 2.1024 | 976307 | 0.0097 | 60 | 1.602E-4 | 27.832 | 25.048 |
| 2590 | 65.40 | 2.1120 | 976366 | 0.0096 | 58 | 1.667E-4 | 28.052 | 25.247 |
| 2590 | 66.19 | 2.1218 | 976423 | 0.0098 | 57 | 1.730E-4 | 28.278 | 25.450 |
| 2590 | 67.00 | 2.1318 | 976478 | 0.0098 | 56 | 1.770E-4 | 28.502 | 25.652 |
| 2590 | 67.78 | 2.1411 | 976530 | 0.0098 | 54 | 1.816E-4 | 28.742 | 25.867 |
| 2590 | 68.64 | 2.1514 | 976586 | 0.0098 | 52 | 1.878E-4 | 28.972 | 26.074 |
| 2590 | 69.48 | 2.1611 | 976640 | 0.0097 | 49 | 1.965E-4 | 29.214 | 26.292 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^0.5) | deltaK |
|--------------|--------|-----------|--------|------------|----|-------------------|-----------------------|----------|
| 2590 | 70.32 | 2.1708 | 976687 | 0.0099 | 48 | 2.064E-4 | 29.454 | 26.508 |
| 2590 | 71.18 | 2.1805 | 976732 | 0.0098 | 46 | 2.150E-4 | 29.696 | 26.726 |
| 2590 | 72.04 | 2.1901 | 976774 | 0.0098 | 43 | 2.247E-4 | 29.950 | 26.954 |
| 2590 | 72.98 | 2.2003 | 976818 | 0.0098 | 41 | 2.348E-4 | 30.199 | 27.178 |
| 2590 | 73.89 | 2.2101 | 976862 | 0.0099 | 39 | 2.493E-4 | 30.460 | 27.413 |
| 2590 | 74.81 | 2.2198 | 976900 | 0.0098 | 38 | 2.652E-4 | 30.717 | 27.644 |
| 2590 | 75.74 | 2.2294 | 976934 | 0.0098 | 36 | 2.798E-4 | 30.985 | 27.885 |
| 2590 | 76.74 | 2.2396 | 976968 | 0.0098 | 33 | 2.984E-4 | 31.246 | 28.121 |
| 2590 | 77.69 | 2.2491 | 976999 | 0.0098 | 31 | 3.131E-4 | 31.524 | 28.370 |
| 2590 | 78.69 | 2.2590 | 977031 | 0.0099 | 30 | 3.294E-4 | 31.796 | 28.615 |
| 2590 | 79.70 | 2.2687 | 977059 | 0.0098 | 28 | 3.474E-4 | 32.081 | 28.872 |
| 2590 | 80.76 | 2.2789 | 977088 | 0.0098 | 27 | 3.670E-4 | 32.362 | 29.125 |
| 2590 | 81.80 | 2.2885 | 977113 | 0.0098 | 25 | 3.883E-4 | 32.657 | 29.389 |
| 2590 | 82.87 | 2.2983 | 977137 | 0.0098 | 24 | 4.079E-4 | 32.945 | 29.649 |
| 2590 | 83.94 | 2.3080 | 977161 | 0.0098 | 23 | 4.337E-4 | 33.247 | 29.920 |
| 2590 | 85.08 | 2.3181 | 977183 | 0.0098 | 21 | 4.645E-4 | 33.544 | 30.188 |
| 2590 | 86.19 | 2.3277 | 977204 | 0.0098 | 20 | 5.063E-4 | 33.856 | 30.468 |
| 2590 | 87.35 | 2.3376 | 977223 | 0.0098 | 19 | 5.397E-4 | 34.167 | 30.747 |
| 2590 | 88.54 | 2.3475 | 977240 | 0.0099 | 18 | 5.690E-4 | 34.483 | 31.031 |
| 2590 | 89.71 | 2.3571 | 977255 | 0.0099 | 16 | 6.036E-4 | 34.804 | 31.320 |
| 2590 | 90.91 | 2.3669 | 977272 | 0.0099 | 15 | 6.435E-4 | 35.144 | 31.626 |
| 2590 | 92.27 | 2.3776 | 977289 | 0.0098 | 15 | 6.834E-4 | 35.471 | 31.920 |
| 2589 | 93.52 | 2.3873 | 977302 | 0.0098 | 14 | 7.174E-4 | 35.821 | 32.234 |
| 2590 | 94.77 | 2.3968 | 977314 | 0.0099 | 13 | 7.645E-4 | 36.158 | 32.537 |
| 2589 | 96.07 | 2.4065 | 977327 | 0.0098 | 12 | 8.148E-4 | 36.502 | 32.846 |
| 2589 | 97.40 | 2.4162 | 977339 | 0.0099 | 11 | 8.709E-4 | 36.859 | 33.167 |
| 2589 | 98.81 | 2.4264 | 977350 | 0.0102 | 11 | 9.246E-4 | 37.224 | 33.495 |
| 2589 | 100.27 | 2.4366 | 977361 | 0.0102 | 11 | 9.824E-4 | 37.605 | 33.835 |
| 2589 | 101.75 | 2.4468 | 977370 | 0.0103 | 10 | 1.055E-3 | 37.990 | 34.173 |
| 2586 | 103.37 | 2.4580 | 977381 | 0.0104 | 9 | 1.165E-3 | 38.390 | 34.539 |
| 2588 | 104.77 | 2.4676 | 977390 | 0.0104 | 8 | 1.270E-3 | 38.803 | 34.900 |
| 2589 | 106.33 | 2.4782 | 977397 | 0.0104 | 8 | 1.373E-3 | 39.217 | 35.280 * |
| 2588 | 107.91 | 2.4886 | 977404 | 0.0102 | 7 | 1.486E-3 | 39.643 | 35.660 * |
| 2588 | 109.50 | 2.4988 | 977411 | 0.0105 | 7 | 1.603E-3 | 40.072 | 36.047 * |
| 2588 | 111.11 | 2.5090 | 977417 | 0.0104 | 6 | 1.689E-3 | 40.502 | 36.432 * |
| 2588 | 112.79 | 2.5193 | 977423 | 0.0103 | 6 | 1.841E-3 | 40.947 | 36.826 * |
| 2585 | 114.63 | 2.5305 | 977429 | 0.0104 | 5 | 1.985E-3 | 41.406 | 37.238 * |
| 2587 | 116.34 | 2.5405 | 977434 | 0.0105 | 5 | 2.134E-3 | 41.861 | 37.640 * |
| 2586 | 118.09 | 2.5507 | 977438 | 0.0106 | 5 | 2.282E-3 | 42.341 | 38.066 * |
| 2586 | 119.99 | 2.5614 | 977443 | 0.0108 | 4 | 2.502E-3 | 42.792 | 38.462 * |
| 2583 | 121.88 | 2.5718 | 977447 | 0.0106 | 4 | 2.769E-3 | 43.300 | 38.910 * |
| 2582 | 123.96 | 2.5831 | 977451 | 0.0106 | 4 | 3.039E-3 | 43.828 | 39.368 * |
| 2582 | 126.31 | 2.5954 | 977455 | 0.0105 | 3 | 3.519E-3 | 44.288 | 39.768 * |
| 2579 | 128.01 | 2.6041 | 977457 | 0.0106 | 3 | 3.624E-3 | 44.856 | 40.271 * |
| 2579 | 130.01 | 2.6142 | 977460 | 0.0104 | 3 | 3.956E-3 | 45.286 | 40.634 * |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^0.5) | deltaK |
|--------------|--------|-----------|--------|------------|----|-------------------|-----------------------|----------|
| 2575 | 132.12 | 2.6245 | 977462 | 0.0103 | 2 | 4.271E-3 | 45.780 | 41.058 * |
| 2569 | 134.40 | 2.6355 | 977465 | 0.0209 | 5 | 4.171E-3 | 46.247 | 41.448 * |
| 2564 | 136.52 | 2.6454 | 977467 | 0.0216 | 4 | 5.391E-3 | 46.664 | 41.766 * |
| | 139.07 | 2.6570 | 977469 | | | | | |

Automated Fatigue Crack
Growth Rate Analysis

| | | | |
|-----------------|--------------|---------------|------|
| Test ID | 5383-FCG-3 | Geometry | C(T) |
| Contract | SSC 10624-01 | Orientation | T-L |
| Material | 5383-H116 | Yield (ksi) | 35.4 |
| Temperature (F) | 75 | Modulus (Msi) | 10.5 |
| Environment | Sea Water | | |

Specimen Dimensions (in)

| | | | |
|---------------|-------|-------------|-------|
| Thickness | 0.487 | Height | 2.400 |
| Net Thickness | 0.487 | Notch Depth | 1.000 |
| Width | 4.000 | Gage Length | 0.500 |

Precrack Parameters

| | | | |
|--------------|-------|--------------------|------|
| Pmax (lbs) | 860.0 | Stress Ratio | 0.10 |
| Final a (in) | 1.050 | Kmax (ksi sqr[in]) | 4.50 |

Test Parameters

| EvBP | Freq | Pmax | R | Ai | Kmaxi | C | DKi |
|--------|------|------|------|-------|-------|------|------|
| 25.056 | 5.00 | 0 | 0.10 | 1.180 | 2.40 | 4.00 | 0.00 |
| 33.659 | 5.00 | 0 | 0.10 | 1.521 | 9.37 | 2.00 | 0.00 |
| 55.211 | 5.00 | 2400 | 0.10 | 0.000 | 0.00 | 0.00 | 0.00 |

| K Coeff | C Coeff |
|---------|----------|
| .886 | 1.00098 |
| 4.64 | -4.66951 |
| -13.32 | 18.4601 |
| 14.72 | -236.825 |
| -5.6 | 1214.88 |
| . | -2143.57 |

Visual Observations

| EvB/P | Crack(EvB/P) | Crack(visual) | Error | CAF |
|--------|--------------|---------------|--------|-------|
| 20.632 | 1.024 | 1.001 | -0.023 | 1.035 |
| 21.843 | 1.085 | 1.090 | 0.005 | 1.031 |
| 23.350 | 1.155 | 1.170 | 0.015 | 1.026 |
| 24.006 | 1.184 | 1.200 | 0.016 | 1.024 |
| 26.368 | 1.281 | 1.280 | -0.001 | 1.017 |
| 29.105 | 1.382 | 1.380 | -0.002 | 1.010 |
| 33.513 | 1.522 | 1.510 | -0.012 | 1.001 |
| 46.153 | 1.824 | 1.820 | -0.004 | 0.982 |
| 54.802 | 1.975 | 1.980 | 0.005 | 0.973 |

Comments

Date of test: 9/2/2006
Waveform Type Sine

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in]^0.5) |
|--------------|-------|-----------|--------|------------|-------|-------------------|-------|-------------------------|
| | 25.54 | 1.2484 | 214020 | | | | | |
| 503 | 25.67 | 1.2537 | 251086 | 0.0097 | 76616 | 1.261E-7 | 2.996 | 2.697 |
| 510 | 25.78 | 1.2581 | 290636 | 0.0098 | 70817 | 1.382E-7 | 3.065 | 2.759 |
| 520 | 25.91 | 1.2635 | 321903 | 0.0048 | 33533 | 1.402E-7 | 3.123 | 2.811 |
| 529 | 26.03 | 1.2679 | 353412 | 0.0046 | 31395 | 1.477E-7 | 3.183 | 2.865 |
| 536 | 26.12 | 1.2716 | 387345 | 0.0046 | 29166 | 1.568E-7 | 3.251 | 2.926 |
| 546 | 26.26 | 1.2773 | 415219 | 0.0046 | 27833 | 1.669E-7 | 3.308 | 2.977 |
| 555 | 26.37 | 1.2815 | 439457 | 0.0046 | 25975 | 1.828E-7 | 3.377 | 3.040 |
| 564 | 26.48 | 1.2858 | 465633 | 0.0047 | 23454 | 2.002E-7 | 3.446 | 3.102 |
| 574 | 26.61 | 1.2909 | 488901 | 0.0046 | 22039 | 2.121E-7 | 3.513 | 3.162 |
| 584 | 26.74 | 1.2958 | 509261 | 0.0046 | 20972 | 2.261E-7 | 3.584 | 3.226 |
| 594 | 26.85 | 1.3000 | 528067 | 0.0047 | 19452 | 2.413E-7 | 3.658 | 3.292 |
| 604 | 26.98 | 1.3048 | 547452 | 0.0047 | 18288 | 2.541E-7 | 3.728 | 3.355 |
| 614 | 27.10 | 1.3093 | 565287 | 0.0047 | 17479 | 2.672E-7 | 3.804 | 3.424 |
| 625 | 27.23 | 1.3142 | 582346 | 0.0047 | 16671 | 2.840E-7 | 3.880 | 3.492 |
| 635 | 27.35 | 1.3189 | 598629 | 0.0047 | 15405 | 3.048E-7 | 3.959 | 3.563 |
| 646 | 27.48 | 1.3237 | 614137 | 0.0047 | 14273 | 3.309E-7 | 4.039 | 3.635 |
| 657 | 27.61 | 1.3283 | 628095 | 0.0046 | 13168 | 3.615E-7 | 4.119 | 3.707 |
| 668 | 27.73 | 1.3328 | 639881 | 0.0046 | 12026 | 3.958E-7 | 4.201 | 3.781 |
| 679 | 27.86 | 1.3374 | 650926 | 0.0047 | 10914 | 4.344E-7 | 4.284 | 3.855 |
| 691 | 27.99 | 1.3421 | 661352 | 0.0046 | 9913 | 4.752E-7 | 4.370 | 3.933 |
| 703 | 28.12 | 1.3468 | 670784 | 0.0046 | 9127 | 5.158E-7 | 4.458 | 4.013 |
| 715 | 28.25 | 1.3516 | 679623 | 0.0046 | 8397 | 5.622E-7 | 4.547 | 4.092 |
| 727 | 28.38 | 1.3562 | 687570 | 0.0047 | 7665 | 6.158E-7 | 4.638 | 4.174 |
| 739 | 28.50 | 1.3606 | 694640 | 0.0046 | 6993 | 6.749E-7 | 4.729 | 4.256 |
| 751 | 28.63 | 1.3652 | 701309 | 0.0046 | 6367 | 7.465E-7 | 4.822 | 4.340 |
| 764 | 28.77 | 1.3700 | 707343 | 0.0047 | 5847 | 8.215E-7 | 4.918 | 4.426 |
| 777 | 28.90 | 1.3746 | 712742 | 0.0047 | 5457 | 8.767E-7 | 5.019 | 4.517 |
| 791 | 29.04 | 1.3795 | 717823 | 0.0047 | 5090 | 9.293E-7 | 5.121 | 4.609 |
| 805 | 29.18 | 1.3843 | 722653 | 0.0047 | 4728 | 9.881E-7 | 5.223 | 4.701 |
| 818 | 29.31 | 1.3887 | 727379 | 0.0047 | 4377 | 1.068E-6 | 5.330 | 4.797 |
| 831 | 29.45 | 1.3934 | 731851 | 0.0046 | 4013 | 1.184E-6 | 5.434 | 4.891 |
| 846 | 29.58 | 1.3982 | 735713 | 0.0046 | 3641 | 1.340E-6 | 5.544 | 4.989 |
| 860 | 29.72 | 1.4028 | 739005 | 0.0046 | 3240 | 1.512E-6 | 5.654 | 5.088 |
| 874 | 29.86 | 1.4074 | 741899 | 0.0046 | 2859 | 1.693E-6 | 5.766 | 5.190 |
| 889 | 30.00 | 1.4120 | 744501 | 0.0047 | 2545 | 1.889E-6 | 5.880 | 5.292 |
| 904 | 30.13 | 1.4166 | 746818 | 0.0047 | 2292 | 2.088E-6 | 5.997 | 5.398 |
| 919 | 30.28 | 1.4213 | 749005 | 0.0047 | 2073 | 2.306E-6 | 6.118 | 5.506 |
| 935 | 30.42 | 1.4262 | 750984 | 0.0047 | 1888 | 2.538E-6 | 6.241 | 5.617 |
| 951 | 30.57 | 1.4308 | 752755 | 0.0047 | 1736 | 2.773E-6 | 6.366 | 5.729 |
| 967 | 30.71 | 1.4354 | 754339 | 0.0047 | 1584 | 3.006E-6 | 6.495 | 5.846 |
| 984 | 30.85 | 1.4401 | 755826 | 0.0047 | 1444 | 3.269E-6 | 6.623 | 5.961 |
| 1000 | 31.00 | 1.4449 | 757235 | 0.0046 | 1318 | 3.562E-6 | 6.757 | 6.081 |
| 1017 | 31.14 | 1.4495 | 758509 | 0.0046 | 1219 | 3.867E-6 | 6.892 | 6.203 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in]^0.5) |
|--------------|-------|-----------|--------|------------|------|-------------------|--------|-------------------------|
| 1034 | 31.29 | 1.4541 | 759646 | 0.0047 | 1135 | 4.176E-6 | 7.025 | 6.322 |
| 1051 | 31.43 | 1.4585 | 760660 | 0.0046 | 1042 | 4.501E-6 | 7.166 | 6.449 |
| 1069 | 31.58 | 1.4632 | 761652 | 0.0046 | 963 | 4.843E-6 | 7.308 | 6.578 |
| 1088 | 31.73 | 1.4681 | 762634 | 0.0047 | 906 | 5.180E-6 | 7.454 | 6.708 |
| 1106 | 31.88 | 1.4727 | 763488 | 0.0047 | 858 | 5.498E-6 | 7.606 | 6.845 |
| 1124 | 32.03 | 1.4773 | 764286 | 0.0047 | 808 | 5.842E-6 | 7.757 | 6.981 |
| 1143 | 32.19 | 1.4820 | 765081 | 0.0047 | 753 | 6.234E-6 | 7.910 | 7.119 |
| 1162 | 32.34 | 1.4866 | 765807 | 0.0047 | 709 | 6.625E-6 | 8.070 | 7.263 |
| 1182 | 32.49 | 1.4914 | 766498 | 0.0047 | 672 | 7.056E-6 | 8.232 | 7.409 |
| 1203 | 32.65 | 1.4962 | 767154 | 0.0047 | 631 | 7.517E-6 | 8.396 | 7.557 |
| 1223 | 32.80 | 1.5008 | 767740 | 0.0047 | 591 | 7.954E-6 | 8.567 | 7.711 |
| 1244 | 32.96 | 1.5055 | 768316 | 0.0047 | 556 | 8.452E-6 | 8.738 | 7.864 |
| 1265 | 33.12 | 1.5103 | 768865 | 0.0092 | 1036 | 8.901E-6 | 8.911 | 8.020 |
| 1286 | 33.27 | 1.5147 | 769352 | 0.0093 | 968 | 9.579E-6 | 9.092 | 8.183 |
| | 33.44 | 1.5196 | 769833 | | | | | |
| | 33.66 | 1.5260 | 770407 | | | | | |
| 1333 | 33.77 | 1.5293 | 770712 | 0.0100 | 927 | 1.082E-5 | 9.544 | 8.590 |
| 1346 | 34.01 | 1.5360 | 771334 | 0.0160 | 1464 | 1.096E-5 | 9.670 | 8.703 |
| 1364 | 34.33 | 1.5453 | 772176 | 0.0187 | 1669 | 1.121E-5 | 9.835 | 8.851 |
| 1382 | 34.67 | 1.5547 | 773003 | 0.0090 | 748 | 1.204E-5 | 10.029 | 9.026 |
| 1401 | 35.01 | 1.5643 | 773771 | 0.0094 | 758 | 1.246E-5 | 10.228 | 9.205 |
| 1420 | 35.35 | 1.5738 | 774485 | 0.0094 | 728 | 1.298E-5 | 10.431 | 9.388 |
| 1439 | 35.70 | 1.5831 | 775198 | 0.0094 | 695 | 1.352E-5 | 10.638 | 9.574 |
| 1459 | 36.05 | 1.5925 | 775884 | 0.0094 | 668 | 1.401E-5 | 10.848 | 9.763 |
| 1478 | 36.40 | 1.6019 | 776543 | 0.0094 | 645 | 1.459E-5 | 11.063 | 9.956 |
| 1498 | 36.76 | 1.6114 | 777174 | 0.0094 | 617 | 1.524E-5 | 11.281 | 10.153 |
| 1518 | 37.12 | 1.6207 | 777777 | 0.0094 | 590 | 1.592E-5 | 11.507 | 10.356 |
| 1539 | 37.50 | 1.6303 | 778354 | 0.0094 | 565 | 1.662E-5 | 11.731 | 10.558 |
| 1559 | 37.86 | 1.6396 | 778902 | 0.0094 | 544 | 1.732E-5 | 11.964 | 10.767 |
| 1580 | 38.23 | 1.6489 | 779424 | 0.0094 | 523 | 1.801E-5 | 12.200 | 10.980 |
| 1601 | 38.62 | 1.6583 | 779933 | 0.0094 | 504 | 1.870E-5 | 12.442 | 11.197 |
| 1623 | 39.01 | 1.6679 | 780435 | 0.0094 | 485 | 1.942E-5 | 12.690 | 11.421 |
| 1645 | 39.40 | 1.6774 | 780916 | 0.0095 | 467 | 2.018E-5 | 12.945 | 11.650 |
| 1667 | 39.81 | 1.6869 | 781375 | 0.0094 | 448 | 2.097E-5 | 13.200 | 11.880 |
| 1689 | 40.20 | 1.6962 | 781812 | 0.0094 | 429 | 2.180E-5 | 13.461 | 12.115 |
| 1711 | 40.61 | 1.7056 | 782227 | 0.0094 | 411 | 2.272E-5 | 13.722 | 12.350 |
| 1733 | 41.00 | 1.7147 | 782619 | 0.0094 | 397 | 2.359E-5 | 13.991 | 12.592 |
| 1756 | 41.42 | 1.7241 | 783011 | 0.0094 | 384 | 2.456E-5 | 14.265 | 12.839 |
| 1779 | 41.84 | 1.7336 | 783384 | 0.0094 | 367 | 2.548E-5 | 14.548 | 13.093 |
| 1803 | 42.28 | 1.7432 | 783758 | 0.0094 | 354 | 2.659E-5 | 14.840 | 13.356 |
| 1827 | 42.72 | 1.7529 | 784113 | 0.0095 | 341 | 2.783E-5 | 15.131 | 13.618 |
| 1850 | 43.14 | 1.7619 | 784430 | 0.0095 | 329 | 2.905E-5 | 15.431 | 13.888 |
| 1874 | 43.59 | 1.7713 | 784743 | 0.0095 | 311 | 3.040E-5 | 15.737 | 14.163 |
| 1900 | 44.05 | 1.7811 | 785056 | 0.0094 | 296 | 3.184E-5 | 16.050 | 14.445 |
| 1925 | 44.53 | 1.7909 | 785355 | 0.0095 | 286 | 3.339E-5 | 16.369 | 14.732 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^0.5) | deltaK |
|--------------|-------|-----------|--------|------------|-----|-------------------|-----------------------|--------|
| 1949 | 44.98 | 1.8001 | 785625 | 0.0096 | 271 | 3.520E-5 | 16.696 | 15.027 |
| 1975 | 45.44 | 1.8094 | 785887 | 0.0094 | 254 | 3.698E-5 | 17.027 | 15.324 |
| 2001 | 45.93 | 1.8192 | 786144 | 0.0093 | 241 | 3.894E-5 | 17.363 | 15.626 |
| 2027 | 46.42 | 1.8287 | 786371 | 0.0095 | 233 | 4.077E-5 | 17.695 | 15.926 |
| 2051 | 46.86 | 1.8372 | 786581 | 0.0095 | 223 | 4.270E-5 | 18.048 | 16.243 |
| 2078 | 47.37 | 1.8469 | 786801 | 0.0095 | 210 | 4.482E-5 | 18.395 | 16.556 |
| 2105 | 47.89 | 1.8568 | 787020 | 0.0094 | 201 | 4.711E-5 | 18.769 | 16.892 |
| 2133 | 48.42 | 1.8667 | 787222 | 0.0096 | 194 | 4.980E-5 | 19.144 | 17.230 |
| 2160 | 48.94 | 1.8761 | 787404 | 0.0096 | 184 | 5.258E-5 | 19.526 | 17.573 |
| 2187 | 49.45 | 1.8854 | 787578 | 0.0096 | 172 | 5.576E-5 | 19.910 | 17.919 |
| 2215 | 49.99 | 1.8950 | 787744 | 0.0095 | 161 | 5.917E-5 | 20.304 | 18.273 |
| 2243 | 50.54 | 1.9047 | 787904 | 0.0095 | 152 | 6.315E-5 | 20.705 | 18.634 |
| 2271 | 51.09 | 1.9141 | 788049 | 0.0095 | 142 | 6.734E-5 | 21.117 | 19.005 |
| 2300 | 51.64 | 1.9236 | 788185 | 0.0095 | 133 | 7.198E-5 | 21.533 | 19.380 |
| 2329 | 52.21 | 1.9332 | 788313 | 0.0095 | 123 | 7.751E-5 | 21.948 | 19.754 |
| 2357 | 52.76 | 1.9423 | 788429 | 0.0095 | 114 | 8.377E-5 | 22.383 | 20.145 |
| 2386 | 53.34 | 1.9518 | 788540 | 0.0191 | 212 | 9.007E-5 | 22.815 | 20.533 |
| 2416 | 53.94 | 1.9614 | 788641 | 0.0190 | 192 | 9.914E-5 | 23.265 | 20.938 |
| | 54.53 | 1.9709 | 788732 | | | | | |
| | 55.21 | 1.9819 | 788832 | | | | | |
| 2400 | 55.75 | 1.9907 | 788930 | 0.0187 | 207 | 9.056E-5 | 23.642 | 21.276 |
| 2400 | 56.37 | 2.0007 | 789039 | 0.0204 | 219 | 9.324E-5 | 23.817 | 21.435 |
| 2400 | 57.03 | 2.0111 | 789149 | 0.0205 | 212 | 9.650E-5 | 24.002 | 21.601 |
| 2400 | 57.67 | 2.0211 | 789251 | 0.0102 | 103 | 9.869E-5 | 24.196 | 21.776 |
| 2400 | 58.34 | 2.0315 | 789353 | 0.0102 | 100 | 1.016E-4 | 24.388 | 21.949 |
| 2400 | 59.02 | 2.0418 | 789454 | 0.0101 | 97 | 1.042E-4 | 24.584 | 22.126 |
| 2400 | 59.70 | 2.0519 | 789548 | 0.0102 | 95 | 1.070E-4 | 24.780 | 22.302 |
| 2400 | 60.37 | 2.0617 | 789637 | 0.0101 | 91 | 1.101E-4 | 24.980 | 22.482 |
| 2400 | 61.07 | 2.0718 | 789731 | 0.0101 | 88 | 1.140E-4 | 25.182 | 22.664 |
| 2400 | 61.81 | 2.0823 | 789820 | 0.0100 | 85 | 1.176E-4 | 25.385 | 22.847 |
| 2400 | 62.51 | 2.0922 | 789901 | 0.0101 | 83 | 1.212E-4 | 25.597 | 23.038 |
| 2400 | 63.25 | 2.1024 | 789983 | 0.0101 | 81 | 1.252E-4 | 25.802 | 23.222 |
| 2400 | 63.97 | 2.1121 | 790060 | 0.0100 | 79 | 1.277E-4 | 26.015 | 23.414 |
| 2400 | 64.72 | 2.1221 | 790136 | 0.0100 | 77 | 1.296E-4 | 26.232 | 23.609 |
| 2400 | 65.52 | 2.1326 | 790216 | 0.0100 | 75 | 1.321E-4 | 26.448 | 23.803 |
| 2400 | 66.29 | 2.1425 | 790291 | 0.0101 | 74 | 1.348E-4 | 26.672 | 24.005 |
| 2400 | 67.07 | 2.1524 | 790365 | 0.0101 | 73 | 1.378E-4 | 26.894 | 24.205 |
| 2400 | 67.87 | 2.1624 | 790435 | 0.0101 | 71 | 1.417E-4 | 27.121 | 24.409 |
| 2400 | 68.70 | 2.1725 | 790505 | 0.0102 | 69 | 1.460E-4 | 27.355 | 24.619 |
| 2400 | 69.55 | 2.1828 | 790575 | 0.0102 | 67 | 1.520E-4 | 27.593 | 24.833 |
| 2400 | 70.41 | 2.1931 | 790642 | 0.0102 | 64 | 1.595E-4 | 27.836 | 25.052 |
| 2400 | 71.29 | 2.2034 | 790707 | 0.0101 | 61 | 1.679E-4 | 28.083 | 25.275 |
| 2400 | 72.19 | 2.2136 | 790764 | 0.0101 | 58 | 1.767E-4 | 28.330 | 25.496 |
| 2400 | 73.07 | 2.2236 | 790817 | 0.0101 | 55 | 1.845E-4 | 28.578 | 25.720 |
| 2400 | 73.95 | 2.2333 | 790870 | 0.0100 | 52 | 1.910E-4 | 28.831 | 25.948 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^0.5) | deltaK |
|--------------|--------|-----------|--------|------------|----|-------------------|-----------------------|----------|
| 2400 | 74.90 | 2.2436 | 790921 | 0.0100 | 52 | 1.949E-4 | 29.083 | 26.175 |
| 2400 | 75.83 | 2.2535 | 790971 | 0.0101 | 50 | 1.992E-4 | 29.344 | 26.409 |
| 2400 | 76.76 | 2.2634 | 791021 | 0.0101 | 48 | 2.065E-4 | 29.612 | 26.650 |
| 2400 | 77.77 | 2.2738 | 791073 | 0.0101 | 47 | 2.162E-4 | 29.880 | 26.892 |
| 2400 | 78.79 | 2.2841 | 791119 | 0.0102 | 45 | 2.304E-4 | 30.156 | 27.140 |
| 2400 | 79.78 | 2.2939 | 791159 | 0.0103 | 42 | 2.470E-4 | 30.436 | 27.392 |
| 2400 | 80.83 | 2.3042 | 791201 | 0.0102 | 39 | 2.656E-4 | 30.728 | 27.654 |
| 2400 | 81.94 | 2.3149 | 791239 | 0.0101 | 36 | 2.831E-4 | 31.016 | 27.915 |
| 2400 | 83.03 | 2.3251 | 791273 | 0.0102 | 34 | 3.016E-4 | 31.315 | 28.182 |
| 2400 | 84.09 | 2.3349 | 791305 | 0.0102 | 32 | 3.218E-4 | 31.604 | 28.443 |
| 2400 | 85.13 | 2.3444 | 791334 | 0.0101 | 30 | 3.387E-4 | 31.910 | 28.718 |
| 2400 | 86.34 | 2.3552 | 791364 | 0.0099 | 28 | 3.538E-4 | 32.213 | 28.991 |
| 2400 | 87.54 | 2.3656 | 791392 | 0.0101 | 27 | 3.698E-4 | 32.533 | 29.278 |
| 2400 | 88.69 | 2.3755 | 791418 | 0.0101 | 26 | 3.849E-4 | 32.842 | 29.557 |
| 2400 | 89.80 | 2.3848 | 791443 | 0.0100 | 25 | 3.999E-4 | 33.165 | 29.847 |
| 2400 | 91.06 | 2.3952 | 791468 | 0.0100 | 24 | 4.195E-4 | 33.479 | 30.130 |
| 2400 | 92.31 | 2.4053 | 791491 | 0.0101 | 23 | 4.415E-4 | 33.818 | 30.435 |
| 2400 | 93.59 | 2.4154 | 791514 | 0.0103 | 22 | 4.665E-4 | 34.159 | 30.741 |
| 2400 | 94.90 | 2.4257 | 791535 | 0.0102 | 21 | 4.900E-4 | 34.513 | 31.060 |
| 2400 | 96.30 | 2.4363 | 791556 | 0.0101 | 20 | 5.180E-4 | 34.866 | 31.378 |
| 2400 | 97.65 | 2.4464 | 791575 | 0.0101 | 18 | 5.504E-4 | 35.232 | 31.707 |
| 2400 | 99.02 | 2.4564 | 791593 | 0.0101 | 17 | 5.963E-4 | 35.586 | 32.025 |
| 2400 | 100.37 | 2.4661 | 791609 | 0.0101 | 16 | 6.434E-4 | 35.950 | 32.352 |
| 2400 | 101.77 | 2.4759 | 791624 | 0.0100 | 15 | 6.871E-4 | 36.318 | 32.683 |
| 2400 | 103.25 | 2.4861 | 791637 | 0.0101 | 14 | 7.346E-4 | 36.704 | 33.030 |
| 2400 | 104.81 | 2.4966 | 791651 | 0.0102 | 13 | 7.867E-4 | 37.087 | 33.374 |
| 2399 | 106.30 | 2.5064 | 791664 | 0.0102 | 12 | 8.499E-4 | 37.508 | 33.753 |
| 2400 | 107.97 | 2.5172 | 791676 | 0.0107 | 12 | 9.410E-4 | 37.904 | 34.107 |
| 2399 | 109.57 | 2.5274 | 791687 | 0.0102 | 10 | 1.031E-3 | 38.327 | 34.486 * |
| 2399 | 111.19 | 2.5374 | 791696 | 0.0102 | 9 | 1.119E-3 | 38.808 | 34.914 * |
| 2400 | 113.30 | 2.5502 | 791706 | 0.0100 | 9 | 1.217E-3 | 39.177 | 35.250 * |
| 2400 | 114.60 | 2.5578 | 791713 | 0.0101 | 8 | 1.291E-3 | 39.669 | 35.689 * |
| 2399 | 116.29 | 2.5676 | 791720 | 0.0101 | 8 | 1.346E-3 | 40.050 | 36.037 * |
| 2399 | 118.03 | 2.5775 | 791727 | 0.0097 | 7 | 1.402E-3 | 40.503 | 36.448 * |
| 2400 | 119.92 | 2.5879 | 791734 | 0.0102 | 7 | 1.456E-3 | 40.952 | 36.848 * |
| 2399 | 121.76 | 2.5979 | 791741 | 0.0103 | 7 | 1.518E-3 | 41.433 | 37.279 * |
| 2399 | 123.70 | 2.6082 | 791748 | 0.0104 | 6 | 1.633E-3 | 41.918 | 37.711 * |
| 2398 | 125.79 | 2.6190 | 791755 | 0.0103 | 6 | 1.773E-3 | 42.423 | 38.161 * |
| 2399 | 127.89 | 2.6296 | 791760 | 0.0103 | 6 | 1.932E-3 | 42.933 | 38.616 * |
| 2398 | 129.96 | 2.6399 | 791765 | 0.0104 | 5 | 2.122E-3 | 43.454 | 39.087 * |
| 2399 | 131.99 | 2.6496 | 791770 | 0.0104 | 5 | 2.315E-3 | 43.966 | 39.537 * |
| 2398 | 134.17 | 2.6599 | 791774 | 0.0105 | 4 | 2.545E-3 | 44.502 | 40.019 * |
| 2397 | 136.51 | 2.6706 | 791778 | 0.0104 | 4 | 2.814E-3 | 45.051 | 40.503 * |
| 2397 | 138.90 | 2.6813 | 791782 | 0.0106 | 3 | 3.270E-3 | 45.620 | 41.010 * |
| 2395 | 141.47 | 2.6925 | 791785 | 0.0119 | 3 | 4.179E-3 | 46.087 | 41.403 * |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^0.5) | deltaK |
|--------------|--------|-----------|--------|------------|----|-------------------|-----------------------|----------|
| 2383 | 143.82 | 2.7025 | 791788 | 0.0129 | 3 | 4.988E-3 | 46.684 | 41.931 * |
| 2384 | 146.36 | 2.7131 | 791790 | 0.0286 | 4 | 7.155E-3 | 47.305 | 42.443 * |
| 2375 | 150.87 | 2.7312 | 791792 | 0.0349 | 5 | 6.974E-3 | 47.886 | 42.911 * |
| | 155.25 | 2.7479 | 791795 | | | | | |

Automated Fatigue Crack
Growth Rate Analysis

| | | | |
|-----------------|--------------|---------------|------|
| Test ID | 5383-FCG-45 | Geometry | C(T) |
| Contract | SSC 10624-01 | Orientation | T-L |
| Material | 5383-H116 | Yield (ksi) | 35.4 |
| Temperature (F) | 75 | Modulus (Msi) | 10.5 |
| Environment | RH = 40% | | |

Specimen Dimensions (in)

| | | | |
|---------------|-------|-------------|-------|
| Thickness | 0.486 | Height | 2.400 |
| Net Thickness | 0.486 | Notch Depth | 1.000 |
| Width | 4.002 | Gage Length | 0.500 |

Precrack Parameters

| | | | |
|--------------|-------|--------------------|------|
| Pmax (lbs) | 859.0 | Stress Ratio | 0.10 |
| Final a (in) | 1.050 | Kmax (ksi sqr[in]) | 4.50 |

Test Parameters

| EvBP | Freq | Pmax | R | Ai | Kmaxi | C | DKi |
|--------|------|------|------|-------|-------|------|------|
| 23.789 | 5.00 | 0 | 0.10 | 1.140 | 3.10 | 4.00 | 0.00 |
| 30.408 | 5.00 | 0 | 0.10 | 1.416 | 9.34 | 2.00 | 0.00 |
| 48.973 | 5.00 | 2575 | 0.10 | 0.000 | 0.00 | 0.00 | 0.00 |

| K Coeff | C Coeff |
|---------|----------|
| .886 | 1.00098 |
| 4.64 | -4.66951 |
| -13.32 | 18.4601 |
| 14.72 | -236.825 |
| -5.6 | 1214.88 |
| . | -2143.57 |

Visual Observations

| EvB/P | Crack(EvB/P) | Crack(visual) | Error | CAF |
|---------|--------------|---------------|--------|-------|
| 20.753 | 0.983 | 1.002 | 0.019 | 0.993 |
| 21.841 | 1.041 | 1.040 | -0.001 | 0.991 |
| 23.480 | 1.121 | 1.100 | -0.021 | 0.989 |
| 23.760 | 1.134 | 1.170 | 0.036 | 0.989 |
| 26.667 | 1.260 | 1.260 | 0.000 | 0.986 |
| 27.531 | 1.294 | 1.280 | -0.014 | 0.985 |
| 30.339 | 1.397 | 1.380 | -0.017 | 0.983 |
| 34.274 | 1.523 | 1.490 | -0.033 | 0.980 |
| 48.661 | 1.865 | 1.880 | 0.015 | 0.972 |
| 59.300 | 2.043 | 2.080 | 0.037 | 0.969 |
| 66.619 | 2.142 | 2.120 | -0.022 | 0.966 |
| 101.006 | 2.462 | 2.460 | -0.002 | 0.959 |

Comments

Date of test: 9/17/2006

Waveform Type

Sine

Test ID 5383-FCG-46

Page 1

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in] ^{0.5}) | deltaK |
|--------------|-------|-----------|--------|------------|-------|-------------------|-----------------------------------|--------|
| | 23.88 | 1.1397 | 98879 | | | | | |
| 592 | 23.99 | 1.1451 | 149517 | 0.0100 | 95897 | 1.043E-7 | 3.295 | 2.966 |
| 601 | 24.10 | 1.1497 | 194776 | 0.0102 | 80660 | 1.269E-7 | 3.370 | 3.033 |
| 613 | 24.22 | 1.1554 | 230177 | 0.0051 | 36339 | 1.477E-7 | 3.435 | 3.091 |
| 623 | 24.32 | 1.1601 | 262838 | 0.0049 | 31739 | 1.654E-7 | 3.508 | 3.158 |
| 633 | 24.43 | 1.1650 | 290853 | 0.0050 | 27100 | 1.889E-7 | 3.580 | 3.222 |
| 644 | 24.55 | 1.1701 | 316914 | 0.0048 | 24356 | 2.097E-7 | 3.649 | 3.284 |
| 654 | 24.65 | 1.1748 | 339948 | 0.0049 | 21817 | 2.344E-7 | 3.725 | 3.352 |
| 666 | 24.77 | 1.1798 | 357374 | 0.0049 | 19901 | 2.505E-7 | 3.795 | 3.415 |
| 676 | 24.87 | 1.1844 | 376314 | 0.0049 | 18184 | 2.714E-7 | 3.874 | 3.487 |
| 688 | 24.99 | 1.1896 | 393740 | 0.0049 | 16568 | 2.941E-7 | 3.948 | 3.553 |
| 699 | 25.09 | 1.1941 | 410257 | 0.0049 | 15684 | 3.184E-7 | 4.031 | 3.628 |
| 711 | 25.21 | 1.1994 | 426017 | 0.0050 | 14224 | 3.586E-7 | 4.113 | 3.701 |
| 724 | 25.33 | 1.2044 | 439353 | 0.0049 | 12936 | 3.988E-7 | 4.195 | 3.776 |
| 736 | 25.44 | 1.2093 | 451477 | 0.0049 | 11685 | 4.385E-7 | 4.285 | 3.856 |
| 749 | 25.56 | 1.2143 | 461659 | 0.0049 | 10480 | 4.783E-7 | 4.368 | 3.931 |
| 761 | 25.67 | 1.2191 | 471354 | 0.0049 | 9615 | 5.147E-7 | 4.457 | 4.011 |
| 774 | 25.78 | 1.2237 | 480369 | 0.0049 | 8757 | 5.580E-7 | 4.547 | 4.093 |
| 788 | 25.91 | 1.2289 | 488898 | 0.0048 | 8082 | 6.017E-7 | 4.636 | 4.172 |
| 801 | 26.02 | 1.2336 | 497041 | 0.0049 | 7501 | 6.660E-7 | 4.731 | 4.258 |
| 814 | 26.14 | 1.2387 | 504019 | 0.0049 | 6919 | 7.224E-7 | 4.822 | 4.340 |
| 827 | 26.25 | 1.2431 | 510148 | 0.0049 | 6326 | 7.842E-7 | 4.924 | 4.432 |
| 842 | 26.38 | 1.2486 | 516358 | 0.0100 | 11736 | 8.521E-7 | 5.017 | 4.516 |
| 856 | 26.49 | 1.2531 | 521884 | 0.0095 | 10496 | 9.030E-7 | 5.124 | 4.612 |
| 870 | 26.62 | 1.2580 | 526854 | 0.0450 | 31113 | 1.446E-6 | 0.000 | 0.000 |
| 999 | 27.63 | 1.2980 | 552997 | 0.0442 | 27932 | 1.581E-6 | 0.000 | 0.000 |
| 1013 | 27.73 | 1.3022 | 554786 | 0.0089 | 3659 | 2.434E-6 | 6.265 | 5.638 |
| 1030 | 27.86 | 1.3069 | 556656 | 0.0095 | 3577 | 2.662E-6 | 6.379 | 5.741 |
| 1047 | 27.98 | 1.3117 | 558363 | 0.0098 | 3333 | 2.933E-6 | 6.507 | 5.856 |
| 1065 | 28.11 | 1.3167 | 559989 | 0.0049 | 1561 | 3.203E-6 | 6.638 | 5.974 |
| 1083 | 28.25 | 1.3218 | 561534 | 0.0050 | 1434 | 3.517E-6 | 6.775 | 6.098 |
| 1102 | 28.38 | 1.3268 | 562916 | 0.0050 | 1315 | 3.859E-6 | 6.914 | 6.223 |
| 1121 | 28.51 | 1.3318 | 564152 | 0.0049 | 1199 | 4.225E-6 | 7.057 | 6.351 |
| 1140 | 28.65 | 1.3367 | 565260 | 0.0049 | 1088 | 4.617E-6 | 7.197 | 6.477 |
| 1159 | 28.78 | 1.3415 | 566255 | 0.0049 | 989 | 5.011E-6 | 7.343 | 6.609 |
| 1179 | 28.91 | 1.3463 | 567184 | 0.0049 | 907 | 5.431E-6 | 7.489 | 6.740 |
| 1199 | 29.04 | 1.3513 | 568059 | 0.0049 | 840 | 5.864E-6 | 7.638 | 6.874 |
| 1219 | 29.17 | 1.3561 | 568851 | 0.0049 | 786 | 6.289E-6 | 7.794 | 7.015 |
| 1240 | 29.31 | 1.3610 | 569595 | 0.0049 | 737 | 6.695E-6 | 7.948 | 7.153 |
| 1261 | 29.45 | 1.3659 | 570299 | 0.0049 | 687 | 7.160E-6 | 8.110 | 7.299 |
| 1282 | 29.59 | 1.3709 | 570970 | 0.0049 | 640 | 7.651E-6 | 8.273 | 7.445 |
| 1304 | 29.72 | 1.3757 | 571607 | 0.0049 | 599 | 8.187E-6 | 8.442 | 7.598 |
| 1326 | 29.86 | 1.3807 | 572178 | 0.0049 | 563 | 8.718E-6 | 8.606 | 7.745 |
| 1347 | 30.00 | 1.3853 | 572690 | 0.0094 | 1010 | 9.343E-6 | 8.781 | 7.903 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^0.5) | deltaK |
|--------------|-------|-----------|--------|------------|-----|-------------------|-----------------------|--------|
| 1370 | 30.13 | 1.3902 | 573188 | 0.0097 | 989 | 9.839E-6 | 8.952 | 8.057 |
| | 30.27 | 1.3951 | 573679 | | | | | |
| | 34.37 | 1.5263 | 581958 | | | | | |
| 1699 | 34.66 | 1.5348 | 582335 | 0.0183 | 857 | 2.135E-5 | 12.199 | 10.979 |
| 1722 | 34.99 | 1.5446 | 582815 | 0.0196 | 950 | 2.067E-5 | 12.426 | 11.183 |
| 1744 | 35.33 | 1.5544 | 583285 | 0.0198 | 919 | 2.153E-5 | 12.676 | 11.408 |
| 1768 | 35.69 | 1.5644 | 583734 | 0.0099 | 443 | 2.234E-5 | 12.930 | 11.637 |
| 1792 | 36.04 | 1.5744 | 584171 | 0.0099 | 426 | 2.320E-5 | 13.192 | 11.873 |
| 1817 | 36.40 | 1.5845 | 584596 | 0.0099 | 410 | 2.414E-5 | 13.457 | 12.112 |
| 1841 | 36.76 | 1.5942 | 584990 | 0.0099 | 396 | 2.495E-5 | 13.727 | 12.354 |
| 1865 | 37.11 | 1.6039 | 585368 | 0.0098 | 378 | 2.593E-5 | 14.004 | 12.604 |
| 1891 | 37.49 | 1.6140 | 585746 | 0.0098 | 362 | 2.698E-5 | 14.281 | 12.853 |
| 1916 | 37.86 | 1.6237 | 586109 | 0.0099 | 352 | 2.812E-5 | 14.569 | 13.112 |
| 1941 | 38.23 | 1.6335 | 586439 | 0.0099 | 339 | 2.929E-5 | 14.859 | 13.373 |
| 1967 | 38.61 | 1.6433 | 586770 | 0.0098 | 323 | 3.052E-5 | 15.163 | 13.646 |
| 1995 | 39.02 | 1.6537 | 587101 | 0.0099 | 309 | 3.195E-5 | 15.467 | 13.920 |
| 2021 | 39.41 | 1.6636 | 587400 | 0.0099 | 298 | 3.323E-5 | 15.780 | 14.202 |
| 2048 | 39.79 | 1.6730 | 587682 | 0.0099 | 285 | 3.467E-5 | 16.100 | 14.490 |
| 2075 | 40.20 | 1.6831 | 587961 | 0.0098 | 270 | 3.631E-5 | 16.417 | 14.775 |
| 2103 | 40.61 | 1.6929 | 588228 | 0.0098 | 258 | 3.806E-5 | 16.750 | 15.075 |
| 2130 | 41.02 | 1.7028 | 588482 | 0.0099 | 247 | 3.998E-5 | 17.085 | 15.377 |
| 2159 | 41.44 | 1.7128 | 588723 | 0.0098 | 234 | 4.194E-5 | 17.430 | 15.687 |
| 2188 | 41.86 | 1.7226 | 588950 | 0.0098 | 222 | 4.417E-5 | 17.777 | 15.999 |
| 2216 | 42.29 | 1.7323 | 589163 | 0.0098 | 211 | 4.649E-5 | 18.128 | 16.316 |
| 2244 | 42.71 | 1.7418 | 589366 | 0.0098 | 201 | 4.896E-5 | 18.486 | 16.638 |
| 2273 | 43.14 | 1.7517 | 589559 | 0.0098 | 189 | 5.176E-5 | 18.856 | 16.971 |
| 2304 | 43.60 | 1.7617 | 589748 | 0.0098 | 179 | 5.505E-5 | 19.235 | 17.311 |
| 2334 | 44.06 | 1.7717 | 589927 | 0.0099 | 169 | 5.879E-5 | 19.616 | 17.654 |
| 2363 | 44.50 | 1.7812 | 590082 | 0.0099 | 159 | 6.258E-5 | 20.014 | 18.013 |
| 2395 | 44.96 | 1.7911 | 590234 | 0.0099 | 148 | 6.718E-5 | 20.408 | 18.367 |
| 2426 | 45.44 | 1.8011 | 590379 | 0.0099 | 138 | 7.229E-5 | 20.815 | 18.734 |
| 2457 | 45.91 | 1.8109 | 590511 | 0.0099 | 130 | 7.734E-5 | 21.241 | 19.117 |
| 2489 | 46.41 | 1.8211 | 590637 | 0.0099 | 121 | 8.271E-5 | 21.667 | 19.500 |
| 2522 | 46.90 | 1.8310 | 590752 | 0.0099 | 113 | 8.836E-5 | 22.103 | 19.892 |
| 2554 | 47.39 | 1.8407 | 590859 | 0.0195 | 209 | 9.346E-5 | 22.548 | 20.293 |
| 2587 | 47.89 | 1.8506 | 590961 | 0.0199 | 198 | 1.003E-4 | 22.995 | 20.696 |
| | 48.41 | 1.8606 | 591057 | | | | | |
| | 48.97 | 1.8713 | 591167 | | | | | |
| 2575 | 49.45 | 1.8803 | 591269 | 0.0190 | 211 | 8.982E-5 | 23.393 | 21.054 |
| 2575 | 49.99 | 1.8902 | 591378 | 0.0198 | 215 | 9.223E-5 | 23.554 | 21.199 |
| 2575 | 50.53 | 1.9001 | 591484 | 0.0197 | 208 | 9.493E-5 | 23.726 | 21.353 |
| 2575 | 51.08 | 1.9100 | 591586 | 0.0099 | 99 | 9.993E-5 | 23.898 | 21.508 |
| 2575 | 51.63 | 1.9197 | 591679 | 0.0098 | 95 | 1.038E-4 | 24.073 | 21.666 |
| 2575 | 52.20 | 1.9297 | 591773 | 0.0099 | 92 | 1.073E-4 | 24.249 | 21.824 |
| 2575 | 52.77 | 1.9396 | 591862 | 0.0099 | 90 | 1.103E-4 | 24.427 | 21.984 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^1.5) | deltaK |
|--------------|--------|-----------|--------|------------|-----|-------------------|-----------------------|----------|
| 2575 | 53.34 | 1.9493 | 591947 | 0.0099 | 87 | 1.125E-4 | 24.609 | 22.148 |
| 2575 | 53.93 | 1.9592 | 592037 | 0.0099 | 85 | 1.157E-4 | 24.792 | 22.313 |
| 2575 | 54.54 | 1.9693 | 592123 | 0.0100 | 83 | 1.194E-4 | 24.977 | 22.480 |
| 2575 | 55.14 | 1.9790 | 592203 | 0.0100 | 81 | 1.236E-4 | 25.171 | 22.654 |
| 2575 | 55.78 | 1.9893 | 592285 | 0.0099 | 77 | 1.289E-4 | 25.364 | 22.828 |
| 2575 | 56.44 | 1.9997 | 592362 | 0.0099 | 74 | 1.338E-4 | 25.557 | 23.001 |
| 2575 | 57.04 | 2.0091 | 592430 | 0.0099 | 71 | 1.387E-4 | 25.756 | 23.180 |
| 2575 | 57.68 | 2.0188 | 592500 | 0.0194 | 136 | 1.427E-4 | 25.947 | 23.352 |
| 2575 | 58.32 | 2.0285 | 592566 | 0.0197 | 131 | 1.504E-4 | 26.148 | 23.533 |
| 2575 | 59.00 | 2.0385 | 592631 | 0.1208 | 649 | 1.862E-4 | 0.000 | 0.000 |
| 2575 | 67.20 | 2.1493 | 593215 | 0.1291 | 660 | 1.956E-4 | 0.000 | 0.000 |
| 2575 | 68.71 | 2.1676 | 593291 | 0.0281 | 114 | 2.468E-4 | 29.161 | 26.243 |
| 2575 | 69.53 | 2.1775 | 593329 | 0.0199 | 76 | 2.613E-4 | 29.511 | 26.560 |
| 2575 | 70.39 | 2.1875 | 593367 | 0.0198 | 75 | 2.642E-4 | 29.760 | 26.784 |
| 2575 | 71.24 | 2.1973 | 593404 | 0.0099 | 37 | 2.699E-4 | 30.020 | 27.017 |
| 2575 | 72.16 | 2.2076 | 593442 | 0.0100 | 35 | 2.805E-4 | 30.276 | 27.248 |
| 2575 | 73.06 | 2.2176 | 593478 | 0.0101 | 34 | 2.963E-4 | 30.539 | 27.485 |
| 2575 | 73.94 | 2.2272 | 593510 | 0.0101 | 33 | 3.121E-4 | 30.810 | 27.728 |
| 2575 | 74.90 | 2.2375 | 593541 | 0.0100 | 30 | 3.343E-4 | 31.083 | 27.974 |
| 2575 | 75.89 | 2.2480 | 593571 | 0.0100 | 28 | 3.560E-4 | 31.359 | 28.222 |
| 2575 | 76.83 | 2.2578 | 593599 | 0.0100 | 27 | 3.710E-4 | 31.640 | 28.475 |
| 2575 | 77.78 | 2.2674 | 593622 | 0.0099 | 26 | 3.820E-4 | 31.921 | 28.728 |
| 2575 | 78.78 | 2.2773 | 593647 | 0.0100 | 25 | 3.982E-4 | 32.202 | 28.980 |
| 2575 | 79.78 | 2.2872 | 593673 | 0.0100 | 24 | 4.137E-4 | 32.491 | 29.242 |
| 2575 | 80.80 | 2.2970 | 593697 | 0.0100 | 24 | 4.265E-4 | 32.797 | 29.516 |
| 2575 | 81.93 | 2.3077 | 593720 | 0.0100 | 23 | 4.477E-4 | 33.092 | 29.782 |
| 2575 | 82.98 | 2.3175 | 593742 | 0.0100 | 21 | 4.736E-4 | 33.413 | 30.070 |
| 2575 | 84.10 | 2.3277 | 593763 | 0.0101 | 20 | 5.006E-4 | 33.718 | 30.345 |
| 2575 | 85.19 | 2.3375 | 593782 | 0.0099 | 19 | 5.308E-4 | 34.035 | 30.630 |
| 2575 | 86.31 | 2.3473 | 593800 | 0.0099 | 17 | 5.741E-4 | 34.362 | 30.924 |
| 2575 | 87.52 | 2.3578 | 593818 | 0.0099 | 16 | 6.301E-4 | 34.678 | 31.208 |
| 2575 | 88.65 | 2.3674 | 593833 | 0.0100 | 15 | 6.825E-4 | 35.010 | 31.507 |
| 2575 | 89.80 | 2.3769 | 593846 | 0.0100 | 14 | 7.337E-4 | 35.349 | 31.812 |
| 2575 | 91.07 | 2.3873 | 593859 | 0.0099 | 13 | 7.798E-4 | 35.688 | 32.117 |
| 2575 | 92.36 | 2.3976 | 593872 | 0.0100 | 12 | 8.232E-4 | 36.037 | 32.430 |
| 2575 | 93.58 | 2.4071 | 593883 | 0.0101 | 12 | 8.526E-4 | 36.398 | 32.755 |
| 2575 | 94.89 | 2.4172 | 593895 | 0.0101 | 12 | 8.796E-4 | 36.754 | 33.075 |
| 2575 | 96.25 | 2.4275 | 593906 | 0.0100 | 11 | 9.133E-4 | 37.128 | 33.411 |
| 2575 | 97.64 | 2.4377 | 593917 | 0.0105 | 11 | 9.704E-4 | 37.507 | 33.752 |
| 2575 | 99.03 | 2.4478 | 593928 | 0.0102 | 10 | 1.028E-3 | 37.884 | 34.091 |
| 2574 | 100.38 | 2.4574 | 593937 | 0.0103 | 10 | 1.093E-3 | 38.320 | 34.476 |
| 2574 | 102.16 | 2.4699 | 593947 | 0.0102 | 9 | 1.182E-3 | 38.681 | 34.806 |
| 2575 | 103.40 | 2.4785 | 593955 | 0.0102 | 8 | 1.253E-3 | 39.148 | 35.222 * |
| 2574 | 105.02 | 2.4895 | 593963 | 0.0103 | 8 | 1.345E-3 | 39.522 | 35.562 * |
| 2574 | 106.48 | 2.4991 | 593970 | 0.0100 | 7 | 1.445E-3 | 39.954 | 35.953 * |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in] ^{.5}) | |
|--------------|--------|-----------|--------|------------|----|-------------------|--------|------------------------------------|---|
| 2575 | 107.99 | 2.5089 | 593977 | 0.0103 | 7 | 1.552E-3 | 40.371 | 36.323 | * |
| 2574 | 109.62 | 2.5193 | 593983 | 0.0101 | 6 | 1.654E-3 | 40.814 | 36.721 | * |
| 2574 | 111.32 | 2.5298 | 593989 | 0.0102 | 6 | 1.810E-3 | 41.261 | 37.121 | * |
| 2574 | 113.00 | 2.5401 | 593995 | 0.0103 | 5 | 1.942E-3 | 41.722 | 37.534 | * |
| 2574 | 114.72 | 2.5503 | 594000 | 0.0103 | 5 | 2.097E-3 | 42.182 | 37.945 | * |
| 2574 | 116.41 | 2.5602 | 594004 | 0.0105 | 5 | 2.191E-3 | 42.653 | 38.366 | * |
| 2574 | 118.22 | 2.5704 | 594009 | 0.0104 | 4 | 2.384E-3 | 43.147 | 38.809 | * |
| 2574 | 120.16 | 2.5813 | 594013 | 0.0103 | 4 | 2.538E-3 | 43.660 | 39.267 | * |
| 2573 | 122.25 | 2.5926 | 594018 | 0.0103 | 4 | 2.806E-3 | 44.162 | 39.715 | * |
| 2572 | 124.12 | 2.6026 | 594021 | 0.0105 | 4 | 3.032E-3 | 44.680 | 40.178 | * |
| 2573 | 125.91 | 2.6118 | 594024 | 0.0107 | 3 | 3.289E-3 | 45.169 | 40.608 | * |
| 2571 | 127.90 | 2.6220 | 594027 | 0.0107 | 3 | 3.706E-3 | 45.683 | 41.062 | * |
| 2568 | 130.18 | 2.6333 | 594030 | 0.0106 | 3 | 4.402E-3 | 46.204 | 41.509 | * |
| 2560 | 132.74 | 2.6456 | 594033 | 0.0107 | 2 | 5.107E-3 | 46.800 | 42.032 | * |
| 2563 | 135.08 | 2.6566 | 594035 | 0.0109 | 2 | 6.174E-3 | 47.313 | 42.472 | * |
| 2560 | 137.14 | 2.6661 | 594036 | 0.0106 | 2 | 6.856E-3 | 47.891 | 42.976 | * |
| 2556 | 139.37 | 2.6761 | 594038 | 0.0101 | 1 | 8.108E-3 | 48.307 | 43.322 | * |
| 2540 | 141.95 | 2.6873 | 594039 | 0.0207 | 2 | 1.033E-2 | 48.759 | 43.700 | * |
| 2532 | 144.15 | 2.6967 | 594040 | 0.0191 | 2 | 9.541E-3 | 49.066 | 43.917 | * |
| | 146.48 | 2.7064 | 594041 | | | | | | |

Automated Fatigue Crack
Growth Rate Analysis

| | | | |
|-----------------|---------------|---------------|------|
| Test ID | 5383-FCG-4pt5 | Geometry | C(T) |
| Contract | SSC 10624-01 | Orientation | T-L |
| Material | 5383-H116 | Yield (ksi) | 35.4 |
| Temperature (F) | 75 | Modulus (Msi) | 10.5 |
| Environment | RH = 40% | | |

Specimen Dimensions (in)

| | | | |
|---------------|-------|-------------|-------|
| Thickness | 0.486 | Height | 2.400 |
| Net Thickness | 0.486 | Notch Depth | 1.000 |
| Width | 4.002 | Gage Length | 0.500 |

Precrack Parameters

| | | | |
|--------------|-------|---------------------|------|
| Pmax (lbs) | 859.0 | Stress Ratio | 0.10 |
| Final a (in) | 1.050 | Kmax (ksi sqrt[in]) | 4.50 |

Test Parameters

| EvBP | Freq | Pmax | R | Ai | Kmaxi | C | DKi |
|--------|------|------|------|-------|-------|------|------|
| 23.789 | 0.50 | 0 | 0.10 | 1.140 | 3.10 | 4.00 | 0.00 |
| 30.408 | 0.50 | 0 | 0.10 | 1.416 | 9.34 | 2.00 | 0.00 |
| 48.973 | 0.50 | 2575 | 0.10 | 0.000 | 0.00 | 0.00 | 0.00 |

| K Coeff | C Coeff |
|---------|----------|
| .886 | 1.00098 |
| 4.64 | -4.66951 |
| -13.32 | 18.4601 |
| 14.72 | -236.825 |
| -5.6 | 1214.88 |
| . | -2143.57 |

Visual Observations

| EvB/P | Crack(EvB/P) | Crack(visual) | Error | CAF |
|---------|--------------|---------------|--------|-------|
| 20.753 | 0.983 | 1.002 | 0.019 | 0.993 |
| 21.841 | 1.041 | 1.040 | -0.001 | 0.991 |
| 23.480 | 1.121 | 1.100 | -0.021 | 0.989 |
| 23.760 | 1.134 | 1.170 | 0.036 | 0.989 |
| 26.667 | 1.260 | 1.260 | 0.000 | 0.986 |
| 27.531 | 1.294 | 1.280 | -0.014 | 0.985 |
| 30.339 | 1.397 | 1.380 | -0.017 | 0.983 |
| 34.274 | 1.523 | 1.490 | -0.033 | 0.980 |
| 48.661 | 1.865 | 1.880 | 0.015 | 0.972 |
| 59.300 | 2.043 | 2.080 | 0.037 | 0.969 |
| 66.619 | 2.142 | 2.120 | -0.022 | 0.966 |
| 101.006 | 2.462 | 2.460 | -0.002 | 0.959 |

Comments

Date of test: 9/17/2006

Waveform Type

Sine

Test ID 5383-FCG-4pt5

Page 1

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^1.5) | deltaK |
|--------------|-------|-----------|--------|------------|-------|-------------------|-----------------------|--------|
| | 26.74 | 1.2630 | 529674 | | | | | |
| 890 | 26.77 | 1.2641 | 530731 | 0.0031 | 2723 | 1.140E-6 | 5.370 | 4.833 |
| 896 | 26.81 | 1.2661 | 532397 | 0.0040 | 3305 | 1.196E-6 | 5.405 | 4.865 |
| 902 | 26.86 | 1.2680 | 534036 | 0.0018 | 1489 | 1.232E-6 | 5.449 | 4.904 |
| 908 | 26.91 | 1.2701 | 535687 | 0.0020 | 1546 | 1.266E-6 | 5.492 | 4.943 |
| 914 | 26.96 | 1.2720 | 537212 | 0.0020 | 1512 | 1.305E-6 | 5.536 | 4.983 |
| 920 | 27.01 | 1.2739 | 538610 | 0.0020 | 1482 | 1.337E-6 | 5.580 | 5.022 |
| 927 | 27.06 | 1.2759 | 540007 | 0.0020 | 1440 | 1.372E-6 | 5.625 | 5.063 |
| 933 | 27.11 | 1.2779 | 541468 | 0.0020 | 1398 | 1.407E-6 | 5.671 | 5.104 |
| 939 | 27.16 | 1.2799 | 542928 | 0.0020 | 1353 | 1.449E-6 | 5.717 | 5.146 |
| 946 | 27.21 | 1.2819 | 544325 | 0.0020 | 1306 | 1.518E-6 | 5.764 | 5.188 |
| 952 | 27.26 | 1.2839 | 545597 | 0.0020 | 1241 | 1.596E-6 | 5.810 | 5.229 |
| 959 | 27.31 | 1.2858 | 546727 | 0.0019 | 1184 | 1.657E-6 | 5.858 | 5.272 |
| 965 | 27.36 | 1.2878 | 547845 | 0.0020 | 1137 | 1.724E-6 | 5.903 | 5.313 |
| 971 | 27.41 | 1.2896 | 548912 | 0.0038 | 2185 | 1.744E-6 | 5.950 | 5.355 |
| 978 | 27.46 | 1.2916 | 550030 | 0.0040 | 2235 | 1.809E-6 | 5.998 | 5.399 |
| 985 | 27.51 | 1.2937 | 551147 | 0.1081 | 23998 | 4.504E-6 | 0.000 | 0.000 |
| 1410 | 30.41 | 1.3997 | 574028 | 0.1074 | 22994 | 4.672E-6 | 0.000 | 0.000 |
| 1413 | 30.45 | 1.4011 | 574141 | 0.0035 | 264 | 1.315E-5 | 9.300 | 8.370 |
| 1417 | 30.51 | 1.4031 | 574292 | 0.0041 | 318 | 1.283E-5 | 9.333 | 8.399 |
| 1421 | 30.57 | 1.4052 | 574459 | 0.0040 | 332 | 1.219E-5 | 9.371 | 8.434 |
| 1425 | 30.63 | 1.4072 | 574624 | 0.0020 | 153 | 1.289E-5 | 9.409 | 8.468 |
| 1429 | 30.68 | 1.4091 | 574769 | 0.0020 | 153 | 1.289E-5 | 9.446 | 8.501 |
| 1432 | 30.74 | 1.4110 | 574908 | 0.0020 | 151 | 1.304E-5 | 9.484 | 8.535 |
| 1436 | 30.80 | 1.4131 | 575060 | 0.0020 | 148 | 1.320E-5 | 9.520 | 8.568 |
| 1440 | 30.86 | 1.4149 | 575212 | 0.0020 | 148 | 1.324E-5 | 9.559 | 8.603 |
| 1444 | 30.91 | 1.4169 | 575364 | 0.0020 | 149 | 1.322E-5 | 9.596 | 8.637 |
| 1448 | 30.97 | 1.4189 | 575509 | 0.0020 | 147 | 1.335E-5 | 9.636 | 8.672 |
| 1452 | 31.03 | 1.4210 | 575655 | 0.0020 | 144 | 1.356E-5 | 9.674 | 8.706 |
| 1456 | 31.09 | 1.4228 | 575800 | 0.0020 | 140 | 1.381E-5 | 9.713 | 8.741 |
| 1460 | 31.15 | 1.4248 | 575939 | 0.0020 | 138 | 1.405E-5 | 9.750 | 8.775 |
| 1464 | 31.20 | 1.4267 | 576077 | 0.0019 | 137 | 1.428E-5 | 9.788 | 8.810 |
| 1468 | 31.26 | 1.4286 | 576203 | 0.0020 | 134 | 1.459E-5 | 9.828 | 8.845 |
| 1472 | 31.32 | 1.4306 | 576339 | 0.0020 | 133 | 1.476E-5 | 9.867 | 8.880 |
| 1476 | 31.38 | 1.4326 | 576476 | 0.0020 | 132 | 1.494E-5 | 9.907 | 8.916 |
| 1480 | 31.44 | 1.4346 | 576603 | 0.0020 | 133 | 1.493E-5 | 9.946 | 8.951 |
| 1484 | 31.50 | 1.4365 | 576735 | 0.0020 | 130 | 1.502E-5 | 9.986 | 8.988 |
| 1488 | 31.56 | 1.4385 | 576867 | 0.0019 | 128 | 1.513E-5 | 10.026 | 9.024 |
| 1492 | 31.62 | 1.4405 | 576999 | 0.0020 | 127 | 1.533E-5 | 10.065 | 9.059 |
| 1496 | 31.68 | 1.4424 | 577121 | 0.0019 | 125 | 1.549E-5 | 10.105 | 9.095 |
| 1500 | 31.74 | 1.4443 | 577243 | 0.0019 | 125 | 1.566E-5 | 10.145 | 9.131 |
| 1504 | 31.80 | 1.4463 | 577365 | 0.0019 | 125 | 1.577E-5 | 10.183 | 9.165 |
| 1508 | 31.85 | 1.4481 | 577482 | 0.0020 | 125 | 1.576E-5 | 10.226 | 9.203 |
| 1512 | 31.92 | 1.4502 | 577614 | 0.0020 | 124 | 1.576E-5 | 10.265 | 9.238 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in]^0.5) |
|--------------|-------|-----------|--------|------------|-------|-------------------|--------|-------------------------|
| 1516 | 31.98 | 1.4521 | 577746 | 0.0019 | 121 | 1.575E-5 | 10.308 | 9.277 |
| 1520 | 32.04 | 1.4542 | 577873 | 0.0040 | 239 | 1.672E-5 | 10.348 | 9.313 |
| 1524 | 32.10 | 1.4561 | 577985 | 0.0036 | 215 | 1.666E-5 | 10.387 | 9.348 |
| 1528 | 32.15 | 1.4578 | 578088 | 0.5905 | 14701 | 4.017E-5 | 0.000 | 0.000 |
| 2574 | 59.55 | 2.0466 | 592686 | 0.5907 | 14611 | 4.043E-5 | 0.000 | 0.000 |
| 2575 | 59.67 | 2.0485 | 592699 | 0.0038 | 27 | 1.409E-4 | 26.554 | 23.896 |
| 2575 | 59.81 | 2.0504 | 592713 | 0.0038 | 26 | 1.452E-4 | 26.595 | 23.935 |
| 2575 | 59.93 | 2.0522 | 592725 | 0.0039 | 26 | 1.505E-4 | 26.638 | 23.974 |
| 2575 | 60.08 | 2.0544 | 592739 | 0.0019 | 13 | 1.514E-4 | 26.676 | 24.009 |
| 2575 | 60.21 | 2.0562 | 592751 | 0.0019 | 12 | 1.539E-4 | 26.717 | 24.046 |
| 2575 | 60.33 | 2.0579 | 592762 | 0.0019 | 12 | 1.537E-4 | 26.757 | 24.081 |
| 2575 | 60.46 | 2.0599 | 592774 | 0.0019 | 12 | 1.556E-4 | 26.796 | 24.117 |
| 2575 | 60.60 | 2.0618 | 592787 | 0.0019 | 12 | 1.585E-4 | 26.836 | 24.152 |
| 2575 | 60.73 | 2.0636 | 592799 | 0.0019 | 12 | 1.628E-4 | 26.878 | 24.191 |
| 2575 | 60.86 | 2.0655 | 592811 | 0.0020 | 12 | 1.674E-4 | 26.919 | 24.227 |
| 2575 | 61.01 | 2.0676 | 592822 | 0.0020 | 12 | 1.720E-4 | 26.962 | 24.265 |
| 2575 | 61.15 | 2.0696 | 592833 | 0.0020 | 12 | 1.755E-4 | 27.005 | 24.305 |
| 2575 | 61.30 | 2.0716 | 592845 | 0.0020 | 12 | 1.754E-4 | 27.049 | 24.344 |
| 2575 | 61.44 | 2.0737 | 592857 | 0.0020 | 12 | 1.719E-4 | 27.093 | 24.384 |
| 2575 | 61.59 | 2.0757 | 592868 | 0.0020 | 12 | 1.700E-4 | 27.136 | 24.422 |
| 2575 | 61.72 | 2.0776 | 592880 | 0.0020 | 12 | 1.703E-4 | 27.178 | 24.460 |
| 2575 | 61.86 | 2.0795 | 592891 | 0.0020 | 12 | 1.699E-4 | 27.221 | 24.499 |
| 2575 | 62.01 | 2.0815 | 592903 | 0.0020 | 12 | 1.690E-4 | 27.265 | 24.539 |
| 2575 | 62.16 | 2.0837 | 592916 | 0.0020 | 12 | 1.706E-4 | 27.309 | 24.578 |
| 2575 | 62.31 | 2.0856 | 592927 | 0.0020 | 12 | 1.714E-4 | 27.354 | 24.618 |
| 2575 | 62.44 | 2.0875 | 592938 | 0.0039 | 23 | 1.687E-4 | 27.397 | 24.657 |
| 2575 | 62.59 | 2.0895 | 592950 | 0.0042 | 24 | 1.738E-4 | 27.442 | 24.698 |
| | 62.75 | 2.0917 | 592962 | | | | | |

Automated Fatigue Crack
Growth Rate Analysis

| | | | |
|-----------------|----------------|---------------|------|
| Test ID | 5383-FCG-4pt05 | Geometry | C(T) |
| Contract | SSC 10624-01 | Orientation | T-L |
| Material | 5383-H116 | Yield (ksi) | 35.4 |
| Temperature (F) | 75 | Modulus (Msi) | 10.5 |
| Environment | RH = 40% | | |

Specimen Dimensions (in)

| | | | |
|---------------|-------|-------------|-------|
| Thickness | 0.486 | Height | 2.400 |
| Net Thickness | 0.486 | Notch Depth | 1.000 |
| Width | 4.002 | Gage Length | 0.500 |

Precrack Parameters

| | | | |
|--------------|-------|--------------------|------|
| Pmax (lbs) | 859.0 | Stress Ratio | 0.10 |
| Final a (in) | 1.050 | Kmax (ksi sqr[in]) | 4.50 |

Test Parameters

| EvBP | Freq | Pmax | R | Ai | Kmaxi | C | DKi |
|--------|------|------|------|-------|-------|------|------|
| 30.410 | 0.05 | 0 | 0.10 | 1.416 | 9.34 | 2.00 | 0.00 |
| 48.970 | 0.05 | 2575 | 0.10 | 0.000 | 0.00 | 0.00 | 0.00 |

| K Coeff | C Coeff |
|---------|----------|
| .886 | 1.00098 |
| 4.64 | -4.66951 |
| -13.32 | 18.4601 |
| 14.72 | -236.825 |
| -5.6 | 1214.88 |
| . | -2143.57 |

Visual Observations

| EvB/P | Crack(EvB/P) | Crack(visual) | Error | CAF |
|---------|--------------|---------------|--------|-------|
| 20.753 | 0.983 | 1.002 | 0.019 | 0.993 |
| 21.841 | 1.041 | 1.040 | -0.001 | 0.991 |
| 23.480 | 1.121 | 1.100 | -0.021 | 0.989 |
| 23.760 | 1.134 | 1.170 | 0.036 | 0.989 |
| 26.667 | 1.260 | 1.260 | 0.000 | 0.986 |
| 27.531 | 1.294 | 1.280 | -0.014 | 0.985 |
| 30.339 | 1.397 | 1.380 | -0.017 | 0.983 |
| 34.274 | 1.523 | 1.490 | -0.033 | 0.980 |
| 48.661 | 1.865 | 1.880 | 0.015 | 0.972 |
| 59.300 | 2.043 | 2.080 | 0.037 | 0.969 |
| 66.619 | 2.142 | 2.120 | -0.022 | 0.966 |
| 101.006 | 2.462 | 2.460 | -0.002 | 0.959 |

Comments

Date of test: 9/18/2006
Waveform Type Sine

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax (ksi[in]^0.5) | deltaK |
|--------------|-------|-----------|--------|------------|-------|-------------------|-----------------------|--------|
| | 32.28 | 1.4618 | 578265 | | | | | |
| 1541 | 32.34 | 1.4638 | 578397 | 0.0040 | 278 | 1.430E-5 | 10.553 | 9.498 |
| 1545 | 32.40 | 1.4658 | 578543 | 0.0042 | 298 | 1.397E-5 | 10.597 | 9.538 |
| 1550 | 32.47 | 1.4679 | 578695 | 0.0020 | 142 | 1.408E-5 | 10.640 | 9.576 |
| 1554 | 32.53 | 1.4699 | 578827 | 0.0020 | 142 | 1.396E-5 | 10.683 | 9.614 |
| 1558 | 32.59 | 1.4717 | 578965 | 0.0020 | 139 | 1.394E-5 | 10.726 | 9.653 |
| 1562 | 32.65 | 1.4737 | 579117 | 0.0019 | 138 | 1.401E-5 | 10.767 | 9.690 |
| 1566 | 32.72 | 1.4757 | 579249 | 0.0037 | 259 | 1.441E-5 | 10.809 | 9.728 |
| 1570 | 32.77 | 1.4775 | 579376 | 0.0038 | 275 | 1.391E-5 | 10.853 | 9.768 |
| 1575 | 32.84 | 1.4796 | 579524 | 0.6184 | 13601 | 4.547E-5 | 0.000 | 0.000 |
| 2574 | 63.06 | 2.0958 | 592977 | 0.6178 | 13461 | 4.590E-5 | 0.000 | 0.000 |
| 2575 | 63.17 | 2.0974 | 592985 | 0.0036 | 19 | 1.884E-4 | 27.617 | 24.858 |
| 2575 | 63.32 | 2.0994 | 592996 | 0.0041 | 22 | 1.875E-4 | 27.660 | 24.894 |
| 2575 | 63.48 | 2.1015 | 593007 | 0.0040 | 21 | 1.901E-4 | 27.705 | 24.934 |
| 2575 | 63.62 | 2.1034 | 593017 | 0.0020 | 10 | 1.989E-4 | 27.751 | 24.976 |
| 2575 | 63.77 | 2.1053 | 593026 | 0.0020 | 10 | 2.043E-4 | 27.795 | 25.015 |
| 2575 | 63.93 | 2.1074 | 593036 | 0.0020 | 10 | 2.094E-4 | 27.841 | 25.058 |
| 2575 | 64.08 | 2.1095 | 593046 | 0.0020 | 9 | 2.135E-4 | 27.887 | 25.099 |
| 2575 | 64.23 | 2.1115 | 593055 | 0.0020 | 10 | 2.117E-4 | 27.933 | 25.140 |
| 2575 | 64.38 | 2.1134 | 593064 | 0.0020 | 10 | 2.111E-4 | 27.978 | 25.181 |
| 2575 | 64.53 | 2.1154 | 593073 | 0.0020 | 9 | 2.114E-4 | 28.022 | 25.220 |
| 2575 | 64.68 | 2.1173 | 593083 | 0.0020 | 9 | 2.104E-4 | 28.069 | 25.262 |
| 2575 | 64.84 | 2.1194 | 593093 | 0.0020 | 9 | 2.134E-4 | 28.114 | 25.303 |
| 2575 | 65.00 | 2.1214 | 593102 | 0.0020 | 9 | 2.182E-4 | 28.160 | 25.345 |
| 2575 | 65.15 | 2.1234 | 593111 | 0.0020 | 9 | 2.262E-4 | 28.209 | 25.388 |
| 2575 | 65.31 | 2.1255 | 593120 | 0.0020 | 9 | 2.342E-4 | 28.253 | 25.428 |
| 2575 | 65.46 | 2.1274 | 593128 | 0.0020 | 8 | 2.396E-4 | 28.301 | 25.471 |
| 2575 | 65.61 | 2.1293 | 593136 | 0.0020 | 8 | 2.450E-4 | 28.347 | 25.512 |
| 2575 | 65.77 | 2.1314 | 593144 | 0.0020 | 8 | 2.514E-4 | 28.393 | 25.554 |
| 2575 | 65.93 | 2.1334 | 593152 | 0.0020 | 8 | 2.548E-4 | 28.440 | 25.596 |
| 2575 | 66.08 | 2.1354 | 593160 | 0.0020 | 8 | 2.579E-4 | 28.488 | 25.639 |
| 2575 | 66.25 | 2.1374 | 593167 | 0.0040 | 15 | 2.652E-4 | 28.534 | 25.680 |
| 2575 | 66.40 | 2.1393 | 593175 | 0.0039 | 15 | 2.572E-4 | 28.581 | 25.723 |
| | 66.55 | 2.1412 | 593182 | | | | | |

Automated Fatigue Crack
Growth Rate Analysis

| | | |
|-----------------|-------------------------|---------------|
| Test ID | 5383-FCG-4Cpt05Geometry | C(T) |
| Contract | SSC 10624-01 | Orientation |
| Material | 5383-H116 | Yield (ksi) |
| Temperature (F) | 75 | Modulus (Msi) |
| Environment | RH = 40% | |

Specimen Dimensions (in)

| | | | |
|---------------|-------|-------------|-------|
| Thickness | 0.486 | Height | 2.400 |
| Net Thickness | 0.486 | Notch Depth | 1.000 |
| Width | 4.002 | Gage Length | 0.500 |

Precrack Parameters

| | | | |
|--------------|-------|--------------------|------|
| Pmax (lbs) | 859.0 | Stress Ratio | 0.10 |
| Final a (in) | 1.050 | Kmax (ksi sqr[in]) | 4.50 |

Test Parameters

| | | | | | | | |
|--------|------|------|------|-------|-------|------|------|
| EvBP | Freq | Pmax | R | Ai | Kmaxi | C | DKi |
| 30.410 | 0.05 | 0 | 0.10 | 1.416 | 9.34 | 2.00 | 0.00 |

| | |
|---------|----------|
| K Coeff | C Coeff |
| .886 | 1.00098 |
| 4.64 | -4.66951 |
| -13.32 | 18.4601 |
| 14.72 | -236.825 |
| -5.6 | 1214.88 |
| . | -2143.57 |

Visual Observations

| EvB/P | Crack(EvB/P) | Crack(visual) | Error | CAF |
|---------|--------------|---------------|--------|-------|
| 20.753 | 0.983 | 1.002 | 0.019 | 0.993 |
| 21.841 | 1.041 | 1.040 | -0.001 | 0.991 |
| 23.480 | 1.121 | 1.100 | -0.021 | 0.989 |
| 23.760 | 1.134 | 1.170 | 0.036 | 0.989 |
| 26.667 | 1.260 | 1.260 | 0.000 | 0.986 |
| 27.531 | 1.294 | 1.280 | -0.014 | 0.985 |
| 30.339 | 1.397 | 1.380 | -0.017 | 0.983 |
| 34.274 | 1.523 | 1.490 | -0.033 | 0.980 |
| 48.661 | 1.865 | 1.880 | 0.015 | 0.972 |
| 59.300 | 2.043 | 2.080 | 0.037 | 0.969 |
| 66.619 | 2.142 | 2.120 | -0.022 | 0.966 |
| 101.006 | 2.462 | 2.460 | -0.002 | 0.959 |

Comments

Date of test: 9/18/2006
Waveform Type Sine

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in] ^{.5}) |
|--------------|-------|-----------|--------|------------|-----|-------------------|--------|------------------------------------|
| | 32.92 | 1.4821 | 579814 | | | | | |
| 1583 | 32.96 | 1.4835 | 579886 | 0.0032 | 165 | 1.936E-5 | 10.988 | 9.889 |
| 1587 | 33.02 | 1.4853 | 579979 | 0.0037 | 198 | 1.889E-5 | 11.025 | 9.922 |
| 1591 | 33.08 | 1.4872 | 580084 | 0.0019 | 96 | 1.980E-5 | 11.070 | 9.963 |
| 1596 | 33.16 | 1.4895 | 580197 | 0.0020 | 100 | 1.986E-5 | 11.114 | 10.003 |
| 1601 | 33.22 | 1.4915 | 580297 | 0.0020 | 100 | 2.006E-5 | 11.161 | 10.045 |
| 1605 | 33.28 | 1.4935 | 580388 | 0.0020 | 98 | 2.028E-5 | 11.205 | 10.085 |
| 1609 | 33.35 | 1.4954 | 580484 | 0.0019 | 95 | 2.040E-5 | 11.250 | 10.125 |
| 1614 | 33.41 | 1.4973 | 580580 | 0.0019 | 94 | 2.053E-5 | 11.293 | 10.164 |
| 1618 | 33.47 | 1.4992 | 580671 | 0.0019 | 94 | 2.059E-5 | 11.337 | 10.204 |
| 1622 | 33.53 | 1.5011 | 580767 | 0.0020 | 95 | 2.090E-5 | 11.381 | 10.243 |
| 1626 | 33.60 | 1.5031 | 580858 | 0.0020 | 94 | 2.110E-5 | 11.427 | 10.285 |
| 1631 | 33.66 | 1.5051 | 580954 | 0.0020 | 93 | 2.134E-5 | 11.474 | 10.327 |
| 1636 | 33.73 | 1.5072 | 581053 | 0.0020 | 92 | 2.145E-5 | 11.520 | 10.368 |
| 1640 | 33.80 | 1.5092 | 581141 | 0.0019 | 90 | 2.137E-5 | 11.568 | 10.411 |
| 1644 | 33.86 | 1.5111 | 581229 | 0.0019 | 90 | 2.142E-5 | 11.613 | 10.451 |
| 1649 | 33.92 | 1.5130 | 581320 | 0.0019 | 88 | 2.168E-5 | 11.656 | 10.490 |
| 1653 | 33.98 | 1.5147 | 581400 | 0.0037 | 171 | 2.155E-5 | 11.702 | 10.532 |
| 1657 | 34.05 | 1.5167 | 581491 | 0.0041 | 183 | 2.219E-5 | 11.747 | 10.572 |
| | 34.12 | 1.5188 | 581583 | | | | | |

Automated Fatigue Crack
Growth Rate Analysis

| | | | |
|-----------------|--------------|---------------|------|
| Test ID | 5383-FCG-5 | Geometry | C(T) |
| Contract | SSC 10624-01 | Orientation | T-L |
| Material | 5383-H116 | Yield (ksi) | 35.4 |
| Temperature (F) | 75 | Modulus (Msi) | 10.5 |
| Environment | RH = 40% | | |

Specimen Dimensions (in)

| | | | |
|---------------|-------|-------------|-------|
| Thickness | 0.485 | Height | 2.400 |
| Net Thickness | 0.485 | Notch Depth | 1.000 |
| Width | 4.000 | Gage Length | 0.500 |

Precrack Parameters

| | | | |
|--------------|-------|---------------------|------|
| Pmax (lbs) | 940.0 | Stress Ratio | 0.10 |
| Final a (in) | 1.070 | Kmax (ksi sqrt[in]) | 5.00 |

Test Parameters

| | | | | | | | |
|--------|-------|------|------|-------|-------|-------|------|
| EvBP | Freq | Pmax | R | Ai | Kmaxi | C | DKi |
| 22.287 | 24.00 | 0 | 0.10 | 1.070 | 5.00 | -4.00 | 0.00 |
| 27.215 | 24.00 | 0 | 0.10 | 1.295 | 3.80 | 4.00 | 0.00 |

| | | |
|---------|----------|------------------------------|
| K Coeff | C Coeff | da/dN Fit Parameters (DKapp) |
| .886 | 1.00098 | Upper da/dN limit |
| 4.64 | -4.66951 | Lower da/dN limit |
| -13.32 | 18.4601 | da/dN intercept (C) |
| 14.72 | -236.825 | da/dN slope (m) |
| -5.6 | 1214.88 | da/dN for delta K |
| . | -2143.57 | delta K |

Visual Observations

| | | | | |
|--------|--------------|---------------|--------|-------|
| EvB/P | Crack(EvB/P) | Crack(visual) | Error | CAF |
| 20.522 | 0.994 | 1.000 | 0.006 | 1.014 |
| 22.228 | 1.092 | 1.080 | -0.012 | 1.019 |
| 25.029 | 1.235 | 1.245 | 0.010 | 1.027 |
| 25.901 | 1.275 | 1.270 | -0.005 | 1.029 |
| 27.145 | 1.296 | 1.310 | 0.014 | 1.001 |
| 29.657 | 1.385 | 1.380 | -0.005 | 0.994 |
| 33.513 | 1.505 | 1.490 | -0.015 | 0.985 |
| 54.805 | 1.955 | 1.960 | 0.005 | 0.951 |

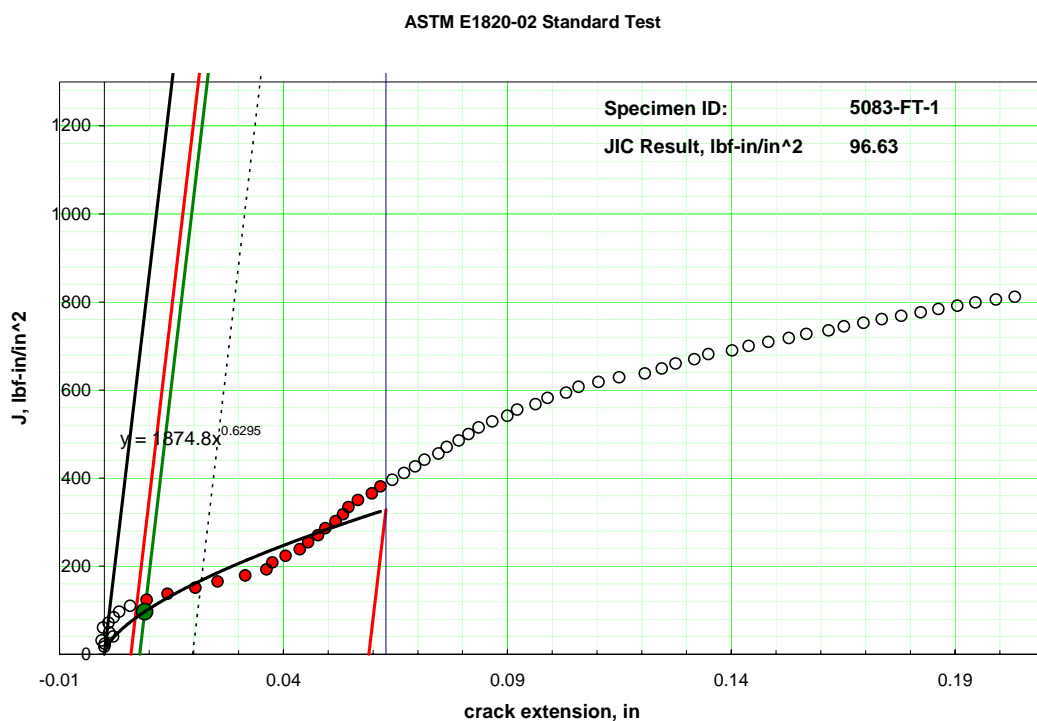
Comments

Date of test: 9/21/2006
Waveform Type Sine

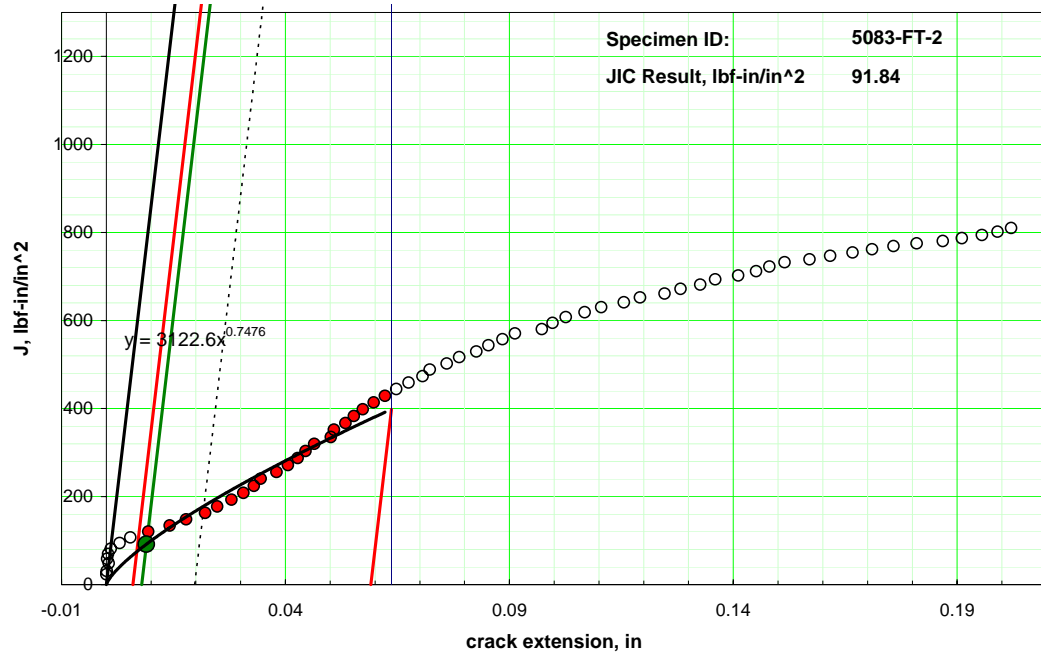
| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in]^0.5) |
|--------------|-------|-----------|---------|------------|--------|-------------------|-------|-------------------------|
| | 22.29 | 1.0954 | 7627 | | | | | |
| 907 | 22.38 | 1.1003 | 20207 | 0.0098 | 25134 | 3.918E-7 | 4.923 | 4.431 |
| 888 | 22.47 | 1.1053 | 32761 | 0.0104 | 27658 | 3.776E-7 | 4.827 | 4.344 |
| 866 | 22.57 | 1.1108 | 47865 | 0.0052 | 17462 | 3.359E-7 | 4.732 | 4.259 |
| 844 | 22.68 | 1.1164 | 70317 | 0.0053 | 19373 | 2.900E-7 | 4.639 | 4.175 |
| 826 | 22.77 | 1.1217 | 93159 | 0.0053 | 22485 | 2.547E-7 | 4.550 | 4.095 |
| 809 | 22.86 | 1.1264 | 112397 | 0.0054 | 24332 | 2.281E-7 | 4.459 | 4.013 |
| 789 | 22.97 | 1.1321 | 136443 | 0.0052 | 25439 | 2.167E-7 | 4.378 | 3.940 |
| 771 | 23.07 | 1.1374 | 167668 | 0.0053 | 27491 | 2.035E-7 | 4.288 | 3.859 |
| 753 | 23.18 | 1.1429 | 193854 | 0.0054 | 28528 | 1.872E-7 | 4.202 | 3.782 |
| 735 | 23.27 | 1.1479 | 222949 | 0.0051 | 29854 | 1.747E-7 | 4.123 | 3.711 |
| 719 | 23.38 | 1.1533 | 258105 | 0.0052 | 32813 | 1.711E-7 | 4.037 | 3.634 |
| 701 | 23.49 | 1.1590 | 283564 | 0.0053 | 34409 | 1.584E-7 | 3.966 | 3.570 |
| 688 | 23.56 | 1.1625 | 315568 | 0.0054 | 37136 | 1.520E-7 | 3.879 | 3.491 |
| 670 | 23.68 | 1.1688 | 364545 | 0.0053 | 40622 | 1.433E-7 | 3.816 | 3.434 |
| 657 | 23.79 | 1.1745 | 400307 | 0.0053 | 42944 | 1.265E-7 | 3.723 | 3.351 |
| 637 | 23.91 | 1.1803 | 445767 | 0.0056 | 43419 | 1.239E-7 | 3.665 | 3.299 |
| 626 | 24.00 | 1.1849 | 501834 | 0.0052 | 43590 | 1.183E-7 | 3.575 | 3.218 |
| 609 | 24.12 | 1.1909 | 541230 | 0.0052 | 51961 | 1.100E-7 | 3.518 | 3.167 |
| 597 | 24.22 | 1.1958 | 576081 | 0.0048 | 61192 | 1.086E-7 | 3.448 | 3.103 |
| 585 | 24.31 | 1.1999 | 626084 | 0.0047 | 68516 | 1.062E-7 | 3.382 | 3.043 |
| 570 | 24.42 | 1.2054 | 712071 | 0.0043 | 78963 | 6.965E-8 | 3.331 | 2.998 |
| 562 | 24.49 | 1.2090 | 812917 | 0.0038 | 89797 | 4.611E-8 | 3.269 | 2.942 |
| 551 | 24.58 | 1.2133 | 912927 | 0.0034 | 98106 | 3.498E-8 | 3.229 | 2.907 |
| 544 | 24.65 | 1.2164 | 1015005 | 0.0028 | 100417 | 2.787E-8 | 3.192 | 2.872 |
| 539 | 24.69 | 1.2184 | 1114861 | 0.0022 | 100253 | 2.165E-8 | 3.160 | 2.844 |
| 534 | 24.73 | 1.2206 | 1214718 | 0.0017 | 100227 | 1.596E-8 | 3.139 | 2.825 |
| 530 | 24.77 | 1.2221 | 1314575 | 0.0016 | 99857 | 1.421E-8 | 3.119 | 2.807 |
| 528 | 24.76 | 1.2220 | 1414432 | 0.0012 | 99857 | 1.218E-8 | 3.108 | 2.797 |
| 527 | 24.79 | 1.2233 | 1514289 | 0.0008 | 99857 | 9.415E-9 | 3.086 | 2.778 |
| 521 | 24.85 | 1.2259 | 1614145 | 0.0011 | 99857 | 1.040E-8 | 3.076 | 2.768 |
| 518 | 24.84 | 1.2258 | 1714002 | 0.0013 | 99857 | 1.221E-8 | 3.061 | 2.755 |
| 518 | 24.84 | 1.2256 | 1813859 | 0.0011 | 99857 | 1.127E-8 | 3.048 | 2.743 |
| 516 | 24.90 | 1.2286 | 1913716 | 0.0008 | 99857 | 9.714E-9 | 3.039 | 2.735 |
| 512 | 24.93 | 1.2300 | 2013572 | 0.0009 | 99857 | 9.823E-9 | 3.033 | 2.729 |
| 512 | 24.94 | 1.2302 | 2113429 | 0.0010 | 99857 | 8.605E-9 | 3.022 | 2.719 |
| 511 | 24.95 | 1.2306 | 2213285 | 0.0009 | 199713 | 4.674E-9 | 3.014 | 2.712 |
| 508 | 24.96 | 1.2311 | 2313142 | 0.0011 | 199714 | 5.453E-9 | 3.006 | 2.706 |
| | 24.97 | 1.2317 | 2412999 | | | | | |
| | 28.37 | 1.3404 | 388127 | | | | | |
| 736 | 28.51 | 1.3453 | 410668 | 0.0098 | 40963 | 2.402E-7 | 4.683 | 4.215 |
| 749 | 28.65 | 1.3503 | 429090 | 0.0092 | 32962 | 2.782E-7 | 4.778 | 4.300 |
| 761 | 28.77 | 1.3545 | 443630 | 0.0090 | 27722 | 3.252E-7 | 4.876 | 4.388 |
| 774 | 28.91 | 1.3593 | 456812 | 0.0046 | 11897 | 4.385E-7 | 4.968 | 4.471 |

| Pmax (lb) | EvB/P | a (in) | N | da (in) | dN | da/dN (in/cyc) | Kmax | deltaK (ksi[in]^0.5) |
|--------------|-------|-----------|--------|------------|------|-------------------|-------|-------------------------|
| 787 | 29.04 | 1.3638 | 466583 | 0.0045 | 9780 | 5.280E-7 | 5.069 | 4.562 |
| 801 | 29.18 | 1.3685 | 474898 | 0.0046 | 8203 | 6.367E-7 | 5.168 | 4.651 |
| 814 | 29.31 | 1.3730 | 482048 | 0.0046 | 6811 | 7.405E-7 | 5.271 | 4.744 |
| 828 | 29.45 | 1.3775 | 487768 | 0.0046 | 5835 | 8.459E-7 | 5.380 | 4.842 |
| 843 | 29.59 | 1.3824 | 492849 | 0.0045 | 5019 | 9.596E-7 | 5.485 | 4.936 |
| 857 | 29.72 | 1.3869 | 497680 | 0.0046 | 4369 | 1.092E-6 | 5.595 | 5.036 |
| 870 | 29.86 | 1.3914 | 501595 | 0.0046 | 3920 | 1.221E-6 | 5.704 | 5.134 |
| 885 | 29.99 | 1.3958 | 505010 | 0.0046 | 3507 | 1.360E-6 | 5.817 | 5.235 |
| 900 | 30.14 | 1.4005 | 508263 | 0.0045 | 3067 | 1.527E-6 | 5.933 | 5.339 |
| 916 | 30.28 | 1.4052 | 511289 | 0.0046 | 2779 | 1.717E-6 | 6.051 | 5.446 |
| 931 | 30.42 | 1.4098 | 513891 | 0.0047 | 2505 | 1.932E-6 | 6.171 | 5.554 |
| 946 | 30.55 | 1.4142 | 516079 | 0.0046 | 2237 | 2.157E-6 | 6.298 | 5.668 |
| 963 | 30.71 | 1.4192 | 518267 | 0.0047 | 1997 | 2.436E-6 | 6.417 | 5.775 |
| 979 | 30.85 | 1.4237 | 520038 | 0.0047 | 1775 | 2.722E-6 | 6.552 | 5.897 |
| 996 | 31.00 | 1.4283 | 521685 | 0.0047 | 1600 | 3.020E-6 | 6.683 | 6.015 |
| 1014 | 31.15 | 1.4333 | 523268 | 0.0046 | 1422 | 3.352E-6 | 6.819 | 6.137 |
| 1031 | 31.30 | 1.4379 | 524539 | 0.0046 | 1305 | 3.649E-6 | 6.954 | 6.258 |
| 1047 | 31.43 | 1.4421 | 525677 | 0.0046 | 1181 | 3.967E-6 | 7.094 | 6.385 |
| 1065 | 31.59 | 1.4468 | 526797 | 0.0045 | 1060 | 4.320E-6 | 7.230 | 6.507 |
| 1083 | 31.74 | 1.4515 | 527865 | 0.0046 | 990 | 4.688E-6 | 7.374 | 6.637 |
| 1101 | 31.88 | 1.4560 | 528772 | 0.0047 | 936 | 5.050E-6 | 7.520 | 6.768 |
| 1119 | 32.03 | 1.4605 | 529626 | 0.0046 | 865 | 5.422E-6 | 7.670 | 6.903 |
| 1138 | 32.19 | 1.4653 | 530480 | 0.0046 | 789 | 5.840E-6 | 7.825 | 7.043 |
| 1159 | 32.35 | 1.4702 | 531292 | 0.0046 | 743 | 6.301E-6 | 7.982 | 7.184 |
| 1178 | 32.50 | 1.4747 | 531987 | 0.0047 | 702 | 6.722E-6 | 8.140 | 7.326 |
| 1197 | 32.64 | 1.4790 | 532600 | 0.0046 | 651 | 7.166E-6 | 8.304 | 7.474 |
| 1218 | 32.80 | 1.4838 | 533231 | 0.0046 | 602 | 7.665E-6 | 8.464 | 7.618 |
| 1238 | 32.96 | 1.4884 | 533835 | 0.0046 | 568 | 8.176E-6 | 8.637 | 7.773 |
| 1259 | 33.12 | 1.4931 | 534384 | 0.0094 | 1070 | 8.762E-6 | 8.809 | 7.928 |
| 1280 | 33.28 | 1.4978 | 534905 | 0.0093 | 1009 | 9.253E-6 | 8.986 | 8.088 |
| | 33.44 | 1.5025 | 535393 | | | | | |

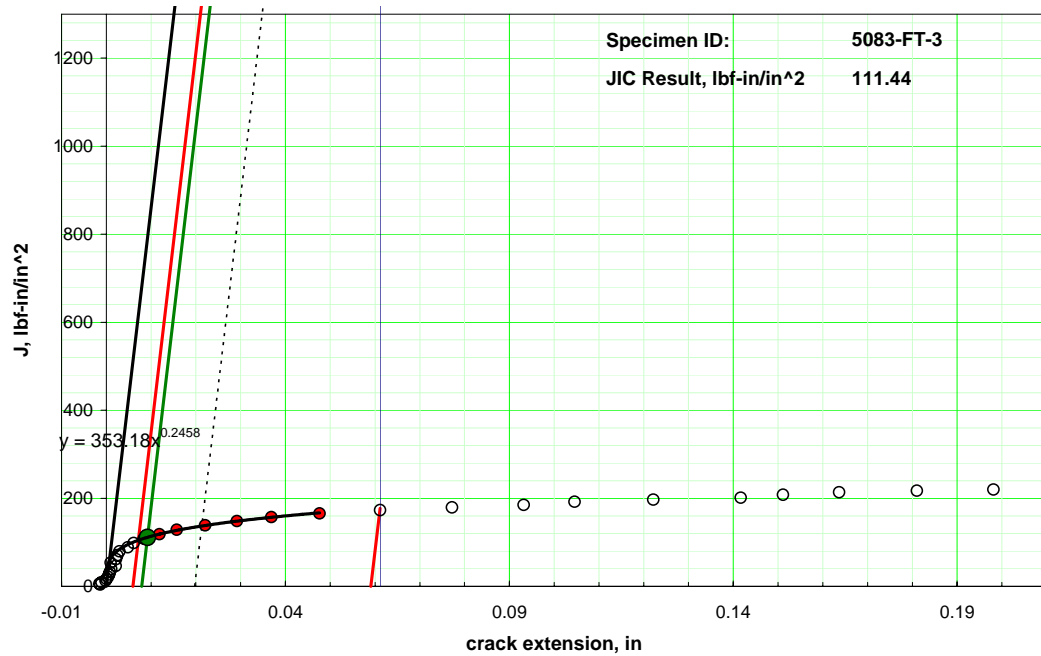
Annex F – Individual J vs. Δa Curves



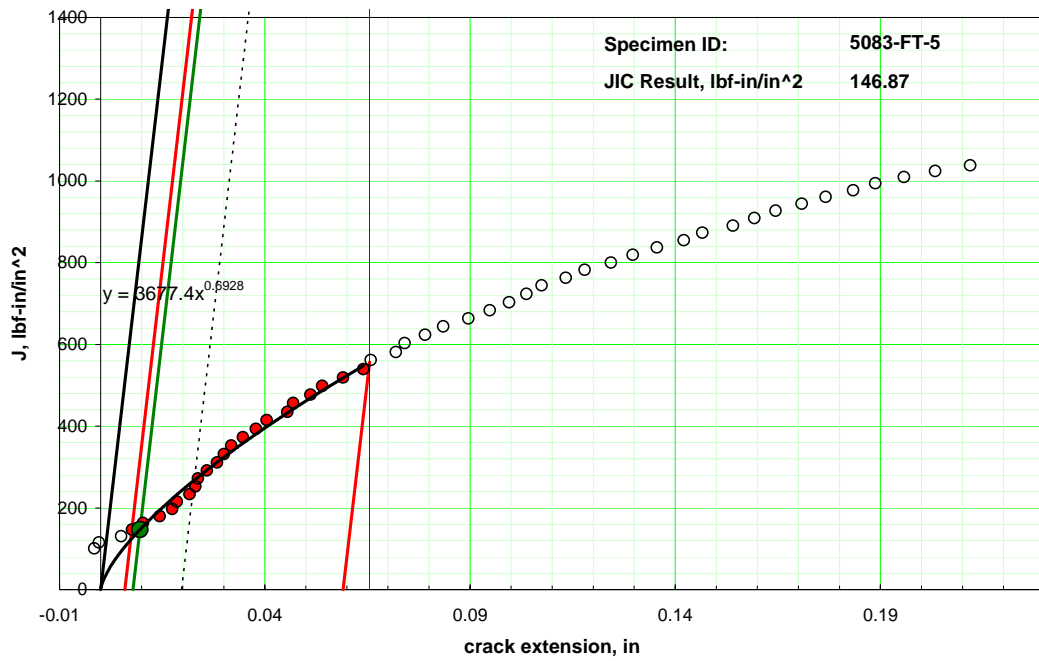
ASTM E1820-02 Standard Test



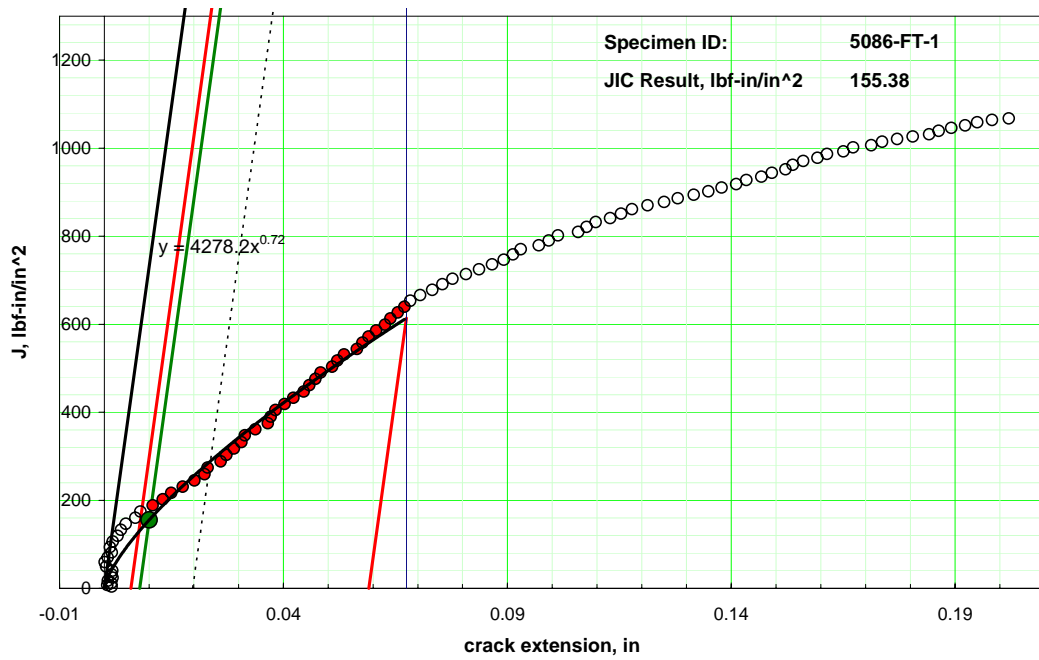
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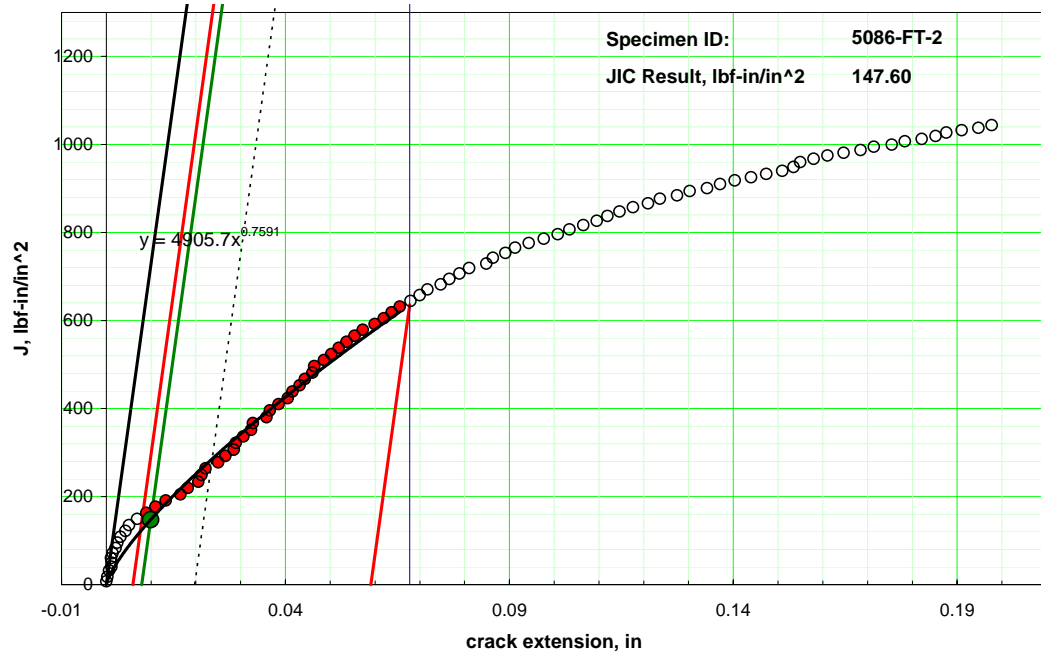
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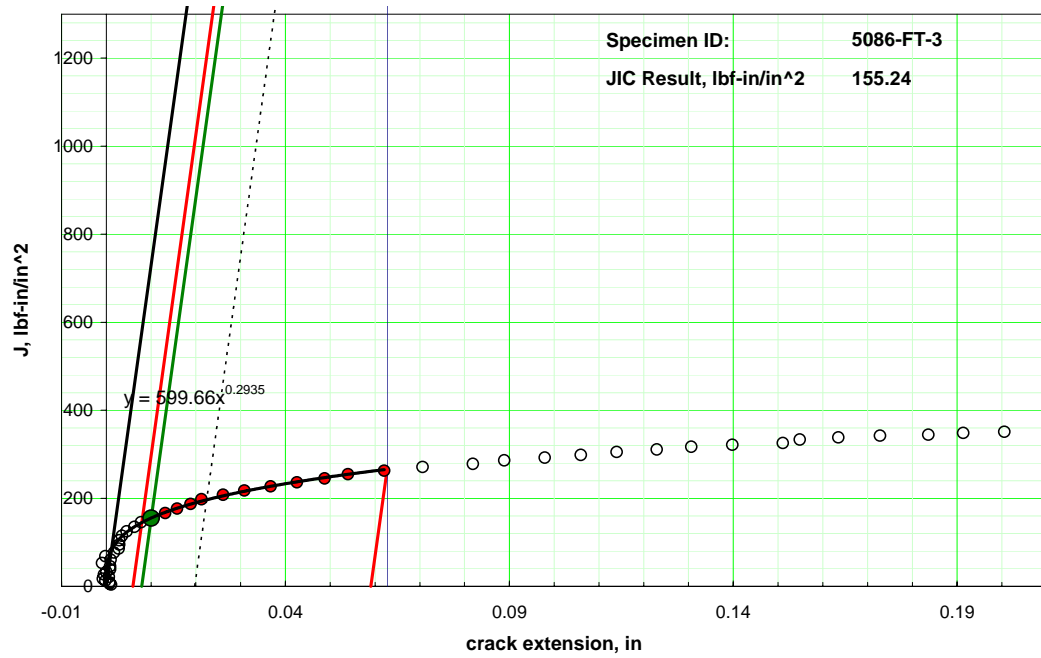
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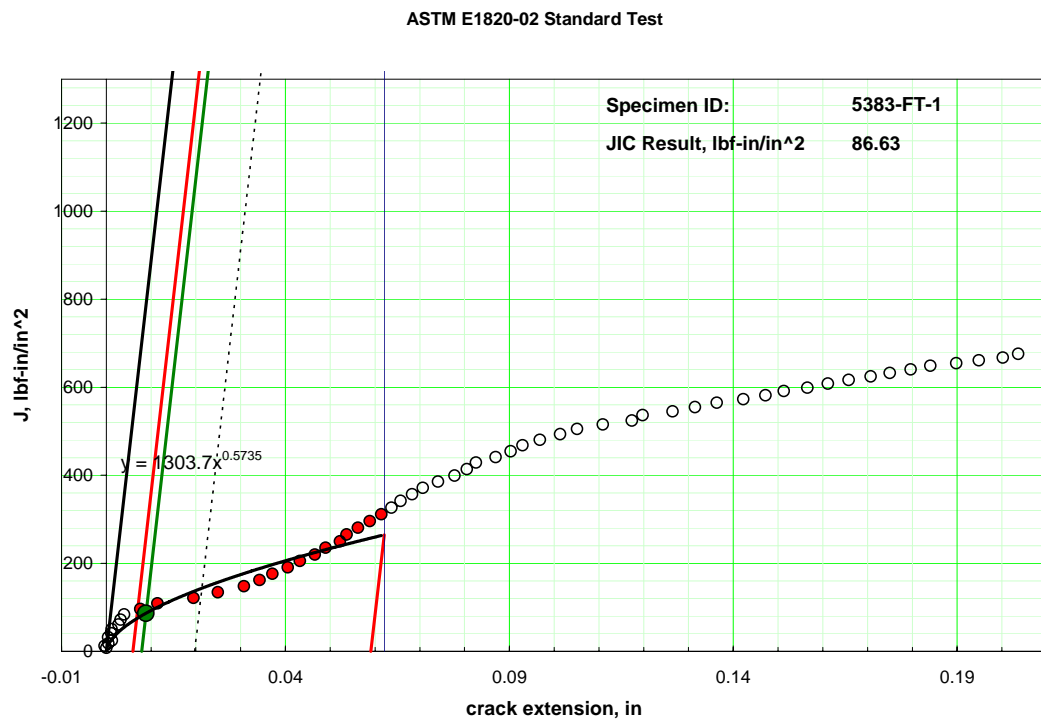
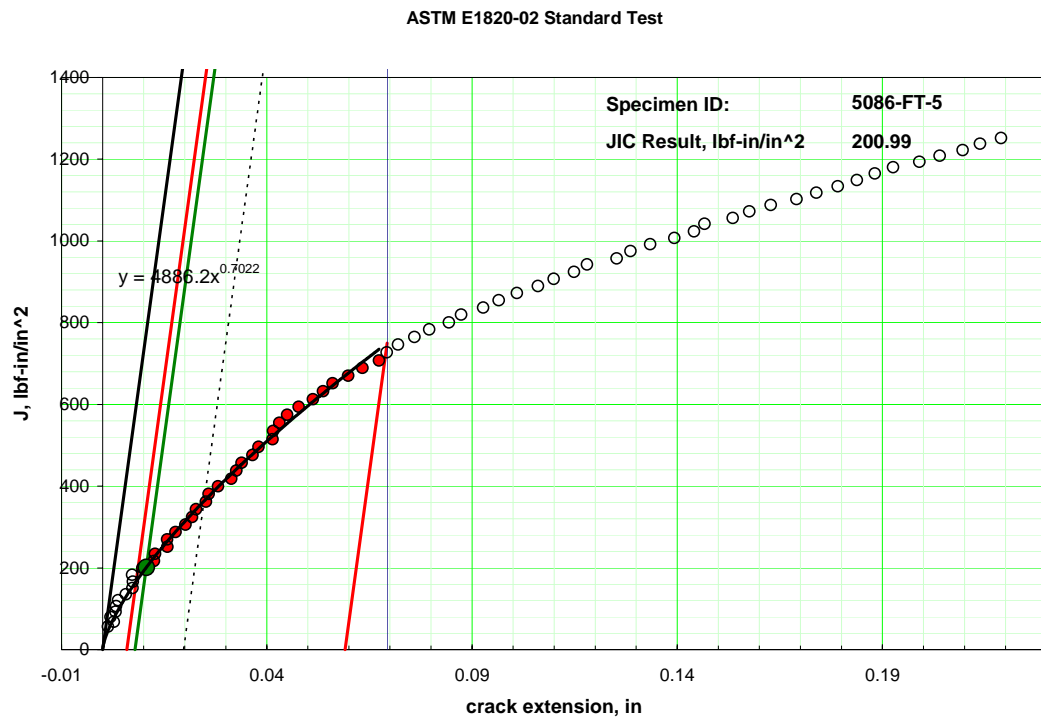


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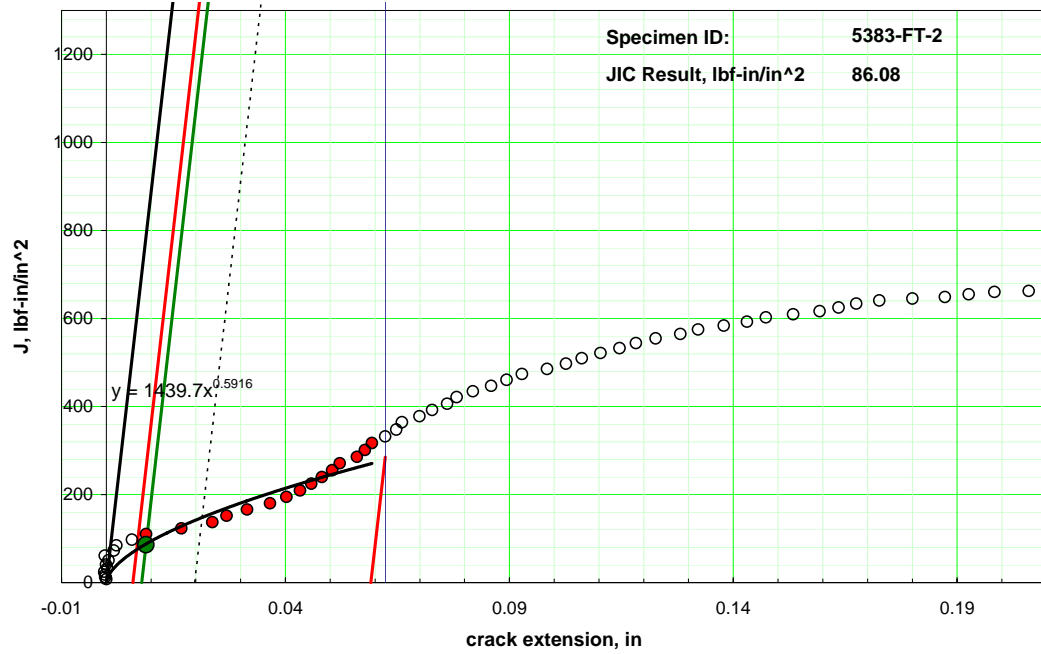


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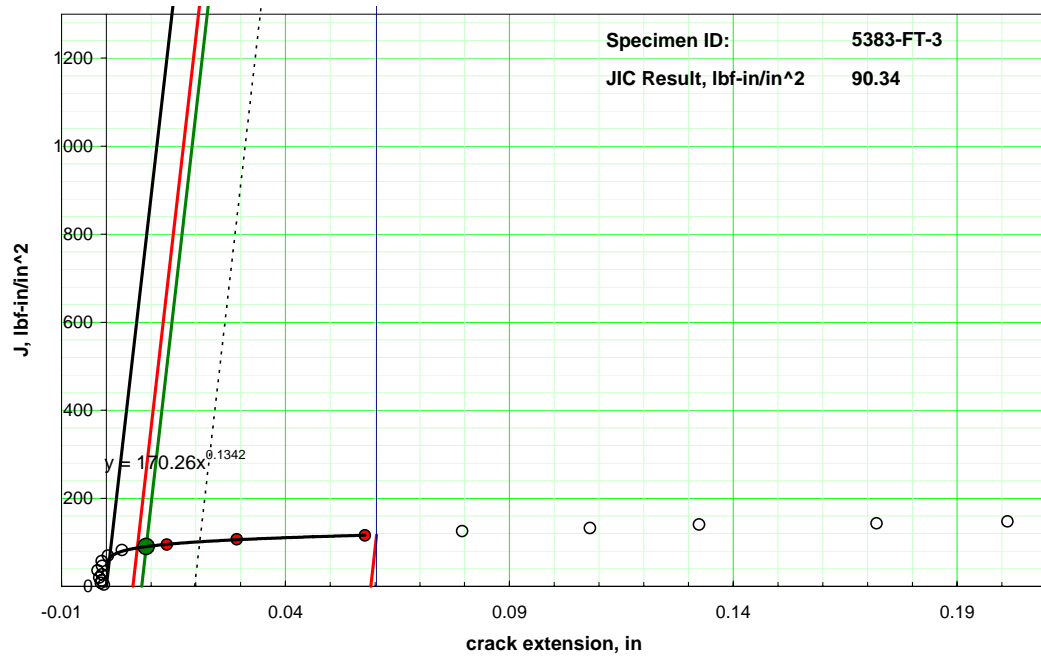




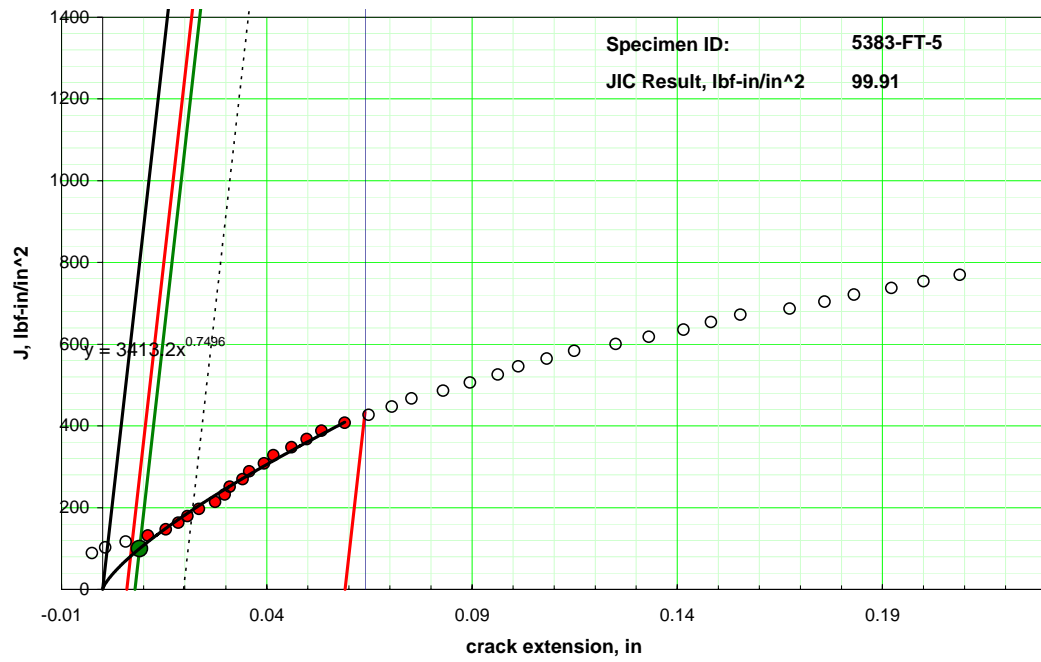
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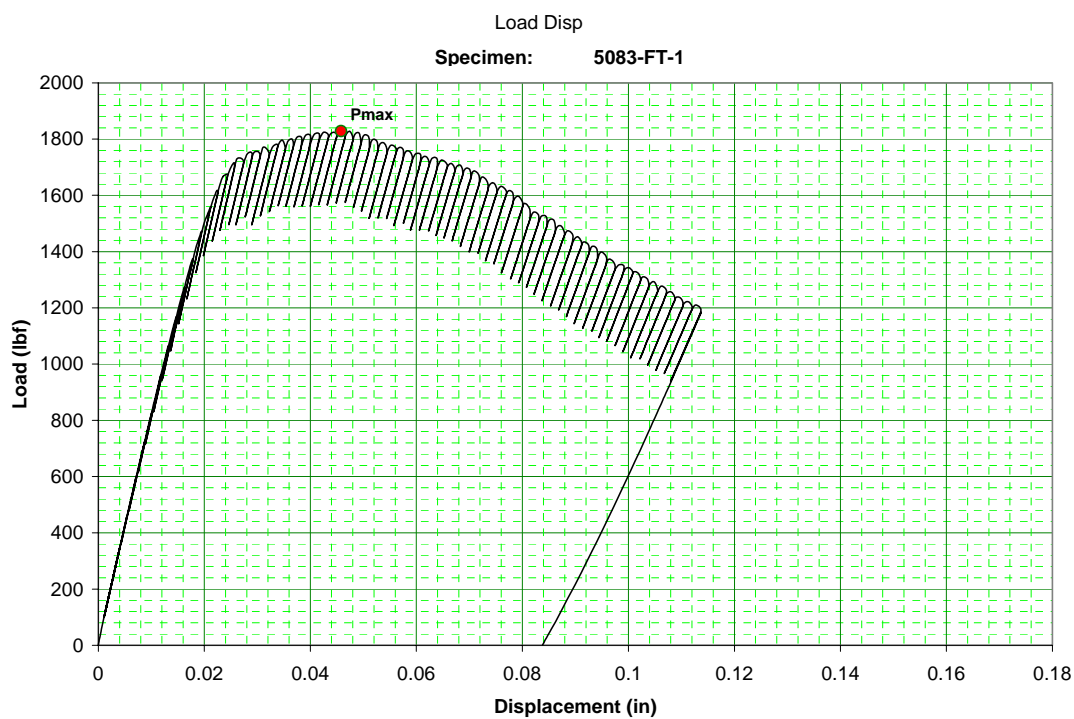
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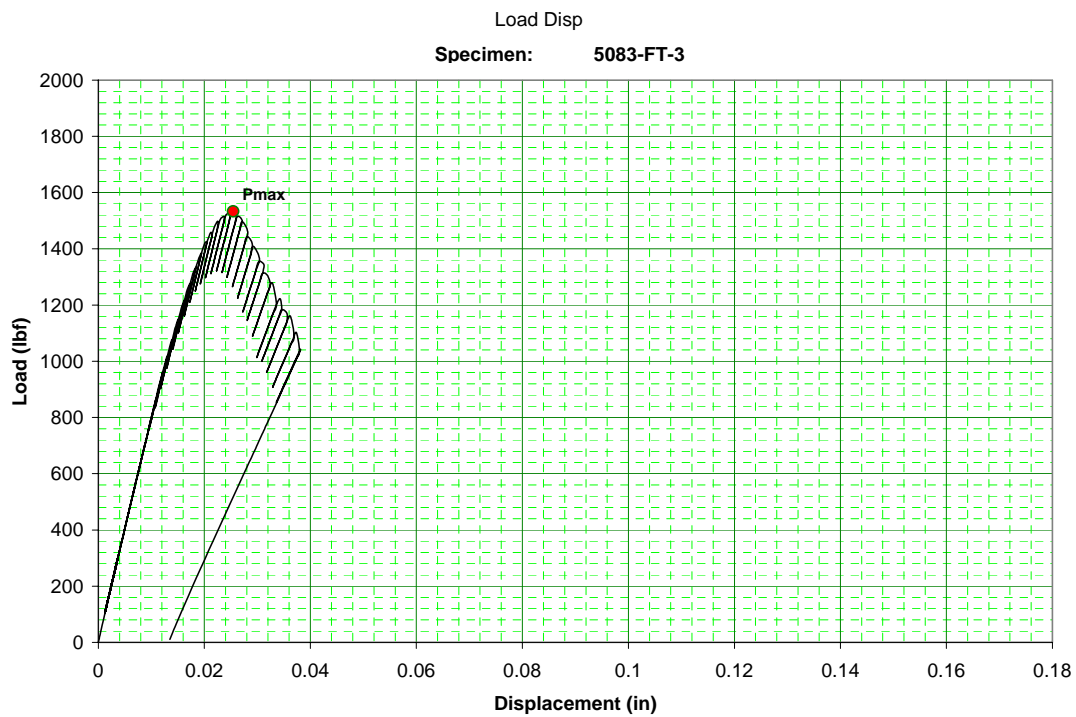
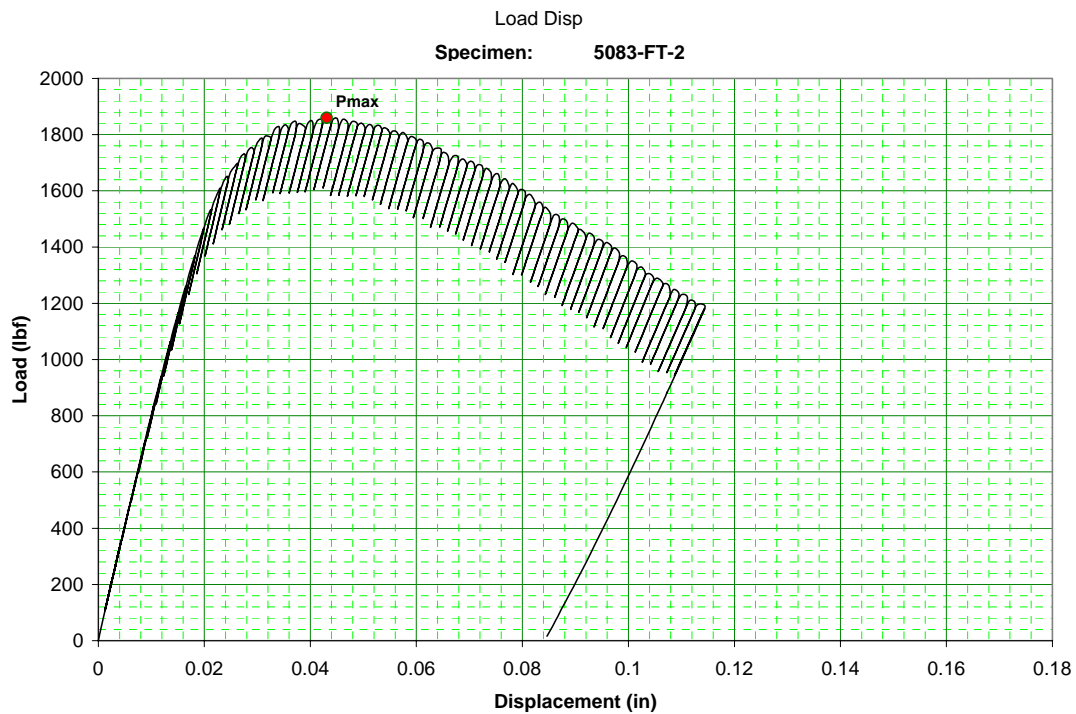


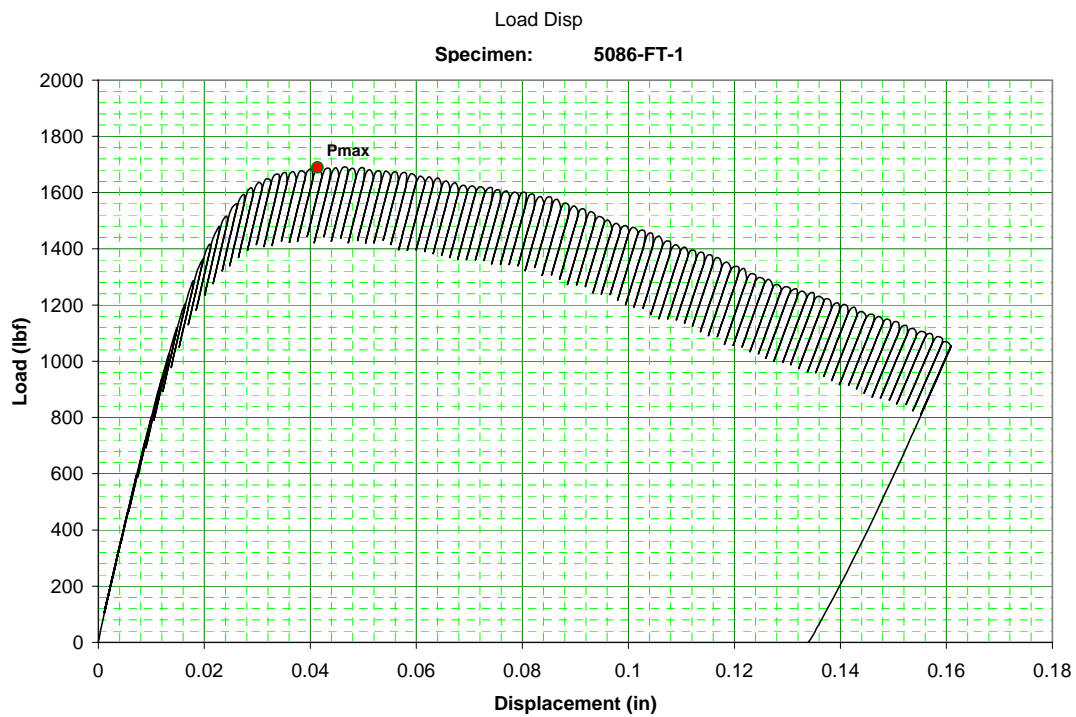
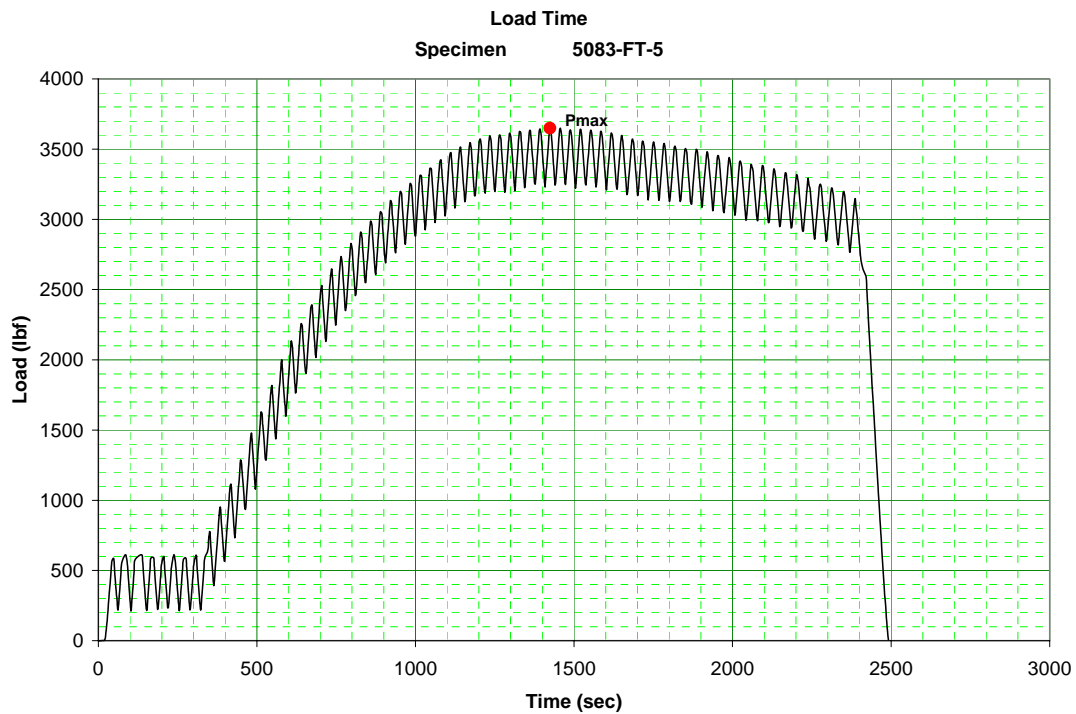
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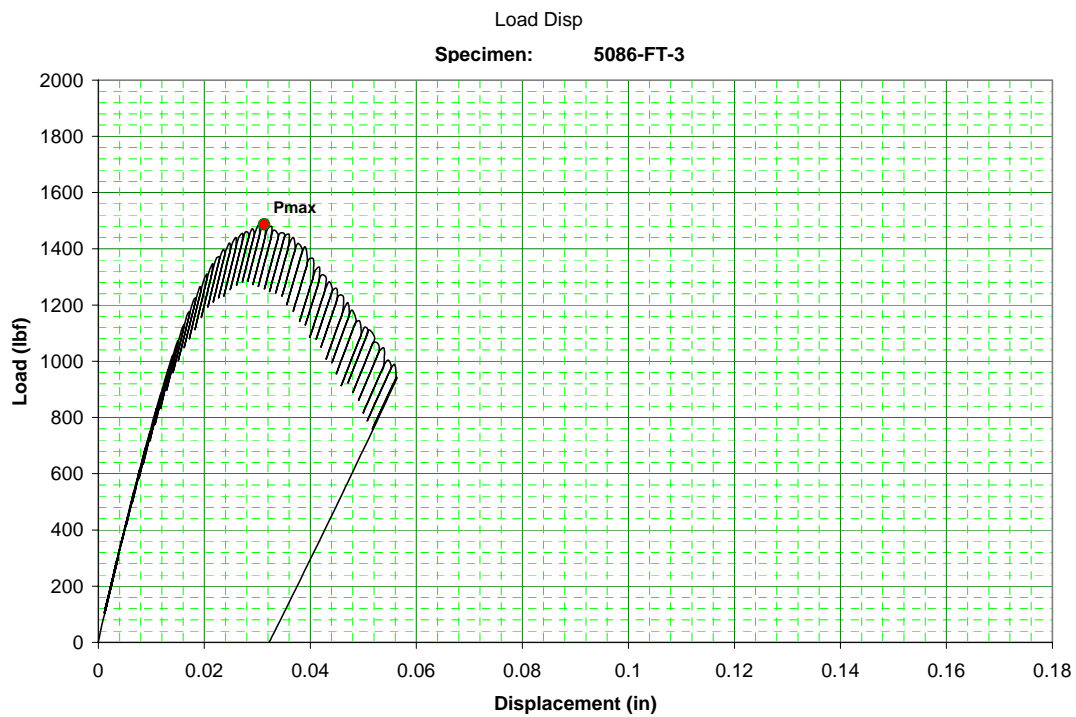
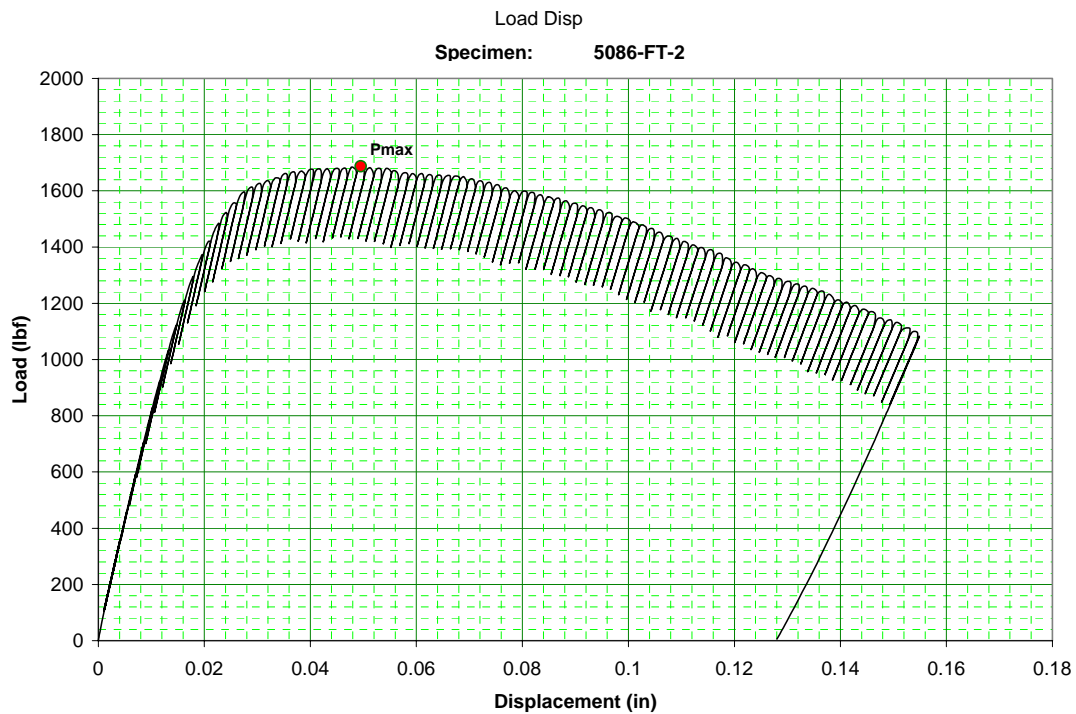


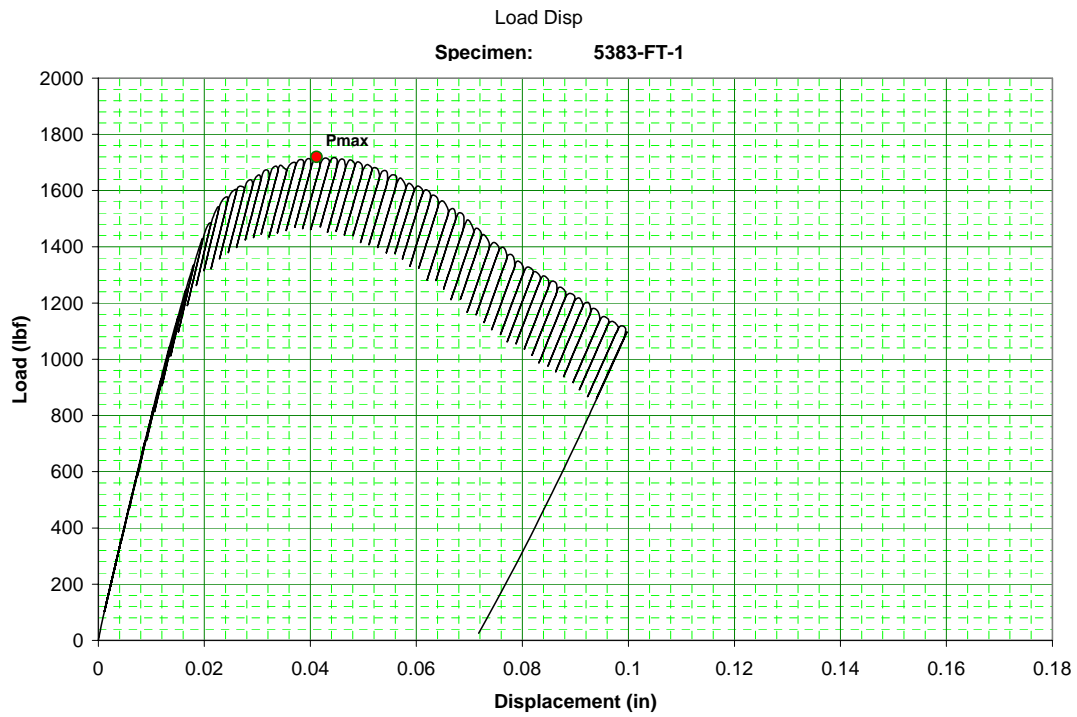
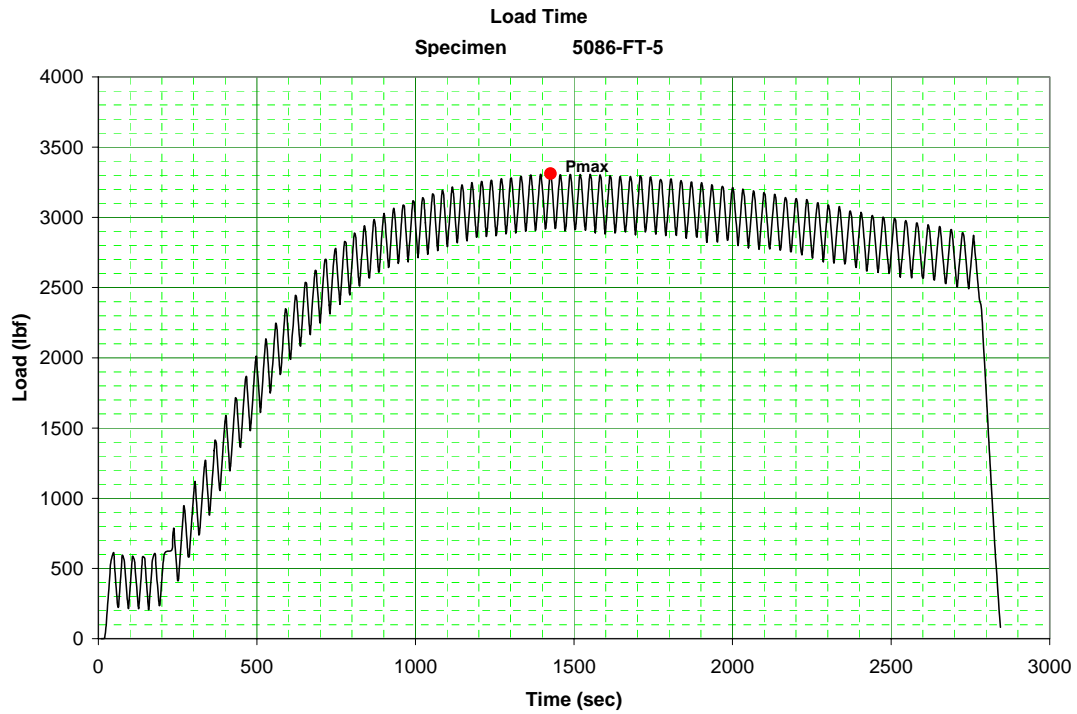
Annex G – Load vs. Load-Line Displacement Plots

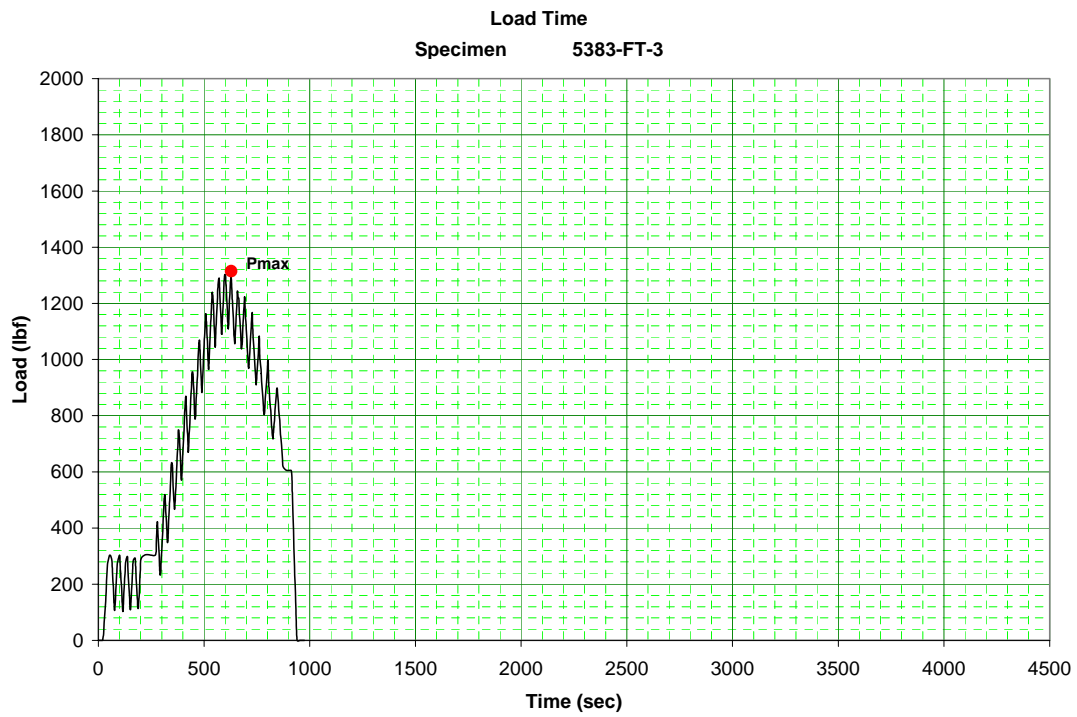
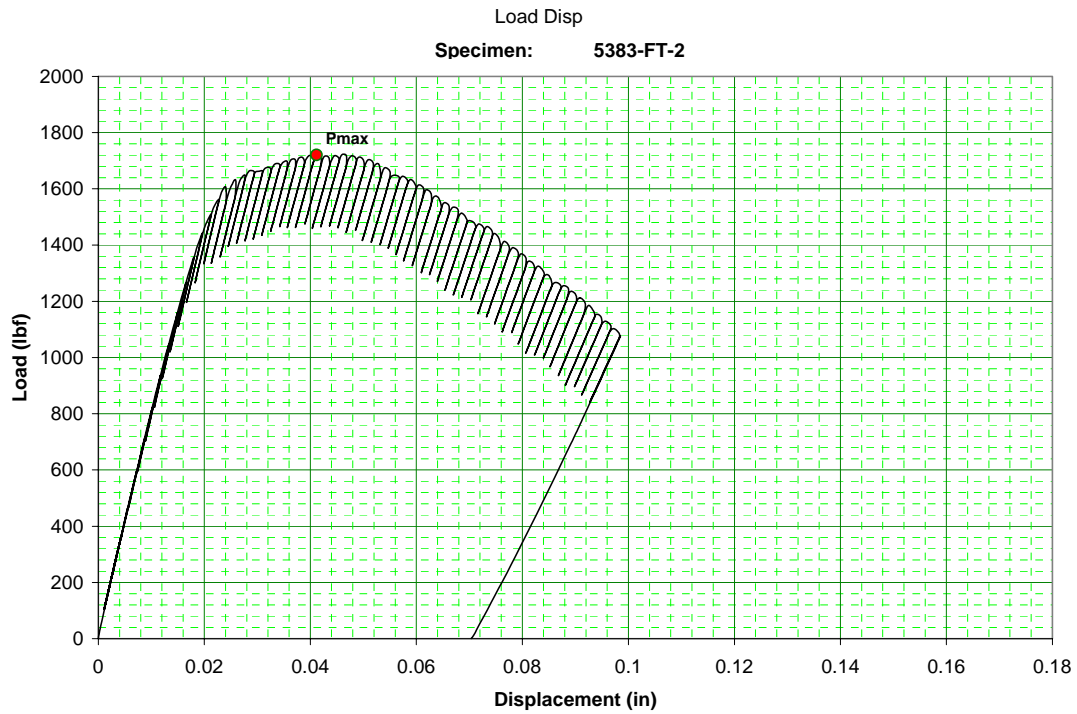


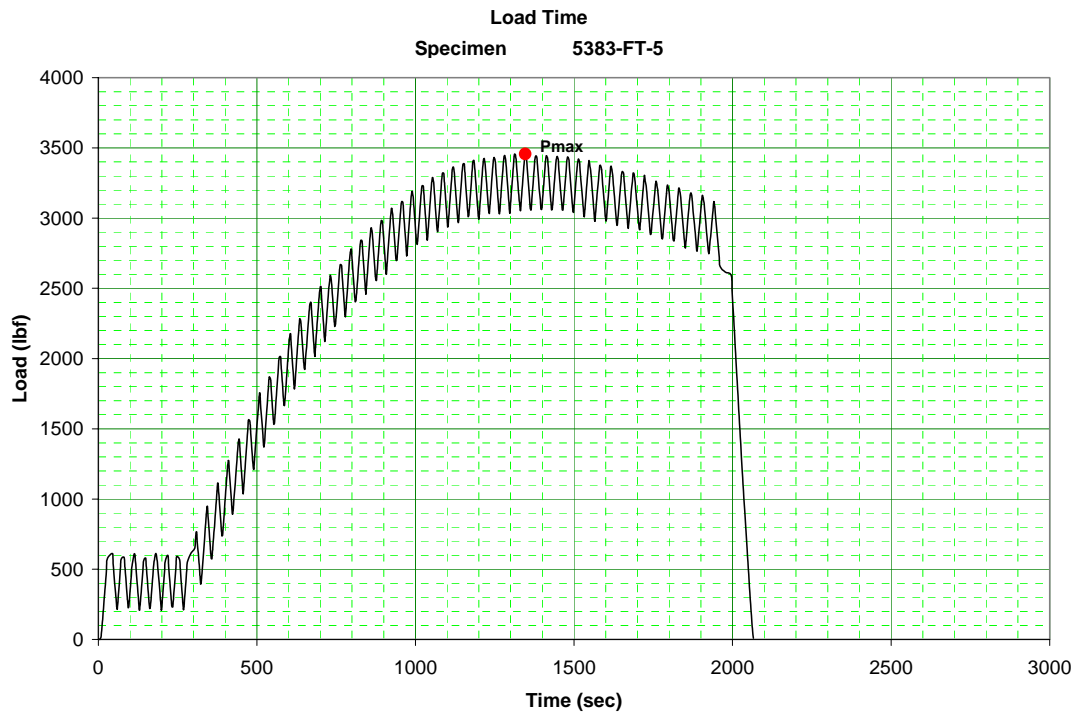












Annex H – Tabular Results – ASTM E1820 Analysis

Elastic-Plastic Fracture Toughness Analysis

| | | | | | | | | |
|--|-------------------|-------------------------|-------|---|-------|-------|-------|-------|
| Specimen ID | 5083-FT-1 | Geometry | C(T) | | | | | |
| Contract | SSC 10624-01 | Orientation | T-L | | | | | |
| Material | 5083-H321 | Yield (ksi) | 34.3 | | | | | |
| Temperature(F) | 75.0 | Tensile (ksi) | 51.8 | | | | | |
| Environment | LAB AIR | Modulus (Msi) | 10.5 | | | | | |
| <u>Specimen Dimensions</u> | | | | | | | | |
| Thickness (in) | 0.500 | Notch Depth (in) | 1.100 | | | | | |
| Net Thickness (in) | 0.500 | Gage Length (in) | 0.200 | | | | | |
| Width (in) | 2.000 | Alpha Ratio | 1 | | | | | |
| Pin Spacing (in) | 1.100 | | | | | | | |
| <u>Precrack Parameters</u> | | | | | | | | |
| Pmax (lbf) | 310.0 | Stress Ratio | 0.1 | | | | | |
| Final a (in) | 1.200 | Kmax (ksi sqrt (in)) | 6.0 | | | | | |
| Pf (lbf) | 1056 | | | | | | | |
| <u>Initial measured crack lengths (in)</u> | | | | | | | | |
| 1.182 | 1.195 | 1.199 | 1.200 | 1.205 | 1.208 | 1.209 | 1.206 | 1.196 |
| <u>Final measured crack lengths (in)</u> | | | | | | | | |
| 1.318 | 1.348 | 1.440 | 1.583 | 1.682 | 1.573 | 1.427 | 1.349 | 1.329 |
| x | x | | x | x | x | | x | x |
| Ave. initial crack length (in) | 1.201 | aoq (in) | n/a | | | | | |
| Ave. final crack length (in) | 1.466 | Compliance Adj. Factor | 1.014 | | | | | |
| Delta a measured (in) | 0.264 | Effective Modulus (Msi) | 10.6 | | | | | |
| Delta a predicted (in) | 0.203 | | | | | | | |
| <u>Results</u> | | | | | | | | |
| J _Q (E1820) | 96.6 lbf-in/in^2 | | | | | | | |
| K _{JIC} (E*JQ)^1/2 | 33.4 ksi sqrt(in) | | | | | | | |
| <u>Qualification of Data</u> | | | | <u>Qualification of J_Q as J_{IC}</u> | | | | |
| 7.4.2: precrack length | valid | | | A9.9.1; thickness | valid | | | |
| 9.1.4.1; precrack | valid | | | A9.9.2; ligament | valid | | | |
| 9.1.4.2; final crack | invalid | | | A9.9.3; slope | valid | | | |
| 9.1.5.1; Δa meas | valid | | | | | | | |
| 9.1.5.2; Δa pred | invalid | | | | | | | |
| A9.6.4; # of pnts in reg.A | valid | | | | | | | |
| A9.6.4; # of pnts in reg.B | valid | | | | | | | |
| A9.8.1; C ₂ <1 | valid | | | | | | | |
| A9.8.2.1; a _{0q} -a ₀ | #VALUE! | | | | | | | |
| A9.8.2.2; # of pnts for J _Q | valid | | | | | | | |
| A9.8.2.2; # of pnts < J _Q | valid | | | | | | | |
| A9.3.3.1; correlation | valid | | | | | | | |

| Index | Time | Force | Disp1 | Disp2 | Crack | Δa | CTOD | K561 | K1820 | KJ1820 | J1820 | Je | Jpl |
|-------|--------|--------|---------|---------|--------|---------|---------|-------------|-------------|-------------|--------|--------|--------|
| | Sec | lbf | inch | inch | inch | inch | inch | ksi sqr(in) | ksi sqr(in) | ksi sqr(in) | lbf/in | lbf/in | lbf/in |
| 8 | 391.1 | 727.8 | 0.00877 | 0.11444 | 1.2018 | 0.0000 | 0.00027 | 14.59 | 14.10 | 14.10 | 17.23 | 17.24 | -0.01 |
| 9 | 428.8 | 847.8 | 0.01032 | 0.13367 | 1.2018 | 0.0001 | 0.00038 | 17.21 | 16.43 | 16.60 | 23.87 | 23.40 | 0.47 |
| 10 | 465.8 | 965.4 | 0.01187 | 0.15198 | 1.2012 | -0.0006 | 0.00052 | 19.84 | 18.68 | 19.09 | 31.57 | 30.26 | 1.31 |
| 11 | 502.6 | 1078.9 | 0.01341 | 0.17029 | 1.2037 | 0.0020 | 0.00066 | 22.66 | 20.99 | 21.49 | 40.01 | 38.17 | 1.84 |
| 12 | 539 | 1187.1 | 0.01496 | 0.18707 | 1.2028 | 0.0011 | 0.00084 | 25.29 | 23.05 | 23.94 | 49.68 | 46.05 | 3.63 |
| 13 | 575.1 | 1291.3 | 0.01652 | 0.20325 | 1.2015 | -0.0003 | 0.00105 | 27.90 | 25.01 | 26.39 | 60.37 | 54.20 | 6.17 |
| 14 | 610.8 | 1390.5 | 0.01808 | 0.21820 | 1.2027 | 0.0009 | 0.00125 | 30.70 | 26.99 | 28.75 | 71.64 | 63.15 | 8.49 |
| 15 | 646.5 | 1480.1 | 0.01964 | 0.23193 | 1.2039 | 0.0021 | 0.00148 | 33.38 | 28.80 | 31.09 | 83.77 | 71.88 | 11.89 |
| 16 | 681.6 | 1559.9 | 0.02121 | 0.24536 | 1.2051 | 0.0033 | 0.00173 | 35.92 | 30.42 | 33.40 | 96.68 | 80.22 | 16.46 |
| 17 | 716.6 | 1631.3 | 0.02278 | 0.25726 | 1.2075 | 0.0057 | 0.00198 | 38.47 | 31.97 | 35.62 | 109.97 | 88.58 | 21.39 |
| 18 | 751.1 | 1673.0 | 0.02436 | 0.26306 | 1.2112 | 0.0095 | 0.00227 | 40.32 | 33.03 | 37.76 | 123.58 | 94.55 | 29.03 |
| 19 | 785.8 | 1723.0 | 0.02596 | 0.27039 | 1.2159 | 0.0141 | 0.00255 | 42.72 | 34.34 | 39.84 | 137.56 | 102.17 | 35.39 |
| 20 | 820.1 | 1729.1 | 0.02754 | 0.27283 | 1.2221 | 0.0203 | 0.00286 | 43.83 | 34.89 | 41.76 | 151.13 | 105.50 | 45.63 |
| 21 | 854.6 | 1745.0 | 0.02912 | 0.27344 | 1.2271 | 0.0253 | 0.00318 | 45.20 | 35.57 | 43.66 | 165.17 | 109.64 | 55.53 |
| 22 | 889.3 | 1754.2 | 0.03070 | 0.27496 | 1.2332 | 0.0315 | 0.00350 | 46.56 | 36.21 | 45.42 | 178.83 | 113.62 | 65.21 |
| 23 | 924 | 1747.4 | 0.03224 | 0.27466 | 1.2380 | 0.0362 | 0.00384 | 47.08 | 36.42 | 47.15 | 192.70 | 114.98 | 77.71 |
| 24 | 959.8 | 1778.4 | 0.03384 | 0.28015 | 1.2393 | 0.0375 | 0.00417 | 48.63 | 37.17 | 49.03 | 208.36 | 119.74 | 88.62 |
| 25 | 995 | 1779.0 | 0.03542 | 0.27985 | 1.2422 | 0.0405 | 0.00452 | 49.20 | 37.41 | 50.76 | 223.34 | 121.30 | 102.05 |
| 26 | 1030.6 | 1796.4 | 0.03703 | 0.28137 | 1.2454 | 0.0436 | 0.00487 | 50.58 | 38.03 | 52.47 | 238.64 | 125.33 | 113.31 |
| 27 | 1066.1 | 1802.4 | 0.03862 | 0.28351 | 1.2473 | 0.0455 | 0.00523 | 51.23 | 38.31 | 54.18 | 254.36 | 127.17 | 127.19 |
| 28 | 1101.6 | 1804.5 | 0.04022 | 0.28381 | 1.2495 | 0.0478 | 0.00560 | 51.78 | 38.53 | 55.83 | 270.18 | 128.66 | 141.52 |
| 29 | 1137.5 | 1811.5 | 0.04182 | 0.28656 | 1.2511 | 0.0494 | 0.00597 | 52.45 | 38.81 | 57.47 | 286.21 | 130.55 | 155.66 |
| 30 | 1173.2 | 1812.4 | 0.04343 | 0.28442 | 1.2534 | 0.0517 | 0.00634 | 52.98 | 39.02 | 59.03 | 302.04 | 131.94 | 170.10 |
| 31 | 1209.1 | 1817.9 | 0.04502 | 0.28534 | 1.2551 | 0.0533 | 0.00671 | 53.61 | 39.27 | 60.57 | 317.98 | 133.68 | 184.30 |
| 32 | 1245 | 1817.6 | 0.04662 | 0.28534 | 1.2563 | 0.0545 | 0.00709 | 53.86 | 39.37 | 62.12 | 334.46 | 134.34 | 200.12 |
| 33 | 1280.9 | 1815.8 | 0.04821 | 0.28473 | 1.2584 | 0.0567 | 0.00747 | 54.24 | 39.51 | 63.56 | 350.10 | 135.28 | 214.82 |
| 34 | 1317 | 1808.5 | 0.04982 | 0.28412 | 1.2615 | 0.0597 | 0.00786 | 54.56 | 39.61 | 64.93 | 365.34 | 135.96 | 229.38 |
| 35 | 1352.9 | 1791.4 | 0.05143 | 0.28076 | 1.2634 | 0.0617 | 0.00826 | 54.11 | 39.40 | 66.32 | 381.24 | 134.52 | 246.72 |
| 36 | 1389.1 | 1783.4 | 0.05303 | 0.27954 | 1.2661 | 0.0643 | 0.00865 | 54.30 | 39.45 | 67.63 | 396.36 | 134.86 | 261.50 |
| 37 | 1425.5 | 1768.8 | 0.05465 | 0.28046 | 1.2687 | 0.0669 | 0.00906 | 54.13 | 39.34 | 68.92 | 411.65 | 134.15 | 277.50 |
| 38 | 1462.2 | 1763.5 | 0.05624 | 0.27832 | 1.2712 | 0.0694 | 0.00945 | 54.42 | 39.44 | 70.16 | 426.59 | 134.78 | 291.81 |
| 39 | 1499.1 | 1757.2 | 0.05783 | 0.27527 | 1.2733 | 0.0715 | 0.00984 | 54.57 | 39.47 | 71.39 | 441.71 | 135.04 | 306.67 |
| 40 | 1536.1 | 1743.8 | 0.05942 | 0.27435 | 1.2764 | 0.0746 | 0.01024 | 54.58 | 39.44 | 72.53 | 455.93 | 134.82 | 321.11 |
| 41 | 1573.4 | 1735.7 | 0.06101 | 0.27313 | 1.2782 | 0.0765 | 0.01064 | 54.58 | 39.42 | 73.72 | 471.06 | 134.66 | 336.40 |
| 42 | 1610.5 | 1726.4 | 0.06261 | 0.27069 | 1.2809 | 0.0792 | 0.01105 | 54.70 | 39.44 | 74.85 | 485.49 | 134.80 | 350.69 |
| 43 | 1648.1 | 1717.8 | 0.06418 | 0.26978 | 1.2831 | 0.0813 | 0.01144 | 54.75 | 39.43 | 75.95 | 499.95 | 134.76 | 365.19 |
| 44 | 1685.9 | 1706.4 | 0.06582 | 0.26794 | 1.2854 | 0.0836 | 0.01187 | 54.66 | 39.37 | 77.09 | 515.03 | 134.30 | 380.73 |
| 45 | 1723.9 | 1699.7 | 0.06740 | 0.26825 | 1.2884 | 0.0866 | 0.01226 | 55.01 | 39.48 | 78.09 | 528.53 | 135.06 | 393.48 |
| 46 | 1761.9 | 1693.6 | 0.06897 | 0.26642 | 1.2918 | 0.0900 | 0.01266 | 55.49 | 39.63 | 79.05 | 541.53 | 136.12 | 405.41 |
| 47 | 1800.1 | 1685.3 | 0.07054 | 0.26581 | 1.2940 | 0.0922 | 0.01306 | 55.58 | 39.64 | 80.07 | 555.66 | 136.16 | 419.50 |
| 48 | 1838.6 | 1665.2 | 0.07215 | 0.26215 | 1.2981 | 0.0963 | 0.01350 | 55.43 | 39.52 | 80.96 | 568.13 | 135.39 | 432.74 |
| 49 | 1877.2 | 1642.0 | 0.07380 | 0.25818 | 1.3008 | 0.0990 | 0.01395 | 54.74 | 39.21 | 81.96 | 582.22 | 133.26 | 448.97 |
| 50 | 1916.6 | 1629.8 | 0.07541 | 0.25665 | 1.3049 | 0.1031 | 0.01437 | 55.06 | 39.29 | 82.79 | 594.09 | 133.79 | 460.31 |
| 51 | 1955.9 | 1612.6 | 0.07701 | 0.25391 | 1.3077 | 0.1059 | 0.01480 | 54.73 | 39.12 | 83.71 | 607.28 | 132.64 | 474.64 |
| 52 | 1995.4 | 1599.3 | 0.07861 | 0.25085 | 1.3121 | 0.1103 | 0.01523 | 55.06 | 39.20 | 84.47 | 618.33 | 133.16 | 485.17 |
| 53 | 2035.1 | 1573.2 | 0.08020 | 0.24811 | 1.3167 | 0.1150 | 0.01568 | 54.64 | 38.97 | 85.19 | 628.99 | 131.63 | 497.36 |
| 54 | 2074.9 | 1538.4 | 0.08178 | 0.24170 | 1.3225 | 0.1207 | 0.01615 | 53.98 | 38.63 | 85.78 | 637.70 | 129.31 | 508.39 |
| 55 | 2115.9 | 1525.3 | 0.08337 | 0.23956 | 1.3263 | 0.1245 | 0.01659 | 54.13 | 38.64 | 86.52 | 648.75 | 129.40 | 519.35 |
| 56 | 2157.1 | 1512.4 | 0.08494 | 0.23834 | 1.3293 | 0.1276 | 0.01702 | 54.11 | 38.59 | 87.29 | 660.37 | 129.10 | 531.27 |
| 57 | 2198.2 | 1492.0 | 0.08650 | 0.23529 | 1.3335 | 0.1317 | 0.01747 | 53.89 | 38.45 | 87.94 | 670.25 | 128.15 | 542.10 |
| 58 | 2239.9 | 1473.1 | 0.08810 | 0.23254 | 1.3367 | 0.1349 | 0.01793 | 53.50 | 38.25 | 88.69 | 681.67 | 126.82 | 554.84 |
| 59 | 2281.9 | 1447.1 | 0.08971 | 0.22858 | 1.3420 | 0.1402 | 0.01840 | 53.20 | 38.06 | 89.23 | 690.02 | 125.57 | 564.45 |
| 60 | 2324.6 | 1434.0 | 0.09129 | 0.22553 | 1.3457 | 0.1439 | 0.01885 | 53.30 | 38.06 | 89.88 | 700.06 | 125.53 | 574.53 |
| 61 | 2367.4 | 1416.6 | 0.09291 | 0.22339 | 1.3501 | 0.1483 | 0.01932 | 53.30 | 38.00 | 90.47 | 709.40 | 125.16 | 584.24 |
| 62 | 2410.6 | 1395.3 | 0.09454 | 0.22125 | 1.3547 | 0.1529 | 0.01980 | 53.08 | 37.85 | 91.04 | 718.24 | 124.19 | 594.05 |
| 63 | 2454.4 | 1374.7 | 0.09615 | 0.21790 | 1.3585 | 0.1568 | 0.02028 | 52.72 | 37.66 | 91.63 | 727.69 | 122.90 | 604.80 |

| Index | Time | Force | Disp1 | Disp2 | Crack | Δa | CTOD | K561 | K1820 | KJ1820 | J1820 | Je | Jpl |
|-------|--------|--------|---------|---------|--------|------------|---------|-------------|-------------|-------------|--------|--------|--------|
| | Sec | lbf | inch | inch | inch | inch | inch | ksi sqr(in) | ksi sqr(in) | ksi sqr(in) | lbf/in | lbf/in | lbf/in |
| 64 | 2498.6 | 1353.8 | 0.09775 | 0.21484 | 1.3635 | 0.1617 | 0.02077 | 52.60 | 37.55 | 92.11 | 735.33 | 122.17 | 613.15 |
| 65 | 2543.4 | 1342.6 | 0.09933 | 0.21210 | 1.3669 | 0.1652 | 0.02122 | 52.75 | 37.56 | 92.70 | 744.80 | 122.26 | 622.53 |
| 66 | 2588.6 | 1329.3 | 0.10091 | 0.21057 | 1.3713 | 0.1695 | 0.02168 | 52.99 | 37.60 | 93.19 | 752.65 | 122.53 | 630.12 |
| 67 | 2634.2 | 1310.0 | 0.10252 | 0.20843 | 1.3754 | 0.1736 | 0.02217 | 52.73 | 37.44 | 93.71 | 761.03 | 121.51 | 639.52 |
| 68 | 2679.9 | 1290.9 | 0.10410 | 0.20416 | 1.3797 | 0.1780 | 0.02266 | 52.54 | 37.31 | 94.17 | 768.63 | 120.65 | 647.98 |
| 69 | 2726.7 | 1273.5 | 0.10573 | 0.20111 | 1.3841 | 0.1823 | 0.02316 | 52.47 | 37.22 | 94.65 | 776.41 | 120.09 | 656.33 |
| 70 | 2773.9 | 1259.2 | 0.10732 | 0.19928 | 1.3881 | 0.1863 | 0.02364 | 52.52 | 37.19 | 95.12 | 784.15 | 119.86 | 664.29 |
| 71 | 2821.6 | 1239.0 | 0.10894 | 0.19714 | 1.3923 | 0.1905 | 0.02414 | 52.19 | 37.00 | 95.57 | 791.61 | 118.65 | 672.96 |
| 72 | 2869.7 | 1221.5 | 0.11055 | 0.19501 | 1.3963 | 0.1946 | 0.02465 | 51.99 | 36.87 | 96.02 | 799.14 | 117.79 | 681.34 |
| 73 | 2918.6 | 1205.8 | 0.11216 | 0.19165 | 1.4009 | 0.1991 | 0.02515 | 52.07 | 36.84 | 96.41 | 805.51 | 117.62 | 687.90 |
| 74 | 2967.7 | 1190.9 | 0.11374 | 0.18951 | 1.4051 | 0.2034 | 0.02564 | 52.12 | 36.80 | 96.79 | 811.95 | 117.37 | 694.58 |

Elastic-Plastic Fracture Toughness Analysis

| | | | |
|----------------|--------------|---------------|------|
| Specimen ID | 5083-FT-2 | Geometry | C(T) |
| Contract | SSC 10624-01 | Orientation | T-L |
| Material | 5083-H321 | Yield (ksi) | 34.3 |
| Temperature(F) | 75.0 | Tensile (ksi) | 51.8 |
| Environment | LAB AIR | Modulus (Msi) | 10.5 |

Specimen Dimensions

| | | | |
|--------------------|-------|------------------|-------|
| Thickness (in) | 0.500 | Notch Depth (in) | 1.100 |
| Net Thickness (in) | 0.500 | Gage Length (in) | 0.200 |
| Width (in) | 2.000 | Alpha Ratio | 1 |
| Pin Spacing (in) | 1.100 | | |

Precrack Parameters

| | | | |
|--------------|-------|----------------------|-----|
| Pmax (lbf) | 310.0 | Stress Ratio | 0.1 |
| Final a (in) | 1.200 | Kmax (ksi sqrt (in)) | 6.0 |
| Pf (lbf) | 1057 | | |

Initial measured crack lengths (in)

| | | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 1.160 | 1.176 | 1.187 | 1.195 | 1.205 | 1.214 | 1.221 | 1.223 | 1.214 |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|

Final measured crack lengths (in)

| | | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 1.296 | 1.335 | 1.427 | 1.570 | 1.652 | 1.562 | 1.433 | 1.365 | 1.354 |
| x | x | | x | x | x | | x | x |

| | | | |
|--------------------------------|-------|-------------------------|-------|
| Ave. initial crack length (in) | 1.201 | aoq (in) | n/a |
| Ave. final crack length (in) | 1.459 | Compliance Adj. Factor | 0.985 |
| Delta a measured (in) | 0.258 | Effective Modulus (Msi) | 10.3 |
| Delta a predicted (in) | 0.202 | | |

Results

| | |
|--|-----------------------------|
| J _a (E1820) | 91.8 lbf-in/in ² |
| K _{JIC} (E*JQ) ^{1/2} | 32.6 ksi sqrt(in) |

Qualification of Data

| | |
|---|---------|
| 7.4.2; precrack length | valid |
| 9.1.4.1; precrack | valid |
| 9.1.4.2; final crack | invalid |
| 9.1.5.1; Δa meas | valid |
| 9.1.5.2; Δa pred | invalid |
| A9.6.4; # of pnts in reg.A | valid |
| A9.6.4; # of pnts in reg.B | valid |
| A9.8.1; C ₂ <1 | valid |
| A9.8.2.1; a _{0a} -a ₀ | #VALUE! |
| A9.8.2.2; # of pnts for J _a | valid |
| A9.8.2.2; # of pnts < J _a | valid |
| A9.3.3.1; correlation | valid |

Qualification of J_a as J_{IC}

| | |
|-------------------|-------|
| A9.9.1; thickness | valid |
| A9.9.2; ligament | valid |
| A9.9.3; slope | valid |

| Index | Time | Force | Disp1 | Disp2 | Crack | Δa | CTOD | K561 | K1820 | KJ1820 | J1820 | Je | Jpl |
|-------|--------|--------|---------|---------|--------|--------|---------|-------------|-------------|-------------|--------|--------|--------|
| | Sec | lbf | inch | inch | inch | inch | inch | ksi sqr(in) | ksi sqr(in) | ksi sqr(in) | lbf/in | lbf/in | lbf/in |
| 9 | 419.3 | 846.7 | 0.01060 | 0.13367 | 1.2015 | 0.0000 | 0.00039 | 17.17 | 16.40 | 16.39 | 23.29 | 23.31 | -0.03 |
| 10 | 456.3 | 961.8 | 0.01217 | 0.15167 | 1.2016 | 0.0001 | 0.00052 | 19.78 | 18.63 | 18.85 | 30.78 | 30.09 | 0.69 |
| 12 | 529.1 | 1180.7 | 0.01529 | 0.18616 | 1.2020 | 0.0005 | 0.00084 | 25.08 | 22.90 | 23.67 | 48.57 | 45.43 | 3.14 |
| 13 | 565.1 | 1282.8 | 0.01684 | 0.20142 | 1.2017 | 0.0002 | 0.00103 | 27.70 | 24.86 | 26.05 | 58.81 | 53.55 | 5.26 |
| 14 | 600.8 | 1379.2 | 0.01840 | 0.21729 | 1.2019 | 0.0004 | 0.00124 | 30.32 | 26.74 | 28.40 | 69.91 | 61.95 | 7.96 |
| 15 | 636.1 | 1470.5 | 0.01999 | 0.23163 | 1.2025 | 0.0010 | 0.00147 | 32.97 | 28.54 | 30.74 | 81.89 | 70.59 | 11.30 |
| 16 | 671.3 | 1547.7 | 0.02156 | 0.24322 | 1.2045 | 0.0030 | 0.00171 | 35.48 | 30.16 | 33.00 | 94.37 | 78.81 | 15.56 |
| 17 | 706 | 1611.2 | 0.02314 | 0.25421 | 1.2069 | 0.0054 | 0.00197 | 37.75 | 31.54 | 35.21 | 107.43 | 86.21 | 21.22 |
| 18 | 740.3 | 1657.3 | 0.02472 | 0.26062 | 1.2109 | 0.0094 | 0.00224 | 39.75 | 32.70 | 37.30 | 120.61 | 92.68 | 27.93 |
| 19 | 775 | 1697.8 | 0.02632 | 0.26642 | 1.2157 | 0.0142 | 0.00253 | 41.78 | 33.82 | 39.35 | 134.17 | 99.15 | 35.02 |
| 20 | 809.5 | 1731.3 | 0.02792 | 0.27252 | 1.2193 | 0.0178 | 0.00283 | 43.52 | 34.74 | 41.37 | 148.33 | 104.62 | 43.71 |
| 21 | 843.8 | 1754.8 | 0.02954 | 0.27557 | 1.2236 | 0.0221 | 0.00314 | 45.04 | 35.52 | 43.34 | 162.80 | 109.33 | 53.47 |
| 22 | 878.6 | 1785.3 | 0.03114 | 0.28046 | 1.2263 | 0.0248 | 0.00346 | 46.69 | 36.34 | 45.28 | 177.71 | 114.42 | 63.29 |
| 23 | 913.3 | 1801.0 | 0.03275 | 0.28320 | 1.2294 | 0.0279 | 0.00380 | 47.87 | 36.89 | 47.18 | 192.95 | 117.96 | 74.99 |
| 24 | 948.1 | 1817.8 | 0.03439 | 0.28778 | 1.2321 | 0.0306 | 0.00415 | 49.04 | 37.44 | 49.07 | 208.71 | 121.48 | 87.23 |
| 25 | 982.8 | 1827.6 | 0.03599 | 0.28839 | 1.2344 | 0.0329 | 0.00450 | 49.90 | 37.82 | 50.88 | 224.38 | 123.97 | 100.40 |
| 26 | 1017.8 | 1839.3 | 0.03762 | 0.28931 | 1.2360 | 0.0345 | 0.00486 | 50.71 | 38.19 | 52.70 | 240.66 | 126.38 | 114.28 |
| 27 | 1052.5 | 1831.1 | 0.03920 | 0.28992 | 1.2395 | 0.0380 | 0.00522 | 51.02 | 38.29 | 54.33 | 255.79 | 127.07 | 128.71 |
| 28 | 1087.6 | 1836.2 | 0.04081 | 0.28900 | 1.2421 | 0.0406 | 0.00558 | 51.76 | 38.60 | 55.96 | 271.44 | 129.16 | 142.28 |
| 29 | 1123 | 1846.9 | 0.04242 | 0.29144 | 1.2442 | 0.0427 | 0.00594 | 52.71 | 39.01 | 57.59 | 287.41 | 131.87 | 155.54 |
| 30 | 1158.2 | 1852.0 | 0.04403 | 0.29083 | 1.2460 | 0.0445 | 0.00631 | 53.32 | 39.25 | 59.19 | 303.66 | 133.55 | 170.11 |
| 31 | 1193.6 | 1848.8 | 0.04565 | 0.29175 | 1.2479 | 0.0464 | 0.00670 | 53.58 | 39.35 | 60.77 | 320.03 | 134.18 | 185.85 |
| 32 | 1228.9 | 1832.4 | 0.04728 | 0.28839 | 1.2516 | 0.0501 | 0.00709 | 53.57 | 39.30 | 62.20 | 335.34 | 133.88 | 201.46 |
| 33 | 1264.6 | 1836.2 | 0.04887 | 0.28992 | 1.2523 | 0.0508 | 0.00747 | 53.92 | 39.45 | 63.72 | 351.85 | 134.85 | 217.00 |
| 34 | 1300.1 | 1826.3 | 0.05043 | 0.28686 | 1.2549 | 0.0534 | 0.00785 | 53.99 | 39.45 | 65.08 | 367.01 | 134.85 | 232.16 |
| 35 | 1336 | 1826.9 | 0.05204 | 0.28748 | 1.2568 | 0.0553 | 0.00823 | 54.43 | 39.61 | 66.47 | 382.97 | 136.00 | 246.96 |
| 36 | 1372 | 1825.6 | 0.05363 | 0.28717 | 1.2588 | 0.0573 | 0.00861 | 54.82 | 39.75 | 67.82 | 398.64 | 136.97 | 261.67 |
| 37 | 1407.7 | 1811.2 | 0.05522 | 0.28534 | 1.2612 | 0.0597 | 0.00900 | 54.64 | 39.65 | 69.12 | 414.00 | 136.24 | 277.76 |
| 38 | 1444.1 | 1802.2 | 0.05682 | 0.28259 | 1.2638 | 0.0623 | 0.00940 | 54.75 | 39.67 | 70.37 | 429.12 | 136.36 | 292.76 |
| 39 | 1480.4 | 1787.1 | 0.05844 | 0.28107 | 1.2662 | 0.0647 | 0.00980 | 54.53 | 39.54 | 71.61 | 444.45 | 135.53 | 308.93 |
| 40 | 1516.7 | 1776.9 | 0.06002 | 0.28015 | 1.2690 | 0.0675 | 0.01020 | 54.63 | 39.55 | 72.77 | 459.00 | 135.58 | 323.42 |
| 41 | 1553.6 | 1768.7 | 0.06162 | 0.27832 | 1.2721 | 0.0706 | 0.01059 | 54.92 | 39.64 | 73.90 | 473.31 | 136.18 | 337.13 |
| 42 | 1590.5 | 1755.7 | 0.06320 | 0.27740 | 1.2737 | 0.0722 | 0.01100 | 54.60 | 39.48 | 75.09 | 488.73 | 135.12 | 353.61 |
| 43 | 1627.4 | 1735.7 | 0.06481 | 0.27283 | 1.2775 | 0.0760 | 0.01141 | 54.41 | 39.36 | 76.12 | 502.21 | 134.26 | 367.95 |
| 44 | 1664.7 | 1718.8 | 0.06645 | 0.27039 | 1.2803 | 0.0788 | 0.01184 | 54.14 | 39.21 | 77.22 | 516.81 | 133.26 | 383.55 |
| 45 | 1702.4 | 1708.1 | 0.06806 | 0.26917 | 1.2841 | 0.0826 | 0.01225 | 54.46 | 39.30 | 78.19 | 529.85 | 133.86 | 395.99 |
| 46 | 1740.1 | 1699.4 | 0.06965 | 0.26703 | 1.2868 | 0.0853 | 0.01265 | 54.62 | 39.34 | 79.21 | 543.71 | 134.10 | 409.61 |
| 47 | 1778.2 | 1692.5 | 0.07127 | 0.26703 | 1.2900 | 0.0885 | 0.01306 | 54.99 | 39.45 | 80.19 | 557.29 | 134.89 | 422.40 |
| 48 | 1816.2 | 1676.5 | 0.07284 | 0.26367 | 1.2928 | 0.0913 | 0.01348 | 54.76 | 39.32 | 81.15 | 570.71 | 134.01 | 436.70 |
| 49 | 1854.7 | 1656.2 | 0.07443 | 0.26215 | 1.2988 | 0.0973 | 0.01390 | 55.07 | 39.38 | 81.85 | 580.61 | 134.37 | 446.25 |
| 50 | 1893.5 | 1636.8 | 0.07604 | 0.25757 | 1.3012 | 0.0997 | 0.01434 | 54.54 | 39.13 | 82.83 | 594.61 | 132.67 | 461.93 |
| 51 | 1932.6 | 1621.1 | 0.07766 | 0.25574 | 1.3041 | 0.1026 | 0.01478 | 54.35 | 39.01 | 83.74 | 607.74 | 131.89 | 475.85 |
| 52 | 1971.9 | 1601.6 | 0.07926 | 0.25146 | 1.3083 | 0.1068 | 0.01522 | 54.24 | 38.92 | 84.52 | 619.07 | 131.25 | 487.82 |
| 53 | 2011.6 | 1589.1 | 0.08083 | 0.24994 | 1.3120 | 0.1105 | 0.01564 | 54.41 | 38.94 | 85.29 | 630.46 | 131.42 | 499.04 |
| 54 | 2051.4 | 1554.6 | 0.08252 | 0.24567 | 1.3171 | 0.1156 | 0.01613 | 53.61 | 38.55 | 86.02 | 641.33 | 128.76 | 512.57 |
| 55 | 2092.1 | 1544.7 | 0.08409 | 0.24445 | 1.3207 | 0.1192 | 0.01656 | 53.91 | 38.62 | 86.76 | 652.40 | 129.29 | 523.11 |
| 56 | 2132.4 | 1510.6 | 0.08570 | 0.23865 | 1.3262 | 0.1247 | 0.01704 | 53.20 | 38.26 | 87.36 | 661.38 | 126.88 | 534.49 |
| 57 | 2173.7 | 1500.4 | 0.08727 | 0.23590 | 1.3297 | 0.1282 | 0.01747 | 53.45 | 38.32 | 88.06 | 672.08 | 127.29 | 544.79 |
| 58 | 2215.2 | 1480.1 | 0.08886 | 0.23346 | 1.3342 | 0.1327 | 0.01792 | 53.30 | 38.21 | 88.69 | 681.73 | 126.51 | 555.22 |
| 59 | 2257.4 | 1461.6 | 0.09053 | 0.23071 | 1.3375 | 0.1360 | 0.01840 | 52.98 | 38.03 | 89.45 | 693.41 | 125.36 | 568.05 |
| 60 | 2299.7 | 1442.9 | 0.09219 | 0.22797 | 1.3426 | 0.1411 | 0.01888 | 53.09 | 38.01 | 90.02 | 702.31 | 125.22 | 577.08 |
| 61 | 2342.5 | 1426.1 | 0.09380 | 0.22614 | 1.3466 | 0.1451 | 0.01934 | 53.02 | 37.94 | 90.64 | 712.00 | 124.73 | 587.27 |
| 62 | 2385.7 | 1413.0 | 0.09536 | 0.22339 | 1.3496 | 0.1481 | 0.01979 | 52.93 | 37.86 | 91.31 | 722.58 | 124.23 | 598.36 |
| 63 | 2428.9 | 1395.0 | 0.09691 | 0.22156 | 1.3530 | 0.1515 | 0.02025 | 52.62 | 37.69 | 91.93 | 732.35 | 123.12 | 609.24 |
| 64 | 2472.7 | 1367.7 | 0.09851 | 0.21667 | 1.3586 | 0.1571 | 0.02074 | 52.25 | 37.47 | 92.35 | 739.07 | 121.67 | 617.41 |
| 65 | 2517.1 | 1350.6 | 0.10008 | 0.21362 | 1.3631 | 0.1616 | 0.02121 | 52.29 | 37.42 | 92.83 | 746.81 | 121.38 | 625.43 |

| Index | Time | Force | Disp1 | Disp2 | Crack | Δa | CTOD | K561 | K1820 | KJ1820 | J1820 | Je | Jpl |
|-------|--------|--------|---------|---------|--------|------------|---------|------------------------|------------------------|------------------------|--------|--------|--------|
| | Sec | lbf | inch | inch | inch | inch | inch | ksi $\sqrt{\text{in}}$ | ksi $\sqrt{\text{in}}$ | ksi $\sqrt{\text{in}}$ | lbf/in | lbf/in | lbf/in |
| 66 | 2562.1 | 1328.0 | 0.10175 | 0.21271 | 1.3681 | 0.1666 | 0.02172 | 52.05 | 37.26 | 93.31 | 754.51 | 120.35 | 634.16 |
| 67 | 2607.4 | 1308.8 | 0.10331 | 0.20752 | 1.3725 | 0.1710 | 0.02220 | 51.87 | 37.14 | 93.77 | 761.99 | 119.52 | 642.48 |
| 68 | 2653.4 | 1292.9 | 0.10490 | 0.20538 | 1.3773 | 0.1758 | 0.02268 | 52.02 | 37.13 | 94.19 | 768.90 | 119.50 | 649.40 |
| 69 | 2699.9 | 1268.8 | 0.10653 | 0.20142 | 1.3825 | 0.1810 | 0.02319 | 51.69 | 36.93 | 94.58 | 775.29 | 118.20 | 657.08 |
| 70 | 2747.2 | 1242.7 | 0.10818 | 0.19867 | 1.3883 | 0.1868 | 0.02373 | 51.36 | 36.72 | 94.90 | 780.59 | 116.88 | 663.71 |
| 71 | 2795.1 | 1231.4 | 0.10975 | 0.19562 | 1.3926 | 0.1911 | 0.02420 | 51.68 | 36.80 | 95.32 | 787.38 | 117.36 | 670.02 |
| 72 | 2843.2 | 1208.9 | 0.11136 | 0.19257 | 1.3971 | 0.1956 | 0.02472 | 51.24 | 36.56 | 95.72 | 794.05 | 115.85 | 678.21 |
| 73 | 2892.6 | 1198.4 | 0.11293 | 0.19073 | 1.4005 | 0.1990 | 0.02519 | 51.40 | 36.58 | 96.19 | 801.81 | 115.96 | 685.85 |
| 74 | 2942.2 | 1190.9 | 0.11448 | 0.18982 | 1.4036 | 0.2021 | 0.02564 | 51.67 | 36.65 | 96.68 | 810.04 | 116.39 | 693.66 |

Elastic-Plastic Fracture Toughness Analysis

| | | | |
|----------------|--------------|---------------|------|
| Specimen ID | 5083-FT-3 | Geometry | C(T) |
| Contract | SSC 10624-01 | Orientation | T-L |
| Material | 5083-H321 | Yield (ksi) | 34.3 |
| Temperature(F) | 75.0 | Tensile (ksi) | 51.8 |
| Environment | LAB AIR | Modulus (Msi) | 10.5 |

Specimen Dimensions

| | | | |
|--------------------|-------|------------------|-------|
| Thickness (in) | 0.500 | Notch Depth (in) | 1.100 |
| Net Thickness (in) | 0.395 | Gage Length (in) | 0.200 |
| Width (in) | 2.000 | Alpha Ratio | 1 |
| Pin Spacing (in) | 1.100 | | |

Precrack Parameters

| | | | |
|--------------|-------|----------------------|-----|
| Pmax (lbf) | 310.9 | Stress Ratio | 0.1 |
| Final a (in) | 1.200 | Kmax (ksi sqrt (in)) | 6.0 |
| Pf (lbf) | 1053 | | |

Initial measured crack lengths (in)

| | | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 1.211 | 1.213 | 1.211 | 1.207 | 1.204 | 1.199 | 1.197 | 1.192 | 1.186 |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|

Final measured crack lengths (in)

| | | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 1.422 | 1.423 | 1.429 | 1.421 | 1.416 | 1.414 | 1.398 | 1.395 | 1.397 |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|

| | | | |
|--------------------------------|-------|-------------------------|-------|
| Ave. initial crack length (in) | 1.203 | aoq (in) | 1.204 |
| Ave. final crack length (in) | 1.413 | Compliance Adj. Factor | 1.019 |
| Delta a measured (in) | 0.210 | Effective Modulus (Msi) | 10.7 |
| Delta a predicted (in) | 0.199 | | |

Results

| | |
|------------------------|------------------------------|
| J_a (E1820) | 111.4 lbf-in/in ² |
| $K_{JIC}(E^*JQ)^{1/2}$ | 35.9 ksi sqrt(in) |

Qualification of Data

| | |
|-------------------------------|---------|
| 7.4.2: precrack length | valid |
| 9.1.4.1; precrack | valid |
| 9.1.4.2; final crack | valid |
| 9.1.5.1; Δa meas | valid |
| 9.1.5.2; Δa pred | valid |
| A9.6.4; # of pnts in reg.A | valid |
| A9.6.4; # of pnts in reg.B | valid |
| A9.8.1; $C_2 < 1$ | valid |
| A9.8.2.1; $a_{0q} - a_0$ | valid |
| A9.8.2.2; # of pnts for J_a | invalid |
| A9.8.2.2; # of pnts $< J_a$ | valid |
| A9.3.3.1; correlation | valid |

Qualification of J_a as J_{IC}

| | |
|-------------------|-------|
| A9.9.1; thickness | valid |
| A9.9.2; ligament | valid |
| A9.9.3; slope | valid |

| Index | Time | Force | Disp1 | Disp2 | Crack | Δa | CTOD | K561 | K1820 | KJ1820 | J1820 | Je | Jpl |
|-------|--------|--------|---------|---------|--------|---------|---------|-------------|-------------|-------------|--------|--------|--------|
| | Sec | lbf | inch | inch | inch | inch | inch | ksi sqr(in) | ksi sqr(in) | ksi sqr(in) | lbf/in | lbf/in | lbf/in |
| 10 | 380.8 | 304.3 | 0.00371 | 0.04822 | 1.2029 | -0.0014 | 0.00004 | 6.70 | 6.65 | 6.65 | 3.84 | 3.83 | 0.01 |
| 11 | 430.1 | 388.2 | 0.00477 | 0.06165 | 1.2027 | -0.0015 | 0.00007 | 8.58 | 8.48 | 8.50 | 6.27 | 6.23 | 0.04 |
| 12 | 462.8 | 471.2 | 0.00583 | 0.07416 | 1.2031 | -0.0011 | 0.00012 | 10.49 | 10.30 | 10.34 | 9.26 | 9.20 | 0.06 |
| 13 | 495.1 | 554.5 | 0.00687 | 0.08698 | 1.2041 | -0.0002 | 0.00017 | 12.45 | 12.15 | 12.15 | 12.80 | 12.78 | 0.01 |
| 14 | 526 | 638.0 | 0.00793 | 0.10071 | 1.2043 | 0.0001 | 0.00023 | 14.46 | 13.98 | 14.00 | 17.00 | 16.94 | 0.06 |
| 15 | 556.1 | 719.9 | 0.00898 | 0.11383 | 1.2047 | 0.0004 | 0.00030 | 16.48 | 15.79 | 15.81 | 21.67 | 21.60 | 0.07 |
| 16 | 586.1 | 800.9 | 0.01002 | 0.12604 | 1.2049 | 0.0006 | 0.00038 | 18.53 | 17.57 | 17.63 | 26.95 | 26.76 | 0.19 |
| 17 | 616.1 | 882.9 | 0.01108 | 0.13916 | 1.2051 | 0.0008 | 0.00047 | 20.68 | 19.37 | 19.47 | 32.85 | 32.53 | 0.32 |
| 18 | 645.8 | 960.5 | 0.01213 | 0.15137 | 1.2053 | 0.0011 | 0.00058 | 22.79 | 21.09 | 21.29 | 39.28 | 38.55 | 0.73 |
| 19 | 675.1 | 1031.2 | 0.01318 | 0.16296 | 1.2063 | 0.0021 | 0.00069 | 24.83 | 22.69 | 23.10 | 46.23 | 44.61 | 1.63 |
| 20 | 704.3 | 1099.4 | 0.01424 | 0.17334 | 1.2052 | 0.0010 | 0.00084 | 26.73 | 24.13 | 24.95 | 53.94 | 50.48 | 3.47 |
| 21 | 733.3 | 1166.2 | 0.01531 | 0.18372 | 1.2064 | 0.0022 | 0.00097 | 28.83 | 25.66 | 26.73 | 61.92 | 57.08 | 4.84 |
| 22 | 762.1 | 1228.5 | 0.01638 | 0.19318 | 1.2067 | 0.0024 | 0.00113 | 30.80 | 27.05 | 28.53 | 70.52 | 63.39 | 7.13 |
| 23 | 790.6 | 1286.3 | 0.01743 | 0.20264 | 1.2072 | 0.0029 | 0.00129 | 32.72 | 28.35 | 30.27 | 79.41 | 69.64 | 9.78 |
| 24 | 819.3 | 1341.9 | 0.01851 | 0.21210 | 1.2090 | 0.0048 | 0.00145 | 34.78 | 29.68 | 31.98 | 88.66 | 76.34 | 12.32 |
| 25 | 847.8 | 1394.0 | 0.01958 | 0.21912 | 1.2103 | 0.0061 | 0.00163 | 36.76 | 30.91 | 33.70 | 98.41 | 82.83 | 15.58 |
| 26 | 876.1 | 1435.6 | 0.02065 | 0.22614 | 1.2126 | 0.0084 | 0.00181 | 38.54 | 31.98 | 35.35 | 108.30 | 88.63 | 19.66 |
| 27 | 904.5 | 1470.5 | 0.02173 | 0.23071 | 1.2161 | 0.0118 | 0.00200 | 40.31 | 32.99 | 36.96 | 118.37 | 94.30 | 24.07 |
| 28 | 932.6 | 1498.4 | 0.02282 | 0.23682 | 1.2200 | 0.0157 | 0.00219 | 41.94 | 33.88 | 38.52 | 128.57 | 99.46 | 29.11 |
| 29 | 960.8 | 1514.1 | 0.02392 | 0.23895 | 1.2263 | 0.0221 | 0.00239 | 43.49 | 34.67 | 39.98 | 138.55 | 104.19 | 34.36 |
| 30 | 989.1 | 1523.4 | 0.02502 | 0.23926 | 1.2334 | 0.0292 | 0.00258 | 44.98 | 35.40 | 41.36 | 148.28 | 108.59 | 39.69 |
| 31 | 1017.3 | 1514.0 | 0.02606 | 0.23834 | 1.2411 | 0.0369 | 0.00279 | 45.78 | 35.74 | 42.62 | 157.45 | 110.71 | 46.73 |
| 32 | 1045.7 | 1500.8 | 0.02714 | 0.23560 | 1.2519 | 0.0476 | 0.00298 | 46.97 | 36.24 | 43.73 | 165.77 | 113.81 | 51.95 |
| 33 | 1074.2 | 1460.1 | 0.02821 | 0.22919 | 1.2654 | 0.0612 | 0.00318 | 47.33 | 36.29 | 44.68 | 173.00 | 114.11 | 58.88 |
| 34 | 1103.9 | 1418.9 | 0.02933 | 0.22308 | 1.2815 | 0.0772 | 0.00338 | 48.14 | 36.52 | 45.50 | 179.46 | 115.57 | 63.88 |
| 35 | 1133.9 | 1365.8 | 0.03040 | 0.21576 | 1.2975 | 0.0932 | 0.00359 | 48.30 | 36.43 | 46.22 | 185.14 | 115.01 | 70.13 |
| 36 | 1165.6 | 1344.0 | 0.03146 | 0.21179 | 1.3088 | 0.1046 | 0.00379 | 49.33 | 36.78 | 47.08 | 192.06 | 117.27 | 74.79 |
| 37 | 1197.6 | 1283.0 | 0.03259 | 0.20233 | 1.3264 | 0.1221 | 0.00402 | 49.32 | 36.58 | 47.68 | 197.03 | 115.99 | 81.04 |
| 38 | 1230.9 | 1215.1 | 0.03380 | 0.19135 | 1.3459 | 0.1417 | 0.00428 | 49.19 | 36.31 | 48.21 | 201.47 | 114.26 | 87.21 |
| 39 | 1266.6 | 1201.2 | 0.03487 | 0.18890 | 1.3554 | 0.1511 | 0.00449 | 50.43 | 36.74 | 49.00 | 208.08 | 116.96 | 91.12 |
| 40 | 1302.6 | 1162.3 | 0.03599 | 0.18372 | 1.3679 | 0.1637 | 0.00473 | 50.65 | 36.68 | 49.67 | 213.78 | 116.60 | 97.18 |
| 41 | 1339.4 | 1099.8 | 0.03718 | 0.17365 | 1.3853 | 0.1810 | 0.00501 | 50.23 | 36.29 | 50.10 | 217.54 | 114.12 | 103.42 |
| 42 | 1378 | 1052.1 | 0.03831 | 0.16632 | 1.4024 | 0.1981 | 0.00524 | 50.82 | 36.31 | 50.40 | 220.16 | 114.28 | 105.87 |

Elastic-Plastic Fracture Toughness Analysis

| | | | |
|----------------|--------------|---------------|------|
| Specimen ID | 5083-FT-5 | Geometry | C(T) |
| Contract | SSC 10624-01 | Orientation | T-L |
| Material | 5083-H321 | Yield (ksi) | 34.3 |
| Temperature(F) | 75.0 | Tensile (ksi) | 51.8 |
| Environment | LAB AIR | Modulus (Msi) | 10.5 |

Specimen Dimensions

| | | | |
|--------------------|-------|------------------|-------|
| Thickness (in) | 0.501 | Notch Depth (in) | 2.200 |
| Net Thickness (in) | 0.501 | Gage Length (in) | 0.200 |
| Width (in) | 4.000 | Alpha Ratio | 1 |
| Pin Spacing (in) | 2.200 | | |

Precrack Parameters

| | | | |
|--------------|-------|----------------------|-----|
| Pmax (lbf) | 733.0 | Stress Ratio | 0.1 |
| Final a (in) | 2.400 | Kmax (ksi sqrt (in)) | 9.9 |
| Pf (lbf) | 2158 | | |

Initial measured crack lengths (in)

| | | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 2.340 | 2.365 | 2.382 | 2.394 | 2.401 | 2.404 | 2.403 | 2.395 | 2.375 |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|

Final measured crack lengths (in)

| | | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 2.484 | 2.531 | 2.617 | 2.754 | 2.815 | 2.719 | 2.596 | 2.548 | 2.519 |
| x | | | | x | | | | |

| | | | |
|--------------------------------|-------|-------------------------|-------|
| Ave. initial crack length (in) | 2.388 | aoq (in) | 2.391 |
| Ave. final crack length (in) | 2.635 | Compliance Adj. Factor | 0.985 |
| Delta a measured (in) | 0.247 | Effective Modulus (Msi) | 10.3 |
| Delta a predicted (in) | 0.213 | | |

Results

| | |
|---|------------------------------|
| J _Q (E1820) | 146.9 lbf-in/in ² |
| K _{JIC} (E**JQ) ^{1/2} | 41.2 ksi sqrt(in) |

Qualification of Data

| | |
|---|---------|
| 7.4.2: precrack length | valid |
| 9.1.4.1; precrack | valid |
| 9.1.4.2; final crack | invalid |
| 9.1.5.1; Δa meas | valid |
| 9.1.5.2; Δa pred | valid |
| A9.6.4; # of pnts in reg.A | valid |
| A9.6.4; # of pnts in reg.B | valid |
| A9.8.1; C ₂ <1 | valid |
| A9.8.2.1; a _{0Q} -a ₀ | valid |
| A9.8.2.2; # of pnts for J _Q | valid |
| A9.8.2.2; # of pnts < J _Q | valid |
| A9.3.3.1; correlation | valid |

Qualification of J_Q as J_{IC}

| | |
|-------------------|-------|
| A9.9.1; thickness | valid |
| A9.9.2; ligament | valid |
| A9.9.3; slope | valid |

| Index | Time | Force | Disp1 | Disp2 | Crack | Δa | CTOD | K561 | K1820 | KJ1820 | J1820 | Je | Jpl |
|-------|--------|--------|---------|---------|--------|---------|---------|-------------|-------------|-------------|---------|--------|--------|
| | Sec | lbf | inch | inch | inch | inch | inch | ksi sq(r)in | ksi sq(r)in | ksi sq(r)in | lbf/in | lbf/in | lbf/in |
| 20 | 704.3 | 2535.4 | 0.03334 | 0.83618 | 2.3892 | -0.0016 | 0.00215 | 37.85 | 34.21 | 34.12 | 100.90 | 101.40 | -0.51 |
| 21 | 735.6 | 2647.3 | 0.03551 | 0.87647 | 2.3903 | -0.0004 | 0.00247 | 39.95 | 35.76 | 36.54 | 115.73 | 110.80 | 4.94 |
| 22 | 767.1 | 2742.0 | 0.03770 | 0.90912 | 2.3957 | 0.0050 | 0.00279 | 42.03 | 37.23 | 38.86 | 130.86 | 120.13 | 10.73 |
| 23 | 798.3 | 2838.8 | 0.03990 | 0.93842 | 2.3984 | 0.0076 | 0.00314 | 44.06 | 38.64 | 41.18 | 146.95 | 129.42 | 17.53 |
| 24 | 829.5 | 2921.9 | 0.04205 | 0.96436 | 2.4010 | 0.0103 | 0.00350 | 45.89 | 39.88 | 43.40 | 163.26 | 137.83 | 25.43 |
| 25 | 860.8 | 2997.1 | 0.04423 | 0.99121 | 2.4051 | 0.0144 | 0.00387 | 47.71 | 41.07 | 45.57 | 179.99 | 146.19 | 33.80 |
| 26 | 892.3 | 3076.8 | 0.04639 | 1.02051 | 2.4082 | 0.0175 | 0.00424 | 49.62 | 42.29 | 47.70 | 197.18 | 155.00 | 42.19 |
| 27 | 923.6 | 3151.1 | 0.04857 | 1.04370 | 2.4093 | 0.0186 | 0.00464 | 51.32 | 43.36 | 49.85 | 215.39 | 162.93 | 52.47 |
| 28 | 954.8 | 3215.2 | 0.05074 | 1.06720 | 2.4124 | 0.0216 | 0.00504 | 52.99 | 44.37 | 51.91 | 233.55 | 170.66 | 62.89 |
| 29 | 986 | 3273.0 | 0.05292 | 1.08612 | 2.4138 | 0.0231 | 0.00546 | 54.44 | 45.24 | 53.97 | 252.47 | 177.36 | 75.10 |
| 30 | 1017.5 | 3328.3 | 0.05510 | 1.10169 | 2.4144 | 0.0237 | 0.00590 | 55.78 | 46.03 | 56.02 | 272.01 | 183.62 | 88.40 |
| 31 | 1048.9 | 3380.1 | 0.05728 | 1.12396 | 2.4166 | 0.0259 | 0.00633 | 57.22 | 46.85 | 57.99 | 291.49 | 190.22 | 101.28 |
| 32 | 1080.5 | 3429.7 | 0.05947 | 1.13251 | 2.4191 | 0.0283 | 0.00677 | 58.65 | 47.65 | 59.92 | 311.21 | 196.79 | 114.43 |
| 33 | 1111.7 | 3475.9 | 0.06165 | 1.15051 | 2.4207 | 0.0300 | 0.00721 | 59.97 | 48.37 | 61.84 | 331.46 | 202.80 | 128.66 |
| 34 | 1143.1 | 3511.5 | 0.06387 | 1.16455 | 2.4225 | 0.0318 | 0.00768 | 61.05 | 48.96 | 63.76 | 352.30 | 207.72 | 144.58 |
| 35 | 1174.4 | 3541.9 | 0.06608 | 1.17584 | 2.4254 | 0.0347 | 0.00815 | 62.13 | 49.52 | 65.59 | 372.88 | 212.53 | 160.34 |
| 36 | 1205.7 | 3574.4 | 0.06830 | 1.18622 | 2.4285 | 0.0378 | 0.00861 | 63.31 | 50.13 | 67.39 | 393.56 | 217.81 | 175.74 |
| 37 | 1237.1 | 3586.4 | 0.07051 | 1.18591 | 2.4312 | 0.0405 | 0.00911 | 63.92 | 50.43 | 69.17 | 414.69 | 220.44 | 194.24 |
| 38 | 1268.5 | 3595.1 | 0.07272 | 1.19049 | 2.4362 | 0.0455 | 0.00959 | 64.71 | 50.81 | 70.83 | 434.82 | 223.77 | 211.05 |
| 39 | 1300 | 3609.6 | 0.07493 | 1.20178 | 2.4376 | 0.0469 | 0.01009 | 65.26 | 51.09 | 72.57 | 456.47 | 226.22 | 230.26 |
| 40 | 1331.6 | 3620.6 | 0.07714 | 1.19751 | 2.4419 | 0.0511 | 0.01058 | 66.05 | 51.46 | 74.19 | 477.06 | 229.54 | 247.52 |
| 41 | 1363.4 | 3627.2 | 0.07940 | 1.20575 | 2.4447 | 0.0540 | 0.01110 | 66.57 | 51.71 | 75.86 | 498.74 | 231.71 | 267.03 |
| 42 | 1395.1 | 3634.9 | 0.08163 | 1.20392 | 2.4498 | 0.0591 | 0.01159 | 67.39 | 52.08 | 77.40 | 519.23 | 235.10 | 284.13 |
| 43 | 1427 | 3634.9 | 0.08386 | 1.20575 | 2.4547 | 0.0640 | 0.01210 | 67.99 | 52.35 | 78.91 | 539.67 | 237.48 | 302.19 |
| 44 | 1459.1 | 3641.4 | 0.08607 | 1.21002 | 2.4565 | 0.0658 | 0.01261 | 68.40 | 52.53 | 80.50 | 561.57 | 239.19 | 322.38 |
| 45 | 1491.1 | 3626.9 | 0.08829 | 1.20056 | 2.4626 | 0.0719 | 0.01313 | 68.73 | 52.65 | 81.90 | 581.26 | 240.27 | 340.99 |
| 46 | 1523.1 | 3630.2 | 0.09053 | 1.20087 | 2.4648 | 0.0741 | 0.01366 | 69.10 | 52.82 | 83.43 | 603.26 | 241.78 | 361.48 |
| 47 | 1555.7 | 3624.4 | 0.09276 | 1.20422 | 2.4698 | 0.0791 | 0.01418 | 69.56 | 53.01 | 84.82 | 623.58 | 243.49 | 380.09 |
| 48 | 1588.2 | 3612.4 | 0.09497 | 1.19934 | 2.4742 | 0.0834 | 0.01471 | 69.76 | 53.07 | 86.20 | 643.98 | 244.07 | 399.91 |
| 49 | 1621 | 3599.6 | 0.09724 | 1.18957 | 2.4803 | 0.0896 | 0.01525 | 70.16 | 53.22 | 87.52 | 663.83 | 245.43 | 418.40 |
| 50 | 1653.6 | 3563.2 | 0.09945 | 1.17706 | 2.4855 | 0.0948 | 0.01581 | 69.71 | 52.97 | 88.81 | 683.52 | 243.14 | 440.37 |
| 51 | 1686.9 | 3561.9 | 0.10166 | 1.18317 | 2.4902 | 0.0995 | 0.01633 | 70.29 | 53.21 | 90.08 | 703.32 | 245.34 | 457.98 |
| 52 | 1720 | 3543.1 | 0.10388 | 1.17188 | 2.4944 | 0.1037 | 0.01689 | 70.25 | 53.16 | 91.37 | 723.54 | 244.91 | 478.64 |
| 53 | 1753.4 | 3534.7 | 0.10614 | 1.17401 | 2.4981 | 0.1074 | 0.01744 | 70.48 | 53.24 | 92.67 | 744.31 | 245.65 | 498.66 |
| 54 | 1787.1 | 3520.2 | 0.10837 | 1.16882 | 2.5040 | 0.1133 | 0.01798 | 70.82 | 53.35 | 93.84 | 763.20 | 246.70 | 516.50 |
| 55 | 1821 | 3510.3 | 0.11057 | 1.16303 | 2.5087 | 0.1179 | 0.01852 | 71.13 | 53.46 | 95.02 | 782.53 | 247.71 | 534.82 |
| 56 | 1854.7 | 3494.0 | 0.11274 | 1.15601 | 2.5150 | 0.1243 | 0.01905 | 71.47 | 53.57 | 96.09 | 800.22 | 248.75 | 551.47 |
| 57 | 1889 | 3482.1 | 0.11497 | 1.15753 | 2.5204 | 0.1297 | 0.01960 | 71.83 | 53.70 | 97.22 | 819.07 | 249.89 | 569.19 |
| 58 | 1923 | 3461.9 | 0.11717 | 1.14532 | 2.5262 | 0.1355 | 0.02016 | 71.98 | 53.72 | 98.29 | 837.30 | 250.12 | 587.18 |
| 59 | 1957.5 | 3431.9 | 0.11938 | 1.14014 | 2.5328 | 0.1421 | 0.02073 | 71.89 | 53.63 | 99.31 | 854.82 | 249.29 | 605.53 |
| 60 | 1992.4 | 3426.1 | 0.12157 | 1.13831 | 2.5373 | 0.1466 | 0.02127 | 72.35 | 53.80 | 100.40 | 873.55 | 250.88 | 622.67 |
| 61 | 2027.4 | 3394.0 | 0.12382 | 1.12244 | 2.5448 | 0.1541 | 0.02186 | 72.32 | 53.73 | 101.37 | 890.49 | 250.23 | 640.26 |
| 62 | 2062.9 | 3377.7 | 0.12607 | 1.11542 | 2.5500 | 0.1593 | 0.02243 | 72.51 | 53.78 | 102.41 | 909.00 | 250.65 | 658.35 |
| 63 | 2098.2 | 3355.3 | 0.12828 | 1.11206 | 2.5552 | 0.1644 | 0.02301 | 72.48 | 53.72 | 103.43 | 927.07 | 250.15 | 676.92 |
| 64 | 2133.9 | 3334.2 | 0.13052 | 1.10596 | 2.5615 | 0.1708 | 0.02359 | 72.67 | 53.76 | 104.38 | 944.27 | 250.48 | 693.79 |
| 65 | 2169.9 | 3320.9 | 0.13270 | 1.10413 | 2.5673 | 0.1766 | 0.02415 | 73.07 | 53.89 | 105.31 | 961.07 | 251.71 | 709.36 |
| 66 | 2206.1 | 3294.5 | 0.13489 | 1.08948 | 2.5740 | 0.1833 | 0.02473 | 73.12 | 53.86 | 106.18 | 977.08 | 251.43 | 725.65 |
| 67 | 2242.4 | 3254.9 | 0.13708 | 1.07819 | 2.5794 | 0.1887 | 0.02534 | 72.48 | 53.54 | 107.11 | 994.23 | 248.39 | 745.84 |
| 68 | 2279.4 | 3239.0 | 0.13927 | 1.07849 | 2.5864 | 0.1957 | 0.02591 | 72.96 | 53.69 | 107.92 | 1009.45 | 249.85 | 759.60 |
| 69 | 2316.4 | 3205.9 | 0.14149 | 1.05743 | 2.5940 | 0.2033 | 0.02652 | 72.89 | 53.60 | 108.72 | 1024.31 | 248.97 | 775.34 |
| 70 | 2353.6 | 3164.8 | 0.14371 | 1.04584 | 2.6026 | 0.2119 | 0.02715 | 72.66 | 53.43 | 109.44 | 1038.01 | 247.40 | 790.61 |

Elastic-Plastic Fracture Toughness Analysis

| | | | |
|----------------|--------------|---------------|------|
| Specimen ID | 5086-FT-1 | Geometry | C(T) |
| Contract | SSC 10624-01 | Orientation | T-L |
| Material | 5086-H116 | Yield (ksi) | 27.0 |
| Temperature(F) | 75.0 | Tensile (ksi) | 46.0 |
| Environment | LAB AIR | Modulus (Msi) | 10.5 |

Specimen Dimensions

| | | | |
|--------------------|-------|------------------|-------|
| Thickness (in) | 0.496 | Notch Depth (in) | 1.100 |
| Net Thickness (in) | 0.496 | Gage Length (in) | 0.200 |
| Width (in) | 2.000 | Alpha Ratio | 1 |
| Pin Spacing (in) | 1.100 | | |

Precrack Parameters

| | | | |
|--------------|-------|---------------------|-----|
| Pmax (lbf) | 308.4 | Stress Ratio | 0.1 |
| Final a (in) | 1.200 | Kmax (ksi sqrt(in)) | 6.0 |
| Pf (lbf) | 887 | | |

Initial measured crack lengths (in)

| | | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 1.172 | 1.189 | 1.200 | 1.204 | 1.208 | 1.212 | 1.213 | 1.207 | 1.197 |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|

Final measured crack lengths (in)

| | | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 1.324 | 1.358 | 1.451 | 1.566 | 1.647 | 1.547 | 1.426 | 1.354 | 1.338 |
| x | x | | x | x | x | | x | x |

| | | | |
|--------------------------------|-------|-------------------------|-------|
| Ave. initial crack length (in) | 1.202 | aoq (in) | 1.201 |
| Ave. final crack length (in) | 1.460 | Compliance Adj. Factor | 0.995 |
| Delta a measured (in) | 0.258 | Effective Modulus (Msi) | 10.4 |
| Delta a predicted (in) | 0.200 | | |

Results

| | |
|------------------------|------------------------------|
| J_Q (E1820) | 155.4 lbf-in/in ² |
| $K_{JIC}(E''JQ)^{1/2}$ | 42.3 ksi sqrt(in) |

Qualification of Data

| | |
|-------------------------------|---------|
| 7.4.2: precrack length | valid |
| 9.1.4.1: precrack | valid |
| 9.1.4.2: final crack | invalid |
| 9.1.5.1: Δa meas | valid |
| 9.1.5.2: Δa pred | invalid |
| A9.6.4: # of pnts in reg.A | valid |
| A9.6.4: # of pnts in reg.B | valid |
| A9.8.1: $C_2 < 1$ | valid |
| A9.8.2.1: $a_{0q} - a_0$ | valid |
| A9.8.2.2: # of pnts for J_Q | valid |
| A9.8.2.2: # of pnts $< J_Q$ | valid |
| A9.3.3.1: correlation | valid |

Qualification of J_Q as J_{IC}

| | |
|-------------------|-------|
| A9.9.1: thickness | valid |
| A9.9.2: ligament | valid |
| A9.9.3: slope | valid |

| Index | Time | Force | Disp1 | Disp2 | Crack | Δa | CTOD | K561 | K1820 | KJ1820 | J1820 | Je | Jpl |
|-------|--------|--------|---------|---------|--------|--------|---------|--------------|--------------|--------------|--------|--------|--------|
| | Sec | lbf | inch | inch | inch | inch | inch | ksi sqrt(in) | ksi sqrt(in) | ksi sqrt(in) | lbf/in | lbf/in | lbf/in |
| 5 | 238.6 | 353.5 | 0.00415 | 0.05585 | 1.2025 | 0.0016 | 0.00003 | 6.99 | 6.91 | 6.92 | 4.15 | 4.14 | 0.01 |
| 6 | 310.3 | 476.7 | 0.00569 | 0.07538 | 1.2015 | 0.0007 | 0.00010 | 9.49 | 9.30 | 9.36 | 7.59 | 7.49 | 0.10 |
| 7 | 350.6 | 598.8 | 0.00725 | 0.09399 | 1.2024 | 0.0016 | 0.00020 | 12.09 | 11.70 | 11.83 | 12.12 | 11.86 | 0.26 |
| 8 | 389.1 | 716.1 | 0.00882 | 0.11322 | 1.2017 | 0.0008 | 0.00032 | 14.64 | 13.97 | 14.29 | 17.70 | 16.92 | 0.78 |
| 9 | 426.7 | 828.7 | 0.01039 | 0.13092 | 1.2027 | 0.0018 | 0.00047 | 17.25 | 16.20 | 16.71 | 24.21 | 22.75 | 1.47 |
| 10 | 464.2 | 937.8 | 0.01196 | 0.14831 | 1.2025 | 0.0016 | 0.00064 | 19.87 | 18.32 | 19.14 | 31.74 | 29.10 | 2.64 |
| 11 | 500.8 | 1039.3 | 0.01354 | 0.16327 | 1.2026 | 0.0018 | 0.00084 | 22.46 | 20.31 | 21.53 | 40.19 | 35.77 | 4.42 |
| 12 | 537.3 | 1133.7 | 0.01509 | 0.17853 | 1.2012 | 0.0004 | 0.00107 | 24.90 | 22.10 | 23.89 | 49.46 | 42.33 | 7.13 |
| 13 | 573.6 | 1219.2 | 0.01665 | 0.19287 | 1.2010 | 0.0001 | 0.00131 | 27.29 | 23.75 | 26.20 | 59.49 | 48.90 | 10.59 |
| 14 | 609.1 | 1298.7 | 0.01824 | 0.20386 | 1.2016 | 0.0007 | 0.00157 | 29.70 | 25.33 | 28.48 | 70.32 | 55.62 | 14.70 |
| 15 | 644.3 | 1365.5 | 0.01981 | 0.21545 | 1.2025 | 0.0016 | 0.00185 | 31.88 | 26.68 | 30.68 | 81.57 | 61.71 | 19.86 |
| 16 | 679.6 | 1424.7 | 0.02139 | 0.22430 | 1.2021 | 0.0013 | 0.00215 | 33.79 | 27.82 | 32.89 | 93.74 | 67.08 | 26.66 |
| 17 | 714.3 | 1477.1 | 0.02298 | 0.23254 | 1.2027 | 0.0019 | 0.00245 | 35.65 | 28.88 | 35.02 | 106.31 | 72.27 | 34.04 |
| 18 | 749.1 | 1519.8 | 0.02459 | 0.23926 | 1.2038 | 0.0030 | 0.00278 | 37.31 | 29.78 | 37.11 | 119.38 | 76.84 | 42.54 |
| 19 | 783.6 | 1558.1 | 0.02620 | 0.24536 | 1.2045 | 0.0037 | 0.00311 | 38.82 | 30.57 | 39.16 | 132.93 | 81.00 | 51.93 |
| 20 | 817.8 | 1589.4 | 0.02779 | 0.24902 | 1.2056 | 0.0048 | 0.00344 | 40.17 | 31.25 | 41.12 | 146.51 | 84.64 | 61.87 |
| 21 | 852 | 1614.4 | 0.02940 | 0.25482 | 1.2078 | 0.0069 | 0.00378 | 41.47 | 31.88 | 42.99 | 160.21 | 88.08 | 72.13 |
| 22 | 886.1 | 1630.7 | 0.03101 | 0.25604 | 1.2089 | 0.0081 | 0.00413 | 42.31 | 32.27 | 44.86 | 174.42 | 90.27 | 84.15 |
| 23 | 920.3 | 1646.1 | 0.03264 | 0.26001 | 1.2116 | 0.0108 | 0.00449 | 43.38 | 32.76 | 46.63 | 188.43 | 92.99 | 95.44 |
| 24 | 954.3 | 1652.5 | 0.03424 | 0.25909 | 1.2139 | 0.0131 | 0.00485 | 44.01 | 33.03 | 48.34 | 202.49 | 94.56 | 107.93 |
| 25 | 988.8 | 1660.8 | 0.03586 | 0.26032 | 1.2158 | 0.0149 | 0.00521 | 44.68 | 33.32 | 50.02 | 216.84 | 96.22 | 120.61 |
| 26 | 1022.8 | 1663.7 | 0.03747 | 0.26123 | 1.2184 | 0.0175 | 0.00557 | 45.25 | 33.55 | 51.61 | 230.88 | 97.57 | 133.31 |
| 27 | 1057.2 | 1665.0 | 0.03908 | 0.26306 | 1.2209 | 0.0201 | 0.00594 | 45.76 | 33.76 | 53.17 | 245.00 | 98.75 | 146.25 |
| 28 | 1091.7 | 1672.8 | 0.04069 | 0.26215 | 1.2232 | 0.0224 | 0.00630 | 46.53 | 34.07 | 54.69 | 259.19 | 100.59 | 158.60 |
| 29 | 1126.1 | 1673.9 | 0.04231 | 0.26367 | 1.2239 | 0.0231 | 0.00668 | 46.72 | 34.14 | 56.26 | 274.35 | 101.02 | 173.33 |
| 30 | 1160.6 | 1671.3 | 0.04392 | 0.26367 | 1.2268 | 0.0260 | 0.00705 | 47.13 | 34.29 | 57.67 | 288.24 | 101.90 | 186.34 |
| 31 | 1195.2 | 1678.5 | 0.04555 | 0.26337 | 1.2281 | 0.0272 | 0.00743 | 47.71 | 34.52 | 59.15 | 303.21 | 103.30 | 199.91 |
| 32 | 1229.9 | 1675.1 | 0.04717 | 0.26337 | 1.2298 | 0.0290 | 0.00781 | 47.88 | 34.58 | 60.56 | 317.82 | 103.61 | 214.20 |
| 33 | 1264.6 | 1673.9 | 0.04878 | 0.26276 | 1.2314 | 0.0306 | 0.00819 | 48.13 | 34.67 | 61.93 | 332.36 | 104.15 | 228.20 |
| 34 | 1299.6 | 1672.5 | 0.05039 | 0.26215 | 1.2322 | 0.0314 | 0.00858 | 48.22 | 34.69 | 63.32 | 347.46 | 104.32 | 243.14 |
| 35 | 1334.6 | 1666.4 | 0.05201 | 0.26215 | 1.2346 | 0.0337 | 0.00896 | 48.38 | 34.74 | 64.59 | 361.51 | 104.57 | 256.94 |
| 36 | 1369.6 | 1663.5 | 0.05360 | 0.26092 | 1.2374 | 0.0365 | 0.00934 | 48.79 | 34.88 | 65.78 | 375.00 | 105.42 | 269.58 |
| 37 | 1404.9 | 1664.4 | 0.05522 | 0.26092 | 1.2380 | 0.0372 | 0.00973 | 48.96 | 34.94 | 67.10 | 390.19 | 105.80 | 284.39 |
| 38 | 1440.1 | 1661.4 | 0.05682 | 0.26062 | 1.2391 | 0.0382 | 0.01011 | 49.02 | 34.95 | 68.35 | 404.93 | 105.87 | 299.06 |
| 39 | 1475.6 | 1657.7 | 0.05843 | 0.26032 | 1.2411 | 0.0402 | 0.01050 | 49.25 | 35.02 | 69.53 | 418.96 | 106.30 | 312.65 |
| 40 | 1510.7 | 1648.4 | 0.06004 | 0.25848 | 1.2430 | 0.0422 | 0.01089 | 49.16 | 34.97 | 70.69 | 433.03 | 105.97 | 327.05 |
| 41 | 1546.5 | 1644.3 | 0.06167 | 0.25940 | 1.2454 | 0.0445 | 0.01129 | 49.43 | 35.05 | 71.81 | 446.92 | 106.46 | 340.45 |
| 42 | 1582.2 | 1641.2 | 0.06329 | 0.25848 | 1.2466 | 0.0458 | 0.01169 | 49.53 | 35.08 | 72.97 | 461.45 | 106.64 | 354.81 |
| 43 | 1618 | 1633.9 | 0.06488 | 0.25726 | 1.2480 | 0.0471 | 0.01208 | 49.42 | 35.02 | 74.08 | 475.64 | 106.29 | 369.35 |
| 44 | 1654 | 1626.4 | 0.06650 | 0.25665 | 1.2491 | 0.0483 | 0.01248 | 49.26 | 34.94 | 75.21 | 490.24 | 105.83 | 384.41 |
| 45 | 1690 | 1619.3 | 0.06813 | 0.25452 | 1.2517 | 0.0509 | 0.01288 | 49.42 | 34.98 | 76.22 | 503.49 | 106.04 | 397.44 |
| 46 | 1726.1 | 1615.8 | 0.06972 | 0.25452 | 1.2529 | 0.0520 | 0.01327 | 49.48 | 34.99 | 77.28 | 517.62 | 106.11 | 411.51 |
| 47 | 1762.5 | 1614.5 | 0.07131 | 0.25574 | 1.2544 | 0.0535 | 0.01366 | 49.73 | 35.07 | 78.30 | 531.39 | 106.61 | 424.78 |
| 48 | 1798.7 | 1608.0 | 0.07290 | 0.25360 | 1.2572 | 0.0564 | 0.01407 | 49.99 | 35.14 | 79.21 | 543.83 | 107.04 | 436.79 |
| 49 | 1835.1 | 1600.7 | 0.07453 | 0.25116 | 1.2585 | 0.0577 | 0.01448 | 49.86 | 35.08 | 80.25 | 558.18 | 106.65 | 451.53 |
| 50 | 1871.9 | 1598.4 | 0.07614 | 0.25146 | 1.2599 | 0.0590 | 0.01487 | 50.03 | 35.13 | 81.25 | 572.16 | 106.95 | 465.21 |
| 51 | 1908.6 | 1595.3 | 0.07775 | 0.25146 | 1.2616 | 0.0607 | 0.01528 | 50.23 | 35.19 | 82.21 | 585.71 | 107.33 | 478.39 |
| 52 | 1945.1 | 1590.9 | 0.07937 | 0.24963 | 1.2635 | 0.0627 | 0.01569 | 50.42 | 35.24 | 83.14 | 599.03 | 107.63 | 491.40 |
| 53 | 1982 | 1586.5 | 0.08099 | 0.24933 | 1.2647 | 0.0639 | 0.01609 | 50.44 | 35.23 | 84.11 | 613.12 | 107.60 | 505.53 |
| 54 | 2018.7 | 1577.2 | 0.08260 | 0.24872 | 1.2664 | 0.0655 | 0.01650 | 50.27 | 35.15 | 85.03 | 626.60 | 107.09 | 519.51 |
| 55 | 2055.6 | 1573.0 | 0.08416 | 0.24780 | 1.2678 | 0.0670 | 0.01690 | 50.36 | 35.17 | 85.92 | 639.78 | 107.21 | 532.58 |
| 56 | 2092.9 | 1570.1 | 0.08577 | 0.24689 | 1.2692 | 0.0683 | 0.01731 | 50.50 | 35.21 | 86.83 | 653.45 | 107.43 | 546.02 |
| 57 | 2130.1 | 1555.9 | 0.08739 | 0.24445 | 1.2714 | 0.0705 | 0.01773 | 50.17 | 35.06 | 87.67 | 666.12 | 106.51 | 559.61 |
| 58 | 2167.4 | 1544.9 | 0.08901 | 0.24353 | 1.2741 | 0.0732 | 0.01816 | 50.14 | 35.01 | 88.46 | 678.13 | 106.25 | 571.87 |
| 59 | 2204.9 | 1535.9 | 0.09066 | 0.24322 | 1.2764 | 0.0755 | 0.01860 | 50.13 | 34.98 | 89.27 | 690.70 | 106.07 | 584.63 |
| 60 | 2242.4 | 1524.8 | 0.09228 | 0.24139 | 1.2786 | 0.0777 | 0.01903 | 49.98 | 34.90 | 90.07 | 703.02 | 105.56 | 597.45 |

| Index | Time | Force | Disp1 | Disp2 | Crack | Δa | CTOD | K561 | K1820 | KJ1820 | J1820 | Je | Jpl |
|-------|--------|--------|---------|---------|--------|------------|---------|-------------|-------------|-------------|---------|--------|--------|
| | Sec | lbf | inch | inch | inch | inch | inch | ksi sqr(in) | ksi sqr(in) | ksi sqr(in) | lbf/in | lbf/in | lbf/in |
| 61 | 2280.4 | 1513.5 | 0.09388 | 0.23773 | 1.2816 | 0.0808 | 0.01946 | 50.00 | 34.87 | 90.77 | 713.99 | 105.40 | 608.59 |
| 62 | 2318.4 | 1500.2 | 0.09545 | 0.23773 | 1.2845 | 0.0837 | 0.01989 | 49.86 | 34.79 | 91.45 | 724.78 | 104.89 | 619.89 |
| 63 | 2356.6 | 1485.8 | 0.09706 | 0.23438 | 1.2874 | 0.0866 | 0.02033 | 49.65 | 34.68 | 92.14 | 735.70 | 104.21 | 631.49 |
| 64 | 2395.2 | 1479.3 | 0.09864 | 0.23438 | 1.2901 | 0.0892 | 0.02075 | 49.87 | 34.73 | 92.82 | 746.62 | 104.54 | 642.09 |
| 65 | 2433.9 | 1471.1 | 0.10023 | 0.23254 | 1.2921 | 0.0913 | 0.02118 | 49.84 | 34.70 | 93.54 | 758.33 | 104.33 | 654.00 |
| 66 | 2472.9 | 1460.9 | 0.10180 | 0.23254 | 1.2939 | 0.0930 | 0.02160 | 49.62 | 34.59 | 94.27 | 770.25 | 103.69 | 666.57 |
| 67 | 2512.1 | 1448.7 | 0.10342 | 0.22919 | 1.2979 | 0.0970 | 0.02206 | 49.80 | 34.61 | 94.82 | 779.20 | 103.83 | 675.37 |
| 68 | 2551.6 | 1440.0 | 0.10501 | 0.22766 | 1.3001 | 0.0992 | 0.02250 | 49.77 | 34.58 | 95.50 | 790.41 | 103.62 | 686.79 |
| 69 | 2591.2 | 1428.2 | 0.10662 | 0.22675 | 1.3021 | 0.1013 | 0.02294 | 49.52 | 34.46 | 96.19 | 801.91 | 102.89 | 699.02 |
| 70 | 2631.1 | 1412.2 | 0.10825 | 0.22430 | 1.3067 | 0.1058 | 0.02342 | 49.56 | 34.42 | 96.66 | 809.76 | 102.69 | 707.07 |
| 71 | 2671.2 | 1399.4 | 0.10984 | 0.22339 | 1.3086 | 0.1077 | 0.02386 | 49.19 | 34.26 | 97.34 | 821.10 | 101.72 | 719.39 |
| 72 | 2711.7 | 1392.5 | 0.11146 | 0.22125 | 1.3106 | 0.1098 | 0.02431 | 49.24 | 34.25 | 97.99 | 832.24 | 101.68 | 730.56 |
| 73 | 2752.2 | 1383.1 | 0.11304 | 0.21942 | 1.3138 | 0.1129 | 0.02476 | 49.38 | 34.27 | 98.52 | 841.26 | 101.78 | 739.48 |
| 74 | 2793.1 | 1374.5 | 0.11463 | 0.21912 | 1.3163 | 0.1154 | 0.02520 | 49.41 | 34.25 | 99.11 | 851.36 | 101.69 | 749.67 |
| 75 | 2834.2 | 1366.6 | 0.11621 | 0.21790 | 1.3187 | 0.1178 | 0.02565 | 49.48 | 34.25 | 99.69 | 861.37 | 101.66 | 759.71 |
| 76 | 2875.6 | 1351.2 | 0.11784 | 0.21515 | 1.3222 | 0.1213 | 0.02613 | 49.29 | 34.14 | 100.19 | 870.01 | 101.00 | 769.00 |
| 77 | 2916.9 | 1339.7 | 0.11942 | 0.21393 | 1.3259 | 0.1250 | 0.02660 | 49.43 | 34.15 | 100.63 | 877.64 | 101.04 | 776.59 |
| 78 | 2958.9 | 1324.9 | 0.12098 | 0.21210 | 1.3289 | 0.1280 | 0.02706 | 49.17 | 34.01 | 101.11 | 886.09 | 100.26 | 785.84 |
| 79 | 3001.2 | 1309.5 | 0.12260 | 0.20843 | 1.3325 | 0.1316 | 0.02755 | 49.00 | 33.91 | 101.56 | 893.96 | 99.63 | 794.33 |
| 80 | 3043.9 | 1298.8 | 0.12417 | 0.20721 | 1.3357 | 0.1349 | 0.02802 | 49.06 | 33.89 | 102.01 | 901.82 | 99.54 | 802.28 |
| 81 | 3086.9 | 1286.9 | 0.12577 | 0.20508 | 1.3387 | 0.1378 | 0.02850 | 48.96 | 33.82 | 102.49 | 910.33 | 99.12 | 811.20 |
| 82 | 3130.1 | 1273.3 | 0.12739 | 0.20355 | 1.3420 | 0.1411 | 0.02899 | 48.83 | 33.73 | 102.94 | 918.30 | 98.60 | 819.70 |
| 83 | 3173.7 | 1262.5 | 0.12896 | 0.20294 | 1.3442 | 0.1434 | 0.02945 | 48.63 | 33.63 | 103.45 | 927.50 | 98.00 | 829.51 |
| 84 | 3217.7 | 1255.8 | 0.13056 | 0.20203 | 1.3476 | 0.1467 | 0.02992 | 48.98 | 33.72 | 103.86 | 934.93 | 98.54 | 836.39 |
| 85 | 3261.9 | 1247.7 | 0.13214 | 0.20050 | 1.3499 | 0.1491 | 0.03039 | 49.00 | 33.70 | 104.36 | 943.91 | 98.41 | 845.50 |
| 86 | 3306.4 | 1236.9 | 0.13375 | 0.19836 | 1.3530 | 0.1521 | 0.03088 | 48.98 | 33.65 | 104.79 | 951.77 | 98.16 | 853.61 |
| 87 | 3351.4 | 1232.2 | 0.13532 | 0.19714 | 1.3546 | 0.1537 | 0.03133 | 49.04 | 33.66 | 105.35 | 961.87 | 98.19 | 863.68 |
| 88 | 3396.4 | 1219.8 | 0.13692 | 0.19562 | 1.3569 | 0.1561 | 0.03181 | 48.74 | 33.52 | 105.83 | 970.71 | 97.36 | 873.36 |
| 89 | 3441.4 | 1202.7 | 0.13856 | 0.19287 | 1.3601 | 0.1593 | 0.03233 | 48.28 | 33.31 | 106.24 | 978.13 | 96.15 | 881.98 |
| 90 | 3487.4 | 1199.2 | 0.14013 | 0.19257 | 1.3622 | 0.1614 | 0.03278 | 48.56 | 33.39 | 106.71 | 986.88 | 96.61 | 890.28 |
| 91 | 3533.4 | 1189.4 | 0.14173 | 0.19135 | 1.3659 | 0.1651 | 0.03328 | 48.78 | 33.42 | 107.03 | 992.73 | 96.81 | 895.91 |
| 92 | 3579.7 | 1176.9 | 0.14336 | 0.18951 | 1.3681 | 0.1672 | 0.03378 | 48.39 | 33.25 | 107.51 | 1001.79 | 95.82 | 905.97 |
| 93 | 3626.2 | 1166.1 | 0.14495 | 0.18799 | 1.3721 | 0.1713 | 0.03429 | 48.62 | 33.29 | 107.77 | 1006.57 | 96.02 | 910.54 |
| 94 | 3673.2 | 1155.8 | 0.14658 | 0.18738 | 1.3746 | 0.1737 | 0.03479 | 48.47 | 33.20 | 108.21 | 1014.73 | 95.53 | 919.20 |
| 95 | 3720.7 | 1147.3 | 0.14820 | 0.18524 | 1.3779 | 0.1771 | 0.03530 | 48.68 | 33.24 | 108.53 | 1020.88 | 95.75 | 925.12 |
| 96 | 3768.6 | 1136.2 | 0.14980 | 0.18372 | 1.3814 | 0.1806 | 0.03581 | 48.73 | 33.21 | 108.83 | 1026.44 | 95.60 | 930.84 |
| 97 | 3816.6 | 1124.0 | 0.15138 | 0.18249 | 1.3851 | 0.1842 | 0.03633 | 48.74 | 33.17 | 109.09 | 1031.43 | 95.35 | 936.09 |
| 98 | 3865.4 | 1116.9 | 0.15296 | 0.18066 | 1.3872 | 0.1863 | 0.03681 | 48.75 | 33.15 | 109.52 | 1039.48 | 95.21 | 944.27 |
| 99 | 3914.2 | 1104.0 | 0.15457 | 0.17883 | 1.3900 | 0.1892 | 0.03733 | 48.45 | 33.00 | 109.87 | 1046.21 | 94.39 | 951.82 |
| 100 | 3963.7 | 1096.8 | 0.15615 | 0.17700 | 1.3931 | 0.1923 | 0.03783 | 48.71 | 33.06 | 110.17 | 1051.94 | 94.70 | 957.24 |
| 101 | 4013.4 | 1085.2 | 0.15776 | 0.17609 | 1.3958 | 0.1950 | 0.03834 | 48.48 | 32.94 | 110.52 | 1058.68 | 94.04 | 964.64 |
| 102 | 4063.4 | 1073.2 | 0.15935 | 0.17456 | 1.3991 | 0.1982 | 0.03887 | 48.37 | 32.86 | 110.80 | 1063.93 | 93.57 | 970.36 |
| 103 | 4113.8 | 1059.4 | 0.16092 | 0.17212 | 1.4029 | 0.2020 | 0.03940 | 48.25 | 32.77 | 110.99 | 1067.71 | 93.05 | 974.65 |

Elastic-Plastic Fracture Toughness Analysis

| | | | |
|----------------|--------------|---------------|------|
| Specimen ID | 5086-FT-2 | Geometry | C(T) |
| Contract | SSC 10624-01 | Orientation | T-L |
| Material | 5086-H116 | Yield (ksi) | 27.0 |
| Temperature(F) | 75.0 | Tensile (ksi) | 46.0 |
| Environment | LAB AIR | Modulus (Msi) | 10.5 |

Specimen Dimensions

| | | | |
|--------------------|-------|------------------|-------|
| Thickness (in) | 0.497 | Notch Depth (in) | 1.100 |
| Net Thickness (in) | 0.497 | Gage Length (in) | 0.200 |
| Width (in) | 2.000 | Alpha Ratio | 1 |
| Pin Spacing (in) | 1.100 | | |

Precrack Parameters

| | | | |
|--------------|-------|----------------------|-----|
| Pmax (lbf) | 308.4 | Stress Ratio | 0.1 |
| Final a (in) | 1.200 | Kmax (ksi sqrt (in)) | 6.0 |
| Pf (lbf) | 885 | | |

Initial measured crack lengths (in)

| | | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 1.180 | 1.199 | 1.208 | 1.208 | 1.209 | 1.211 | 1.209 | 1.199 | 1.181 |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|

Final measured crack lengths (in)

| | | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 1.331 | 1.362 | 1.446 | 1.577 | 1.636 | 1.514 | 1.405 | 1.349 | 1.338 |
| x | x | | x | x | | | x | x |

| | | | |
|--------------------------------|-------|-------------------------|-------|
| Ave. initial crack length (in) | 1.203 | aoq (in) | n/a |
| Ave. final crack length (in) | 1.453 | Compliance Adj. Factor | 1.014 |
| Delta a measured (in) | 0.250 | Effective Modulus (Msi) | 10.6 |
| Delta a predicted (in) | 0.198 | | |

Results

| | |
|--------------------------|------------------------------|
| J_Q (E1820) | 147.6 lbf-in/in ² |
| $K_{JIC}(E^{*}JQ)^{1/2}$ | 41.3 ksi sqrt(in) |

Qualification of Data

| | |
|-------------------------------|---------|
| 7.4.2; precrack length | valid |
| 9.1.4.1; precrack | valid |
| 9.1.4.2; final crack | invalid |
| 9.1.5.1; Δa meas | valid |
| 9.1.5.2; Δa pred | invalid |
| A9.6.4; # of pnts in reg.A | valid |
| A9.6.4; # of pnts in reg.B | valid |
| A9.8.1; $C_2 < 1$ | valid |
| A9.8.2.1; $a_{0q} - a_0$ | #VALUE! |
| A9.8.2.2; # of pnts for J_Q | valid |
| A9.8.2.2; # of pnts < J_Q | valid |
| A9.3.3.1; correlation | valid |

Qualification of J_Q as J_{IC}

| | |
|-------------------|-------|
| A9.9.1; thickness | valid |
| A9.9.2; ligament | valid |
| A9.9.3; slope | valid |

| Index | Time | Force | Disp1 | Disp2 | Crack | Δa | CTOD | K561 | K1820 | KJ1820 | J1820 | Je | Jpl |
|-------|--------|--------|---------|---------|--------|--------|---------|-------------|-------------|-------------|--------|--------|--------|
| | Sec | lbf | inch | inch | inch | inch | inch | ksi sqr(in) | ksi sqr(in) | ksi sqr(in) | lbf/in | lbf/in | lbf/in |
| 7 | 361.7 | 478.5 | 0.00561 | 0.07507 | 1.2031 | 0.0000 | 0.00010 | 9.56 | 9.36 | 9.37 | 7.61 | 7.60 | 0.01 |
| 9 | 439.8 | 719.3 | 0.00872 | 0.11322 | 1.2033 | 0.0002 | 0.00033 | 14.76 | 14.08 | 14.35 | 17.86 | 17.18 | 0.68 |
| 11 | 513.8 | 942.5 | 0.01185 | 0.14801 | 1.2037 | 0.0006 | 0.00065 | 20.05 | 18.46 | 19.26 | 32.14 | 29.54 | 2.60 |
| 12 | 550.5 | 1044.3 | 0.01341 | 0.16419 | 1.2043 | 0.0012 | 0.00085 | 22.69 | 20.48 | 21.65 | 40.64 | 36.34 | 4.29 |
| 13 | 586.8 | 1139.7 | 0.01498 | 0.17914 | 1.2043 | 0.0012 | 0.00107 | 25.27 | 22.35 | 24.04 | 50.11 | 43.29 | 6.81 |
| 14 | 622.6 | 1227.7 | 0.01658 | 0.19379 | 1.2042 | 0.0011 | 0.00132 | 27.78 | 24.07 | 26.43 | 60.54 | 50.21 | 10.33 |
| 15 | 658.1 | 1304.6 | 0.01815 | 0.20508 | 1.2045 | 0.0014 | 0.00159 | 30.14 | 25.59 | 28.72 | 71.48 | 56.78 | 14.71 |
| 16 | 693.5 | 1372.8 | 0.01974 | 0.21545 | 1.2052 | 0.0020 | 0.00188 | 32.37 | 26.97 | 30.98 | 83.21 | 63.02 | 20.18 |
| 17 | 728.3 | 1432.7 | 0.02133 | 0.22461 | 1.2056 | 0.0024 | 0.00218 | 34.42 | 28.16 | 33.20 | 95.52 | 68.75 | 26.77 |
| 18 | 763.1 | 1483.9 | 0.02294 | 0.23285 | 1.2063 | 0.0031 | 0.00249 | 36.30 | 29.21 | 35.38 | 108.46 | 73.96 | 34.50 |
| 19 | 797.5 | 1525.4 | 0.02455 | 0.23956 | 1.2074 | 0.0043 | 0.00282 | 37.96 | 30.10 | 37.47 | 121.70 | 78.51 | 43.19 |
| 20 | 831.6 | 1561.4 | 0.02615 | 0.24597 | 1.2082 | 0.0051 | 0.00315 | 39.43 | 30.86 | 39.51 | 135.26 | 82.51 | 52.74 |
| 21 | 865.8 | 1587.2 | 0.02778 | 0.24994 | 1.2100 | 0.0069 | 0.00350 | 40.69 | 31.48 | 41.48 | 149.13 | 85.88 | 63.26 |
| 22 | 899.8 | 1606.0 | 0.02941 | 0.25177 | 1.2121 | 0.0089 | 0.00385 | 41.76 | 31.98 | 43.39 | 163.17 | 88.65 | 74.52 |
| 23 | 933.8 | 1620.5 | 0.03102 | 0.25391 | 1.2141 | 0.0110 | 0.00420 | 42.67 | 32.40 | 45.21 | 177.16 | 90.99 | 86.17 |
| 24 | 968.1 | 1629.0 | 0.03265 | 0.25635 | 1.2164 | 0.0133 | 0.00457 | 43.40 | 32.72 | 46.98 | 191.32 | 92.81 | 98.51 |
| 25 | 1002.1 | 1640.3 | 0.03425 | 0.25818 | 1.2197 | 0.0165 | 0.00492 | 44.42 | 33.17 | 48.63 | 204.96 | 95.34 | 109.62 |
| 26 | 1036.4 | 1650.4 | 0.03588 | 0.25879 | 1.2213 | 0.0182 | 0.00528 | 45.16 | 33.48 | 50.33 | 219.52 | 97.16 | 122.36 |
| 27 | 1070.6 | 1656.7 | 0.03750 | 0.26001 | 1.2237 | 0.0205 | 0.00565 | 45.85 | 33.77 | 51.94 | 233.78 | 98.83 | 134.95 |
| 28 | 1104.7 | 1660.8 | 0.03913 | 0.25971 | 1.2244 | 0.0212 | 0.00603 | 46.17 | 33.90 | 53.59 | 248.94 | 99.60 | 149.34 |
| 29 | 1139.1 | 1663.8 | 0.04075 | 0.26123 | 1.2253 | 0.0221 | 0.00640 | 46.48 | 34.03 | 55.19 | 263.94 | 100.34 | 163.60 |
| 30 | 1173.2 | 1664.4 | 0.04236 | 0.26062 | 1.2281 | 0.0250 | 0.00677 | 47.03 | 34.24 | 56.62 | 277.83 | 101.58 | 176.25 |
| 31 | 1207.5 | 1664.3 | 0.04395 | 0.26184 | 1.2297 | 0.0266 | 0.00715 | 47.33 | 34.34 | 58.07 | 292.21 | 102.22 | 189.99 |
| 32 | 1242.1 | 1666.1 | 0.04557 | 0.26276 | 1.2316 | 0.0285 | 0.00752 | 47.77 | 34.51 | 59.49 | 306.73 | 103.24 | 203.49 |
| 33 | 1276.7 | 1670.4 | 0.04717 | 0.26306 | 1.2320 | 0.0289 | 0.00790 | 48.07 | 34.63 | 60.95 | 321.92 | 103.95 | 217.97 |
| 34 | 1311.4 | 1674.3 | 0.04881 | 0.26367 | 1.2337 | 0.0306 | 0.00828 | 48.61 | 34.84 | 62.33 | 336.65 | 105.19 | 231.46 |
| 35 | 1346.1 | 1675.7 | 0.05044 | 0.26367 | 1.2355 | 0.0324 | 0.00867 | 49.03 | 34.99 | 63.68 | 351.41 | 106.12 | 245.30 |
| 36 | 1380.7 | 1666.6 | 0.05206 | 0.26245 | 1.2358 | 0.0327 | 0.00906 | 48.63 | 34.83 | 65.06 | 366.86 | 105.12 | 261.74 |
| 37 | 1415.6 | 1666.0 | 0.05367 | 0.26215 | 1.2389 | 0.0358 | 0.00944 | 49.23 | 35.04 | 66.25 | 380.33 | 106.39 | 273.95 |
| 38 | 1450.7 | 1666.1 | 0.05530 | 0.26154 | 1.2396 | 0.0365 | 0.00983 | 49.38 | 35.09 | 67.57 | 395.67 | 106.72 | 288.95 |
| 39 | 1485.5 | 1650.7 | 0.05691 | 0.25971 | 1.2416 | 0.0385 | 0.01022 | 48.98 | 34.91 | 68.76 | 409.78 | 105.62 | 304.17 |
| 40 | 1520.6 | 1650.1 | 0.05852 | 0.25909 | 1.2436 | 0.0405 | 0.01061 | 49.37 | 35.05 | 69.93 | 423.78 | 106.44 | 317.34 |
| 41 | 1555.9 | 1650.1 | 0.06012 | 0.26184 | 1.2447 | 0.0415 | 0.01100 | 49.59 | 35.12 | 71.13 | 438.46 | 106.90 | 331.56 |
| 42 | 1591.2 | 1645.8 | 0.06172 | 0.25848 | 1.2463 | 0.0432 | 0.01139 | 49.70 | 35.15 | 72.27 | 452.65 | 107.07 | 345.58 |
| 43 | 1626.6 | 1642.5 | 0.06334 | 0.25757 | 1.2475 | 0.0443 | 0.01178 | 49.77 | 35.16 | 73.43 | 467.30 | 107.15 | 360.15 |
| 44 | 1662.4 | 1641.8 | 0.06495 | 0.25848 | 1.2492 | 0.0460 | 0.01217 | 50.10 | 35.27 | 74.53 | 481.39 | 107.84 | 373.55 |
| 45 | 1698.1 | 1643.5 | 0.06656 | 0.25787 | 1.2496 | 0.0464 | 0.01256 | 50.28 | 35.34 | 75.70 | 496.58 | 108.25 | 388.34 |
| 46 | 1733.9 | 1643.4 | 0.06817 | 0.25909 | 1.2517 | 0.0486 | 0.01295 | 50.75 | 35.50 | 76.73 | 510.25 | 109.23 | 401.02 |
| 47 | 1769.6 | 1635.9 | 0.06975 | 0.25665 | 1.2534 | 0.0503 | 0.01335 | 50.71 | 35.46 | 77.76 | 524.02 | 109.00 | 415.02 |
| 48 | 1805.2 | 1629.9 | 0.07135 | 0.25574 | 1.2550 | 0.0519 | 0.01374 | 50.73 | 35.46 | 78.78 | 537.95 | 108.95 | 429.00 |
| 49 | 1841.1 | 1622.0 | 0.07293 | 0.25574 | 1.2568 | 0.0536 | 0.01414 | 50.67 | 35.41 | 79.77 | 551.55 | 108.69 | 442.86 |
| 50 | 1877.2 | 1615.1 | 0.07456 | 0.25330 | 1.2586 | 0.0554 | 0.01455 | 50.69 | 35.40 | 80.77 | 565.41 | 108.60 | 456.81 |
| 51 | 1913.4 | 1607.2 | 0.07619 | 0.25269 | 1.2604 | 0.0573 | 0.01496 | 50.64 | 35.36 | 81.75 | 579.22 | 108.37 | 470.85 |
| 52 | 1949.6 | 1591.6 | 0.07778 | 0.24963 | 1.2630 | 0.0599 | 0.01537 | 50.35 | 35.22 | 82.63 | 591.70 | 107.50 | 484.20 |
| 53 | 1986 | 1588.1 | 0.07941 | 0.24963 | 1.2651 | 0.0620 | 0.01579 | 50.61 | 35.30 | 83.55 | 605.00 | 107.98 | 497.02 |
| 54 | 2022.6 | 1584.5 | 0.08102 | 0.24994 | 1.2668 | 0.0637 | 0.01619 | 50.80 | 35.35 | 84.47 | 618.45 | 108.29 | 510.16 |
| 55 | 2059.2 | 1579.9 | 0.08264 | 0.24841 | 1.2687 | 0.0656 | 0.01660 | 50.95 | 35.39 | 85.38 | 631.75 | 108.52 | 523.23 |
| 56 | 2095.9 | 1570.3 | 0.08425 | 0.24811 | 1.2711 | 0.0679 | 0.01702 | 50.94 | 35.35 | 86.23 | 644.40 | 108.32 | 536.08 |
| 57 | 2132.9 | 1563.1 | 0.08589 | 0.24689 | 1.2731 | 0.0700 | 0.01745 | 50.99 | 35.35 | 87.10 | 657.55 | 108.29 | 549.26 |
| 58 | 2170.1 | 1560.2 | 0.08749 | 0.24567 | 1.2749 | 0.0717 | 0.01785 | 51.22 | 35.42 | 87.96 | 670.54 | 108.72 | 561.82 |
| 59 | 2207.2 | 1550.8 | 0.08907 | 0.24384 | 1.2778 | 0.0747 | 0.01827 | 51.34 | 35.43 | 88.70 | 681.92 | 108.78 | 573.14 |
| 60 | 2244.7 | 1541.4 | 0.09066 | 0.24261 | 1.2797 | 0.0766 | 0.01869 | 51.23 | 35.37 | 89.52 | 694.60 | 108.40 | 586.20 |
| 61 | 2282.2 | 1534.6 | 0.09226 | 0.24261 | 1.2820 | 0.0789 | 0.01911 | 51.36 | 35.38 | 90.30 | 706.73 | 108.51 | 598.21 |
| 62 | 2319.9 | 1526.2 | 0.09388 | 0.24109 | 1.2841 | 0.0810 | 0.01954 | 51.36 | 35.36 | 91.10 | 719.20 | 108.36 | 610.84 |
| 63 | 2357.9 | 1513.7 | 0.09550 | 0.23865 | 1.2880 | 0.0849 | 0.01999 | 51.51 | 35.37 | 91.73 | 729.31 | 108.42 | 620.89 |
| 64 | 2395.9 | 1508.6 | 0.09712 | 0.23865 | 1.2895 | 0.0863 | 0.02041 | 51.55 | 35.37 | 92.55 | 742.40 | 108.42 | 633.98 |

| Index | Time | Force | Disp1 | Disp2 | Crack | Δa | CTOD | K561 | K1820 | KJ1820 | J1820 | Je | Jpl |
|-------|--------|--------|---------|---------|--------|------------|---------|-------------|-------------|-------------|---------|--------|--------|
| | Sec | lbf | inch | inch | inch | inch | inch | ksi sqg(in) | ksi sqg(in) | ksi sqg(in) | lbf/in | lbf/in | lbf/in |
| 65 | 2434.1 | 1497.3 | 0.09874 | 0.23651 | 1.2923 | 0.0891 | 0.02085 | 51.52 | 35.32 | 93.25 | 753.68 | 108.14 | 645.54 |
| 66 | 2472.6 | 1490.5 | 0.10034 | 0.23590 | 1.2944 | 0.0913 | 0.02128 | 51.61 | 35.33 | 93.99 | 765.56 | 108.20 | 657.36 |
| 67 | 2510.9 | 1473.7 | 0.10196 | 0.23377 | 1.2975 | 0.0944 | 0.02173 | 51.29 | 35.18 | 94.64 | 776.19 | 107.25 | 668.94 |
| 68 | 2549.9 | 1460.3 | 0.10354 | 0.23071 | 1.3008 | 0.0977 | 0.02218 | 51.25 | 35.12 | 95.23 | 785.96 | 106.90 | 679.06 |
| 69 | 2588.9 | 1450.0 | 0.10515 | 0.23010 | 1.3039 | 0.1008 | 0.02263 | 51.36 | 35.12 | 95.84 | 796.09 | 106.92 | 689.16 |
| 70 | 2628.2 | 1440.3 | 0.10676 | 0.22858 | 1.3066 | 0.1034 | 0.02307 | 51.37 | 35.10 | 96.49 | 806.91 | 106.76 | 700.15 |
| 71 | 2667.7 | 1424.4 | 0.10836 | 0.22583 | 1.3097 | 0.1065 | 0.02353 | 51.09 | 34.96 | 97.08 | 816.73 | 105.91 | 710.82 |
| 72 | 2707.6 | 1414.3 | 0.10994 | 0.22430 | 1.3127 | 0.1095 | 0.02398 | 51.18 | 34.95 | 97.65 | 826.44 | 105.88 | 720.56 |
| 73 | 2747.7 | 1405.5 | 0.11156 | 0.22308 | 1.3151 | 0.1119 | 0.02443 | 51.19 | 34.93 | 98.29 | 837.32 | 105.73 | 731.59 |
| 74 | 2788.2 | 1396.6 | 0.11319 | 0.22186 | 1.3177 | 0.1146 | 0.02489 | 51.27 | 34.92 | 98.90 | 847.71 | 105.70 | 742.00 |
| 75 | 2828.7 | 1384.1 | 0.11479 | 0.22064 | 1.3208 | 0.1176 | 0.02535 | 51.18 | 34.86 | 99.45 | 857.24 | 105.29 | 751.94 |
| 76 | 2869.6 | 1371.9 | 0.11643 | 0.21820 | 1.3241 | 0.1210 | 0.02583 | 51.20 | 34.82 | 99.98 | 866.35 | 105.08 | 761.28 |
| 77 | 2910.4 | 1358.6 | 0.11808 | 0.21607 | 1.3267 | 0.1236 | 0.02630 | 50.95 | 34.70 | 100.58 | 876.67 | 104.35 | 772.32 |
| 78 | 2951.9 | 1344.8 | 0.11970 | 0.21393 | 1.3306 | 0.1275 | 0.02679 | 50.97 | 34.66 | 101.02 | 884.46 | 104.11 | 780.35 |
| 79 | 2993.4 | 1331.2 | 0.12131 | 0.21179 | 1.3334 | 0.1303 | 0.02726 | 50.74 | 34.54 | 101.56 | 893.87 | 103.39 | 790.48 |
| 80 | 3035.2 | 1320.7 | 0.12288 | 0.21027 | 1.3373 | 0.1341 | 0.02773 | 51.00 | 34.59 | 101.95 | 900.87 | 103.67 | 797.20 |
| 81 | 3077.7 | 1308.8 | 0.12452 | 0.20904 | 1.3402 | 0.1371 | 0.02822 | 50.91 | 34.52 | 102.47 | 910.00 | 103.26 | 806.74 |
| 82 | 3120.2 | 1298.7 | 0.12613 | 0.20691 | 1.3435 | 0.1403 | 0.02869 | 51.04 | 34.52 | 102.93 | 918.16 | 103.29 | 814.86 |
| 83 | 3163.1 | 1283.4 | 0.12773 | 0.20447 | 1.3471 | 0.1440 | 0.02919 | 50.89 | 34.42 | 103.34 | 925.45 | 102.69 | 822.76 |
| 84 | 3206.2 | 1274.9 | 0.12934 | 0.20325 | 1.3505 | 0.1474 | 0.02967 | 51.17 | 34.48 | 103.76 | 933.08 | 103.03 | 830.05 |
| 85 | 3249.9 | 1263.3 | 0.13091 | 0.20172 | 1.3541 | 0.1510 | 0.03015 | 51.26 | 34.47 | 104.14 | 939.98 | 102.95 | 837.03 |
| 86 | 3293.9 | 1258.7 | 0.13250 | 0.20142 | 1.3566 | 0.1535 | 0.03061 | 51.60 | 34.55 | 104.64 | 948.93 | 103.48 | 845.45 |
| 87 | 3338.2 | 1250.5 | 0.13410 | 0.20050 | 1.3581 | 0.1550 | 0.03107 | 51.38 | 34.46 | 105.23 | 959.75 | 102.90 | 856.86 |
| 88 | 3382.4 | 1240.5 | 0.13569 | 0.19867 | 1.3611 | 0.1580 | 0.03156 | 51.45 | 34.44 | 105.66 | 967.54 | 102.80 | 864.74 |
| 89 | 3427.2 | 1228.0 | 0.13728 | 0.19714 | 1.3642 | 0.1610 | 0.03205 | 51.32 | 34.36 | 106.07 | 975.07 | 102.30 | 872.77 |
| 90 | 3472.1 | 1208.8 | 0.13885 | 0.19348 | 1.3678 | 0.1647 | 0.03256 | 50.81 | 34.13 | 106.40 | 981.18 | 100.95 | 880.23 |
| 91 | 3517.7 | 1201.6 | 0.14047 | 0.19287 | 1.3716 | 0.1685 | 0.03306 | 51.30 | 34.25 | 106.73 | 987.17 | 101.69 | 885.48 |
| 92 | 3563.6 | 1190.6 | 0.14207 | 0.19073 | 1.3745 | 0.1714 | 0.03355 | 51.24 | 34.19 | 107.13 | 994.66 | 101.34 | 893.32 |
| 93 | 3609.6 | 1176.2 | 0.14367 | 0.18921 | 1.3785 | 0.1754 | 0.03407 | 51.21 | 34.13 | 107.41 | 999.80 | 100.95 | 898.85 |
| 94 | 3656.2 | 1168.5 | 0.14527 | 0.18860 | 1.3815 | 0.1783 | 0.03457 | 51.42 | 34.16 | 107.80 | 1007.10 | 101.16 | 905.95 |
| 95 | 3702.9 | 1145.6 | 0.14689 | 0.18494 | 1.3852 | 0.1821 | 0.03511 | 50.58 | 33.82 | 108.09 | 1012.65 | 99.14 | 913.51 |
| 96 | 3750.4 | 1137.8 | 0.14848 | 0.18311 | 1.3883 | 0.1852 | 0.03561 | 50.82 | 33.86 | 108.44 | 1019.08 | 99.39 | 919.69 |
| 97 | 3798.2 | 1129.3 | 0.15009 | 0.18189 | 1.3907 | 0.1876 | 0.03610 | 50.79 | 33.82 | 108.86 | 1027.05 | 99.14 | 927.91 |
| 98 | 3846.2 | 1117.6 | 0.15167 | 0.18005 | 1.3942 | 0.1910 | 0.03662 | 50.79 | 33.78 | 109.15 | 1032.48 | 98.87 | 933.62 |
| 99 | 3894.7 | 1097.6 | 0.15331 | 0.17761 | 1.3979 | 0.1948 | 0.03718 | 50.14 | 33.50 | 109.42 | 1037.64 | 97.27 | 940.37 |
| 100 | 3943.7 | 1087.7 | 0.15488 | 0.17609 | 1.4008 | 0.1977 | 0.03768 | 50.13 | 33.46 | 109.74 | 1043.70 | 97.02 | 946.68 |

Elastic-Plastic Fracture Toughness Analysis

| | | | |
|----------------|--------------|---------------|------|
| Specimen ID | 5086-FT-3 | Geometry | C(T) |
| Contract | SSC 10624-01 | Orientation | T-L |
| Material | 5086-H116 | Yield (ksi) | 27.0 |
| Temperature(F) | 75.0 | Tensile (ksi) | 46.0 |
| Environment | LAB AIR | Modulus (Msi) | 10.5 |

Specimen Dimensions

| | | | |
|--------------------|-------|------------------|-------|
| Thickness (in) | 0.496 | Notch Depth (in) | 1.100 |
| Net Thickness (in) | 0.396 | Gage Length (in) | 0.200 |
| Width (in) | 2.000 | Alpha Ratio | 1 |
| Pin Spacing (in) | 1.100 | | |

Precrack Parameters

| | | | |
|--------------|-------|----------------------|-----|
| Pmax (lbf) | 308.0 | Stress Ratio | 0.1 |
| Final a (in) | 1.200 | Kmax (ksi sqrt (in)) | 6.1 |
| Pf (lbf) | 872 | | |

Initial measured crack lengths (in)

| | | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 1.187 | 1.204 | 1.208 | 1.207 | 1.210 | 1.213 | 1.215 | 1.213 | 1.207 |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|

Final measured crack lengths (in)

| | | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 1.419 | 1.424 | 1.429 | 1.416 | 1.409 | 1.418 | 1.415 | 1.418 | 1.416 |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|

| | | | |
|--------------------------------|-------|-------------------------|-------|
| Ave. initial crack length (in) | 1.208 | aoq (in) | 1.207 |
| Ave. final crack length (in) | 1.418 | Compliance Adj. Factor | 1.017 |
| Delta a measured (in) | 0.210 | Effective Modulus (Msi) | 10.7 |
| Delta a predicted (in) | 0.199 | | |

Results

| | |
|---|------------------------------|
| J _a (E1820) | 155.2 lbf-in/in ² |
| K _{JIC} (E**JQ) ^{1/2} | 42.3 ksi sqrt(in) |

Qualification of Data

| | |
|---|-------|
| 7.4.2: precrack length | valid |
| 9.1.4.1; precrack | valid |
| 9.1.4.2; final crack | valid |
| 9.1.5.1; Δa meas | valid |
| 9.1.5.2; Δa pred | valid |
| A9.6.4; # of pnts in reg.A | valid |
| A9.6.4; # of pnts in reg.B | valid |
| A9.8.1; C ₂ <1 | valid |
| A9.8.2.1; a _{0a} -a ₀ | valid |
| A9.8.2.2; # of pnts for J _a | valid |
| A9.8.2.2; # of pnts < J _a | valid |
| A9.3.3.1; correlation | valid |

Qualification of J_a as J_{IC}

| | |
|-------------------|-------|
| A9.9.1; thickness | valid |
| A9.9.2; ligament | valid |
| A9.9.3; slope | valid |

| Index | Time | Force | Disp1 | Disp2 | Crack | Δa | CTOD | K561 | K1820 | KJ1820 | J1820 | Je | Jpl |
|-------|--------|--------|---------|---------|--------|---------|---------|-------------|-------------|-------------|--------|--------|--------|
| | Sec | lbf | inch | inch | inch | inch | inch | ksi sqr(in) | ksi sqr(in) | ksi sqr(in) | lbf/in | lbf/in | lbf/in |
| 10 | 342.7 | 304.1 | 0.00366 | 0.04822 | 1.2084 | 0.0011 | 0.00002 | 6.81 | 6.73 | 6.75 | 3.95 | 3.93 | 0.02 |
| 11 | 385.4 | 385.6 | 0.00471 | 0.06103 | 1.2080 | 0.0007 | 0.00007 | 8.68 | 8.53 | 8.57 | 6.36 | 6.31 | 0.05 |
| 12 | 418.3 | 464.9 | 0.00577 | 0.07294 | 1.2080 | 0.0007 | 0.00013 | 10.55 | 10.29 | 10.39 | 9.36 | 9.17 | 0.19 |
| 13 | 450.6 | 544.6 | 0.00682 | 0.08575 | 1.2071 | -0.0002 | 0.00021 | 12.45 | 12.03 | 12.21 | 12.91 | 12.54 | 0.37 |
| 14 | 481.3 | 619.2 | 0.00787 | 0.09766 | 1.2065 | -0.0008 | 0.00030 | 14.29 | 13.66 | 14.02 | 17.02 | 16.18 | 0.85 |
| 15 | 511.8 | 695.3 | 0.00894 | 0.10956 | 1.2079 | 0.0006 | 0.00040 | 16.29 | 15.38 | 15.80 | 21.65 | 20.51 | 1.14 |
| 16 | 542.1 | 766.5 | 0.00998 | 0.12085 | 1.2068 | -0.0005 | 0.00052 | 18.13 | 16.92 | 17.60 | 26.85 | 24.81 | 2.04 |
| 17 | 571.8 | 836.3 | 0.01105 | 0.13214 | 1.2073 | 0.0000 | 0.00064 | 20.08 | 18.48 | 19.37 | 32.52 | 29.60 | 2.92 |
| 18 | 601.6 | 904.2 | 0.01211 | 0.14282 | 1.2081 | 0.0008 | 0.00078 | 22.08 | 20.01 | 21.13 | 38.71 | 34.72 | 4.00 |
| 19 | 631.1 | 969.8 | 0.01318 | 0.15350 | 1.2082 | 0.0008 | 0.00093 | 24.05 | 21.47 | 22.89 | 45.41 | 39.94 | 5.47 |
| 20 | 660.5 | 1031.7 | 0.01425 | 0.16296 | 1.2064 | -0.0010 | 0.00110 | 25.86 | 22.75 | 24.70 | 52.87 | 44.87 | 8.00 |
| 21 | 689.5 | 1088.6 | 0.01532 | 0.17212 | 1.2083 | 0.0010 | 0.00126 | 27.85 | 24.10 | 26.38 | 60.32 | 50.34 | 9.98 |
| 22 | 718.6 | 1142.0 | 0.01639 | 0.17944 | 1.2071 | -0.0002 | 0.00145 | 29.57 | 25.23 | 28.13 | 68.60 | 55.15 | 13.46 |
| 23 | 747.3 | 1191.7 | 0.01748 | 0.18738 | 1.2090 | 0.0017 | 0.00164 | 31.51 | 26.42 | 29.80 | 76.97 | 60.51 | 16.45 |
| 24 | 775.8 | 1236.6 | 0.01857 | 0.19501 | 1.2101 | 0.0028 | 0.00184 | 33.28 | 27.48 | 31.47 | 85.84 | 65.43 | 20.41 |
| 25 | 804.3 | 1277.0 | 0.01966 | 0.20111 | 1.2102 | 0.0029 | 0.00205 | 34.85 | 28.38 | 33.14 | 95.19 | 69.81 | 25.37 |
| 26 | 832.6 | 1313.6 | 0.02074 | 0.20691 | 1.2102 | 0.0029 | 0.00226 | 36.31 | 29.19 | 34.78 | 104.86 | 73.87 | 31.00 |
| 27 | 860.8 | 1347.7 | 0.02185 | 0.21240 | 1.2108 | 0.0035 | 0.00248 | 37.80 | 29.99 | 36.41 | 114.92 | 77.94 | 36.99 |
| 28 | 888.8 | 1375.7 | 0.02296 | 0.21698 | 1.2119 | 0.0045 | 0.00271 | 39.13 | 30.68 | 37.99 | 125.06 | 81.56 | 43.51 |
| 29 | 916.8 | 1399.5 | 0.02406 | 0.22125 | 1.2136 | 0.0063 | 0.00294 | 40.42 | 31.31 | 39.51 | 135.31 | 84.98 | 50.33 |
| 30 | 945 | 1420.4 | 0.02517 | 0.22308 | 1.2151 | 0.0077 | 0.00317 | 41.59 | 31.88 | 41.02 | 145.80 | 88.06 | 57.74 |
| 31 | 973 | 1433.9 | 0.02628 | 0.22491 | 1.2179 | 0.0105 | 0.00340 | 42.65 | 32.36 | 42.44 | 156.10 | 90.75 | 65.35 |
| 32 | 1000.8 | 1448.1 | 0.02739 | 0.22736 | 1.2205 | 0.0132 | 0.00364 | 43.76 | 32.85 | 43.83 | 166.51 | 93.54 | 72.97 |
| 33 | 1028.7 | 1456.8 | 0.02848 | 0.22949 | 1.2231 | 0.0158 | 0.00387 | 44.63 | 33.23 | 45.17 | 176.85 | 95.69 | 81.17 |
| 34 | 1057 | 1467.7 | 0.02960 | 0.23132 | 1.2261 | 0.0188 | 0.00411 | 45.72 | 33.68 | 46.49 | 187.34 | 98.32 | 89.02 |
| 35 | 1085 | 1476.4 | 0.03071 | 0.23193 | 1.2286 | 0.0212 | 0.00436 | 46.61 | 34.05 | 47.81 | 198.10 | 100.48 | 97.62 |
| 36 | 1112.9 | 1472.2 | 0.03181 | 0.23193 | 1.2334 | 0.0261 | 0.00460 | 47.29 | 34.29 | 48.98 | 207.95 | 101.90 | 106.05 |
| 37 | 1141.1 | 1468.2 | 0.03292 | 0.23163 | 1.2382 | 0.0308 | 0.00484 | 47.99 | 34.53 | 50.12 | 217.74 | 103.36 | 114.38 |
| 38 | 1169.4 | 1451.9 | 0.03402 | 0.22858 | 1.2440 | 0.0367 | 0.00509 | 48.22 | 34.57 | 51.18 | 227.02 | 103.57 | 123.45 |
| 39 | 1198.2 | 1450.2 | 0.03515 | 0.22766 | 1.2499 | 0.0425 | 0.00534 | 49.32 | 34.96 | 52.22 | 236.34 | 105.90 | 130.45 |
| 40 | 1227.2 | 1437.4 | 0.03625 | 0.22644 | 1.2561 | 0.0488 | 0.00559 | 49.87 | 35.10 | 53.20 | 245.28 | 106.80 | 138.48 |
| 41 | 1256.5 | 1420.9 | 0.03739 | 0.22400 | 1.2613 | 0.0540 | 0.00586 | 49.97 | 35.09 | 54.24 | 254.99 | 106.70 | 148.29 |
| 42 | 1286 | 1400.3 | 0.03853 | 0.22003 | 1.2694 | 0.0621 | 0.00612 | 50.46 | 35.19 | 55.08 | 262.97 | 107.31 | 155.66 |
| 43 | 1316 | 1371.5 | 0.03974 | 0.21576 | 1.2780 | 0.0706 | 0.00641 | 50.53 | 35.11 | 55.96 | 271.40 | 106.87 | 164.53 |
| 44 | 1346.4 | 1330.7 | 0.04098 | 0.20935 | 1.2892 | 0.0818 | 0.00671 | 50.37 | 34.93 | 56.68 | 278.42 | 105.72 | 172.70 |
| 45 | 1377.4 | 1316.1 | 0.04210 | 0.20721 | 1.2962 | 0.0889 | 0.00698 | 51.02 | 35.09 | 57.45 | 286.07 | 106.71 | 179.36 |
| 46 | 1408.6 | 1282.5 | 0.04320 | 0.20264 | 1.3052 | 0.0979 | 0.00725 | 50.81 | 34.90 | 58.08 | 292.33 | 105.58 | 186.75 |
| 47 | 1441.1 | 1264.5 | 0.04431 | 0.19928 | 1.3133 | 0.1059 | 0.00752 | 51.49 | 35.06 | 58.72 | 298.80 | 106.51 | 192.29 |
| 48 | 1473.7 | 1243.9 | 0.04544 | 0.19531 | 1.3213 | 0.1140 | 0.00780 | 51.99 | 35.14 | 59.36 | 305.35 | 106.99 | 198.36 |
| 49 | 1506.6 | 1201.8 | 0.04653 | 0.18921 | 1.3303 | 0.1229 | 0.00810 | 51.01 | 34.67 | 59.90 | 310.95 | 104.19 | 206.76 |
| 50 | 1541.1 | 1185.5 | 0.04766 | 0.18677 | 1.3380 | 0.1306 | 0.00838 | 51.74 | 34.84 | 60.49 | 317.13 | 105.19 | 211.94 |
| 51 | 1575.2 | 1152.9 | 0.04874 | 0.18189 | 1.3471 | 0.1398 | 0.00867 | 51.52 | 34.64 | 60.93 | 321.79 | 104.02 | 217.77 |
| 52 | 1610.5 | 1114.7 | 0.04992 | 0.17578 | 1.3584 | 0.1511 | 0.00899 | 51.34 | 34.44 | 61.30 | 325.66 | 102.78 | 222.89 |
| 53 | 1647.2 | 1115.6 | 0.05103 | 0.17578 | 1.3622 | 0.1549 | 0.00926 | 52.51 | 34.79 | 62.04 | 333.59 | 104.91 | 228.68 |
| 54 | 1683.7 | 1084.6 | 0.05214 | 0.17090 | 1.3708 | 0.1635 | 0.00957 | 52.20 | 34.57 | 62.47 | 338.20 | 103.58 | 234.62 |
| 55 | 1721.1 | 1051.9 | 0.05327 | 0.16510 | 1.3801 | 0.1728 | 0.00988 | 51.88 | 34.34 | 62.83 | 342.18 | 102.18 | 240.00 |
| 56 | 1758.9 | 1008.3 | 0.05435 | 0.15869 | 1.3909 | 0.1836 | 0.01021 | 50.90 | 33.85 | 63.04 | 344.38 | 99.32 | 245.06 |
| 57 | 1798.6 | 988.5 | 0.05543 | 0.15564 | 1.3987 | 0.1914 | 0.01051 | 51.27 | 33.87 | 63.40 | 348.34 | 99.45 | 248.90 |
| 58 | 1838.9 | 957.8 | 0.05652 | 0.15198 | 1.4079 | 0.2006 | 0.01083 | 50.96 | 33.64 | 63.65 | 351.12 | 98.10 | 253.03 |

Elastic-Plastic Fracture Toughness Analysis

| | | | |
|----------------|--------------|---------------|------|
| Specimen ID | 5086-FT-5 | Geometry | C(T) |
| Contract | SSC 10624-01 | Orientation | T-L |
| Material | 5086-H116 | Yield (ksi) | 27.0 |
| Temperature(F) | 75.0 | Tensile (ksi) | 46.0 |
| Environment | LAB AIR | Modulus (Msi) | 10.5 |

Specimen Dimensions

| | | | |
|--------------------|-------|------------------|-------|
| Thickness (in) | 0.497 | Notch Depth (in) | 2.200 |
| Net Thickness (in) | 0.497 | Gage Length (in) | 0.200 |
| Width (in) | 4.000 | Alpha Ratio | 1 |
| Pin Spacing (in) | 2.200 | | |

Precrack Parameters

| | | | |
|--------------|-------|----------------------|-----|
| Pmax (lbf) | 727.0 | Stress Ratio | 0.1 |
| Final a (in) | 2.400 | Kmax (ksi sqrt (in)) | 9.9 |
| Pf (lbf) | 1811 | | |

Initial measured crack lengths (in)

2.362 2.387 2.401 2.406 2.405 2.401 2.390 2.372 2.343

Final measured crack lengths (in)

2.510 2.552 2.633 2.727 2.784
x

| | | | |
|--------------------------------|-------|-------------------------|-------|
| Ave. initial crack length (in) | 2.389 | aoq (in) | 2.389 |
| Ave. final crack length (in) | 2.624 | Compliance Adj. Factor | 0.991 |
| Delta a measured (in) | 0.234 | Effective Modulus (Msi) | 10.4 |
| Delta a predicted (in) | 0.218 | | |

Results

| | |
|--------------------------|------------------------------|
| J_a (E1820) | 201.0 lbf-in/in ² |
| $K_{JIC}(E^{*}JQ)^{1/2}$ | 48.2 ksi sqrt(in) |

Qualification of Data

| | |
|-------------------------------|---------|
| 7.4.2; precrack length | valid |
| 9.1.4.1; precrack | valid |
| 9.1.4.2; final crack | invalid |
| 9.1.5.1; Δa meas | valid |
| 9.1.5.2; Δa pred | valid |
| A9.6.4; # of pnts in reg.A | valid |
| A9.6.4; # of pnts in reg.B | valid |
| A9.8.1; $C_2 < 1$ | valid |
| A9.8.2.1; $a_{0a} - a_0$ | valid |
| A9.8.2.2; # of pnts for J_a | valid |
| A9.8.2.2; # of pnts $< J_a$ | valid |
| A9.3.3.1; correlation | valid |

Qualification of J_a as J_{IC}

| | |
|-------------------|-------|
| A9.9.1; thickness | valid |
| A9.9.2; ligament | valid |
| A9.9.3; slope | valid |

| Index | Time | Force | Disp1 | Disp2 | Crack | Δa | CTOD | K561 | K1820 | KJ1820 | J1820 | Je | Jpl |
|-------|--------|--------|---------|---------|--------|--------|---------|-------------|-------------|-------------|---------|--------|--------|
| | Sec | lbf | inch | inch | inch | inch | inch | ksi sqr(in) | ksi sqr(in) | ksi sqr(in) | lbf/in | lbf/in | lbf/in |
| 13 | 466.3 | 1883.2 | 0.02421 | 0.62164 | 2.3904 | 0.0013 | 0.00140 | 27.74 | 25.65 | 25.60 | 56.80 | 57.00 | -0.20 |
| 14 | 498.2 | 2016.1 | 0.02637 | 0.66681 | 2.3919 | 0.0027 | 0.00168 | 30.11 | 27.49 | 28.01 | 67.99 | 65.51 | 2.48 |
| 15 | 529.8 | 2141.9 | 0.02853 | 0.70343 | 2.3911 | 0.0019 | 0.00199 | 32.34 | 29.19 | 30.41 | 80.15 | 73.82 | 6.33 |
| 16 | 561.1 | 2259.8 | 0.03071 | 0.74554 | 2.3923 | 0.0031 | 0.00231 | 34.59 | 30.83 | 32.75 | 92.97 | 82.37 | 10.60 |
| 17 | 592.3 | 2368.8 | 0.03289 | 0.78369 | 2.3924 | 0.0033 | 0.00266 | 36.70 | 32.32 | 35.07 | 106.59 | 90.53 | 16.06 |
| 18 | 623.8 | 2467.5 | 0.03507 | 0.81177 | 2.3929 | 0.0038 | 0.00303 | 38.69 | 33.68 | 37.34 | 120.86 | 98.33 | 22.53 |
| 19 | 655 | 2560.1 | 0.03727 | 0.84503 | 2.3948 | 0.0057 | 0.00341 | 40.71 | 35.01 | 39.56 | 135.60 | 106.24 | 29.36 |
| 20 | 686.1 | 2641.9 | 0.03943 | 0.87128 | 2.3964 | 0.0073 | 0.00380 | 42.54 | 36.19 | 41.70 | 150.71 | 113.50 | 37.21 |
| 21 | 717.3 | 2716.4 | 0.04162 | 0.89752 | 2.3965 | 0.0074 | 0.00422 | 44.18 | 37.21 | 43.85 | 166.68 | 120.01 | 46.67 |
| 22 | 748.6 | 2785.9 | 0.04383 | 0.91736 | 2.3963 | 0.0072 | 0.00466 | 45.73 | 38.16 | 45.99 | 183.32 | 126.19 | 57.14 |
| 23 | 779.6 | 2842.1 | 0.04604 | 0.94116 | 2.3989 | 0.0097 | 0.00510 | 47.20 | 39.02 | 48.03 | 199.89 | 131.97 | 67.92 |
| 24 | 810.5 | 2895.8 | 0.04826 | 0.95551 | 2.4017 | 0.0125 | 0.00554 | 48.67 | 39.87 | 50.02 | 216.82 | 137.77 | 79.06 |
| 25 | 841.1 | 2943.3 | 0.05045 | 0.97198 | 2.4019 | 0.0128 | 0.00600 | 49.84 | 40.53 | 52.00 | 234.38 | 142.40 | 91.98 |
| 26 | 871.8 | 2985.4 | 0.05264 | 0.98419 | 2.4049 | 0.0158 | 0.00645 | 51.13 | 41.24 | 53.87 | 251.53 | 147.37 | 104.16 |
| 27 | 902.8 | 3024.4 | 0.05485 | 0.99640 | 2.4049 | 0.0157 | 0.00693 | 52.11 | 41.77 | 55.81 | 269.94 | 151.23 | 118.71 |
| 28 | 933.6 | 3059.2 | 0.05705 | 1.00952 | 2.4069 | 0.0178 | 0.00740 | 53.18 | 42.34 | 57.64 | 287.89 | 155.35 | 132.54 |
| 29 | 964.1 | 3089.4 | 0.05923 | 1.02020 | 2.4093 | 0.0202 | 0.00787 | 54.18 | 42.86 | 59.40 | 305.82 | 159.19 | 146.63 |
| 30 | 995.1 | 3116.5 | 0.06146 | 1.03332 | 2.4109 | 0.0218 | 0.00836 | 55.05 | 43.30 | 61.19 | 324.49 | 162.50 | 161.99 |
| 31 | 1025.9 | 3138.9 | 0.06365 | 1.03882 | 2.4119 | 0.0228 | 0.00885 | 55.75 | 43.66 | 62.94 | 343.31 | 165.17 | 178.15 |
| 32 | 1057 | 3165.3 | 0.06586 | 1.04523 | 2.4143 | 0.0252 | 0.00934 | 56.70 | 44.13 | 64.62 | 361.89 | 168.75 | 193.13 |
| 33 | 1087.7 | 3187.6 | 0.06804 | 1.05194 | 2.4150 | 0.0259 | 0.00983 | 57.39 | 44.47 | 66.29 | 380.89 | 171.37 | 209.52 |
| 34 | 1118.6 | 3207.3 | 0.07024 | 1.06445 | 2.4173 | 0.0281 | 0.01032 | 58.17 | 44.84 | 67.92 | 399.78 | 174.27 | 225.51 |
| 35 | 1149.4 | 3219.8 | 0.07245 | 1.06415 | 2.4205 | 0.0314 | 0.01082 | 58.87 | 45.16 | 69.48 | 418.37 | 176.77 | 241.60 |
| 36 | 1180.2 | 3237.6 | 0.07466 | 1.07391 | 2.4217 | 0.0326 | 0.01132 | 59.51 | 45.47 | 71.08 | 437.91 | 179.17 | 258.74 |
| 37 | 1211.1 | 3248.3 | 0.07684 | 1.08093 | 2.4230 | 0.0338 | 0.01182 | 59.96 | 45.68 | 72.63 | 457.17 | 180.81 | 276.36 |
| 38 | 1242 | 3252.9 | 0.07907 | 1.07269 | 2.4257 | 0.0365 | 0.01233 | 60.39 | 45.86 | 74.14 | 476.39 | 182.29 | 294.10 |
| 39 | 1273 | 3267.8 | 0.08127 | 1.08307 | 2.4271 | 0.0380 | 0.01284 | 61.00 | 46.14 | 75.65 | 495.97 | 184.51 | 311.46 |
| 40 | 1304 | 3275.6 | 0.08350 | 1.08612 | 2.4306 | 0.0414 | 0.01335 | 61.62 | 46.41 | 77.08 | 514.92 | 186.66 | 328.26 |
| 41 | 1334.9 | 3286.4 | 0.08571 | 1.08490 | 2.4307 | 0.0416 | 0.01387 | 61.97 | 46.57 | 78.59 | 535.25 | 187.96 | 347.29 |
| 42 | 1366 | 3291.5 | 0.08794 | 1.09222 | 2.4322 | 0.0431 | 0.01439 | 62.30 | 46.71 | 80.04 | 555.26 | 189.10 | 366.16 |
| 43 | 1397.1 | 3297.1 | 0.09015 | 1.08734 | 2.4341 | 0.0450 | 0.01491 | 62.69 | 46.88 | 81.44 | 574.85 | 190.48 | 384.37 |
| 44 | 1428.1 | 3297.7 | 0.09236 | 1.08795 | 2.4369 | 0.0478 | 0.01543 | 63.04 | 47.02 | 82.79 | 594.07 | 191.62 | 402.45 |
| 45 | 1459.2 | 3291.6 | 0.09457 | 1.08643 | 2.4404 | 0.0512 | 0.01595 | 63.26 | 47.10 | 84.09 | 612.79 | 192.25 | 420.54 |
| 46 | 1490.5 | 3290.4 | 0.09680 | 1.08734 | 2.4429 | 0.0537 | 0.01649 | 63.52 | 47.20 | 85.42 | 632.32 | 193.07 | 439.25 |
| 47 | 1522.1 | 3294.2 | 0.09902 | 1.09192 | 2.4452 | 0.0560 | 0.01701 | 63.92 | 47.36 | 86.72 | 651.71 | 194.43 | 457.28 |
| 48 | 1553.6 | 3292.4 | 0.10123 | 1.09344 | 2.4490 | 0.0598 | 0.01754 | 64.33 | 47.52 | 87.94 | 670.21 | 195.70 | 474.51 |
| 49 | 1585.1 | 3284.3 | 0.10346 | 1.08398 | 2.4524 | 0.0633 | 0.01808 | 64.49 | 47.57 | 89.17 | 689.11 | 196.12 | 493.00 |
| 50 | 1616.6 | 3276.5 | 0.10569 | 1.08612 | 2.4565 | 0.0673 | 0.01862 | 64.75 | 47.65 | 90.35 | 707.51 | 196.81 | 510.70 |
| 51 | 1648.4 | 3277.9 | 0.10794 | 1.08337 | 2.4584 | 0.0692 | 0.01916 | 65.03 | 47.77 | 91.62 | 727.45 | 197.74 | 529.71 |
| 52 | 1680.1 | 3281.9 | 0.11017 | 1.08337 | 2.4611 | 0.0720 | 0.01969 | 65.52 | 47.96 | 92.82 | 746.60 | 199.34 | 547.27 |
| 53 | 1712.2 | 3280.5 | 0.11240 | 1.08307 | 2.4651 | 0.0760 | 0.02023 | 65.99 | 48.13 | 93.95 | 764.92 | 200.80 | 564.12 |
| 54 | 1744.1 | 3272.1 | 0.11460 | 1.08276 | 2.4687 | 0.0796 | 0.02077 | 66.18 | 48.19 | 95.07 | 783.27 | 201.26 | 582.01 |
| 55 | 1776.1 | 3265.8 | 0.11681 | 1.08215 | 2.4735 | 0.0844 | 0.02131 | 66.60 | 48.33 | 96.12 | 800.74 | 202.48 | 598.26 |
| 56 | 1808.1 | 3260.6 | 0.11903 | 1.08520 | 2.4765 | 0.0874 | 0.02186 | 66.82 | 48.41 | 97.25 | 819.59 | 203.09 | 616.50 |
| 57 | 1840.5 | 3246.8 | 0.12126 | 1.07056 | 2.4819 | 0.0927 | 0.02242 | 67.06 | 48.47 | 98.25 | 836.68 | 203.62 | 633.06 |
| 58 | 1872.9 | 3237.6 | 0.12347 | 1.07544 | 2.4857 | 0.0965 | 0.02297 | 67.26 | 48.52 | 99.31 | 854.74 | 204.07 | 650.67 |
| 59 | 1905.2 | 3226.2 | 0.12571 | 1.07117 | 2.4901 | 0.1009 | 0.02353 | 67.46 | 48.58 | 100.33 | 872.47 | 204.51 | 667.96 |
| 60 | 1937.7 | 3217.2 | 0.12794 | 1.06506 | 2.4952 | 0.1061 | 0.02409 | 67.85 | 48.70 | 101.30 | 889.38 | 205.55 | 683.83 |
| 61 | 1970.5 | 3213.4 | 0.13016 | 1.06506 | 2.4990 | 0.1099 | 0.02464 | 68.25 | 48.84 | 102.31 | 907.24 | 206.73 | 700.51 |
| 62 | 2003.2 | 3197.6 | 0.13238 | 1.05408 | 2.5040 | 0.1148 | 0.02521 | 68.38 | 48.85 | 103.26 | 924.16 | 206.86 | 717.30 |
| 63 | 2036.1 | 3182.8 | 0.13461 | 1.05072 | 2.5072 | 0.1180 | 0.02579 | 68.28 | 48.79 | 104.29 | 942.58 | 206.33 | 736.25 |
| 64 | 2068.9 | 3166.2 | 0.13683 | 1.04858 | 2.5144 | 0.1252 | 0.02636 | 68.71 | 48.91 | 105.10 | 957.26 | 207.33 | 749.93 |
| 65 | 2102.4 | 3161.0 | 0.13907 | 1.04553 | 2.5178 | 0.1286 | 0.02693 | 69.01 | 49.01 | 106.08 | 975.30 | 208.14 | 767.16 |
| 66 | 2135.9 | 3146.2 | 0.14127 | 1.04279 | 2.5226 | 0.1334 | 0.02750 | 69.15 | 49.03 | 106.97 | 991.70 | 208.32 | 783.38 |
| 67 | 2169.6 | 3130.8 | 0.14348 | 1.03394 | 2.5284 | 0.1393 | 0.02808 | 69.43 | 49.09 | 107.80 | 1007.17 | 208.89 | 798.28 |
| 68 | 2203.4 | 3118.0 | 0.14569 | 1.03455 | 2.5332 | 0.1441 | 0.02866 | 69.66 | 49.15 | 108.67 | 1023.38 | 209.34 | 814.04 |

| Index | Time | Force | Disp1 | Disp2 | Crack | Δa | CTOD | K561 | K1820 | KJ1820 | J1820 | Je | Jpl |
|-------|--------|--------|---------|---------|--------|------------|---------|------------------------|------------------------|------------------------|---------|--------|---------|
| | Sec | lbf | inch | inch | inch | inch | inch | ksi $\sqrt{\text{in}}$ | ksi $\sqrt{\text{in}}$ | ksi $\sqrt{\text{in}}$ | lbf/in | lbf/in | lbf/in |
| 69 | 2237.2 | 3103.9 | 0.14789 | 1.02875 | 2.5358 | 0.1467 | 0.02923 | 69.49 | 49.06 | 109.63 | 1041.64 | 208.61 | 833.04 |
| 70 | 2271.2 | 3088.7 | 0.15012 | 1.01990 | 2.5427 | 0.1535 | 0.02982 | 69.93 | 49.18 | 110.38 | 1055.92 | 209.65 | 846.27 |
| 71 | 2305.2 | 3067.2 | 0.15229 | 1.01990 | 2.5467 | 0.1576 | 0.03041 | 69.69 | 49.06 | 111.23 | 1072.22 | 208.58 | 863.64 |
| 72 | 2339.4 | 3053.4 | 0.15452 | 1.01135 | 2.5519 | 0.1628 | 0.03100 | 69.95 | 49.12 | 112.03 | 1087.77 | 209.07 | 878.71 |
| 73 | 2373.9 | 3030.1 | 0.15677 | 0.99731 | 2.5582 | 0.1691 | 0.03161 | 69.97 | 49.08 | 112.78 | 1102.36 | 208.74 | 893.62 |
| 74 | 2408.7 | 3017.9 | 0.15900 | 1.00342 | 2.5630 | 0.1739 | 0.03221 | 70.23 | 49.14 | 113.58 | 1118.08 | 209.27 | 908.81 |
| 75 | 2443.6 | 2998.4 | 0.16124 | 0.99426 | 2.5682 | 0.1791 | 0.03282 | 70.24 | 49.10 | 114.36 | 1133.38 | 208.96 | 924.42 |
| 76 | 2478.6 | 2987.5 | 0.16347 | 0.98724 | 2.5729 | 0.1838 | 0.03342 | 70.54 | 49.18 | 115.14 | 1148.98 | 209.61 | 939.37 |
| 77 | 2513.9 | 2979.7 | 0.16572 | 0.98084 | 2.5773 | 0.1881 | 0.03401 | 70.92 | 49.29 | 115.94 | 1164.95 | 210.55 | 954.40 |
| 78 | 2549.1 | 2962.5 | 0.16793 | 0.98145 | 2.5818 | 0.1926 | 0.03462 | 70.91 | 49.25 | 116.71 | 1180.42 | 210.22 | 970.20 |
| 79 | 2584.4 | 2949.8 | 0.17013 | 0.97229 | 2.5881 | 0.1990 | 0.03522 | 71.42 | 49.39 | 117.35 | 1193.57 | 211.42 | 982.15 |
| 80 | 2620.2 | 2933.5 | 0.17234 | 0.96863 | 2.5931 | 0.2040 | 0.03583 | 71.53 | 49.39 | 118.08 | 1208.34 | 211.44 | 996.90 |
| 81 | 2655.9 | 2909.2 | 0.17455 | 0.96039 | 2.5987 | 0.2095 | 0.03646 | 71.39 | 49.29 | 118.75 | 1222.21 | 210.59 | 1011.62 |
| 82 | 2692.2 | 2895.2 | 0.17679 | 0.95306 | 2.6029 | 0.2138 | 0.03707 | 71.48 | 49.29 | 119.51 | 1237.82 | 210.58 | 1027.24 |
| 83 | 2728.7 | 2885.0 | 0.17899 | 0.95062 | 2.6080 | 0.2189 | 0.03768 | 71.90 | 49.41 | 120.18 | 1251.80 | 211.54 | 1040.26 |

Elastic-Plastic Fracture Toughness Analysis

| | | | |
|----------------|--------------|---------------|------|
| Specimen ID | 5383-FT-1 | Geometry | C(T) |
| Contract | SSC 10624-01 | Orientation | T-L |
| Material | 5383-H116 | Yield (ksi) | 35.4 |
| Temperature(F) | 75.0 | Tensile (ksi) | 53.3 |
| Environment | LAB AIR | Modulus (Msi) | 10.5 |

Specimen Dimensions

| | | | |
|--------------------|-------|------------------|-------|
| Thickness (in) | 0.487 | Notch Depth (in) | 1.100 |
| Net Thickness (in) | 0.487 | Gage Length (in) | 0.200 |
| Width (in) | 2.000 | Alpha Ratio | 1 |
| Pin Spacing (in) | 1.100 | | |

Precrack Parameters

| | | | |
|--------------|-------|----------------------|-----|
| Pmax (lbf) | 303.0 | Stress Ratio | 0.1 |
| Final a (in) | 1.200 | Kmax (ksi sqrt (in)) | 6.0 |
| Pf (lbf) | 1060 | | |

Initial measured crack lengths (in)

| | | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 1.194 | 1.209 | 1.214 | 1.210 | 1.208 | 1.205 | 1.198 | 1.184 | 1.171 |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|

Final measured crack lengths (in)

| | | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 1.303 | 1.349 | 1.482 | 1.592 | 1.630 | 1.544 | 1.426 | 1.332 | 1.326 |
| x | x | | x | x | x | | x | x |

| | | | |
|--------------------------------|-------|-------------------------|-------|
| Ave. initial crack length (in) | 1.201 | aoq (in) | n/a |
| Ave. final crack length (in) | 1.459 | Compliance Adj. Factor | 1.003 |
| Delta a measured (in) | 0.258 | Effective Modulus (Msi) | 10.5 |
| Delta a predicted (in) | 0.204 | | |

Results

| | |
|------------------------|-----------------------------|
| J_a (E1820) | 86.6 lbf-in/in ² |
| $K_{JIC}(E^*JQ)^{1/2}$ | 31.6 ksi sqrt(in) |

Qualification of Data

| | |
|-------------------------------|---------|
| 7.4.2: precrack length | valid |
| 9.1.4.1; precrack | valid |
| 9.1.4.2; final crack | invalid |
| 9.1.5.1; Δa meas | valid |
| 9.1.5.2; Δa pred | invalid |
| A9.6.4; # of pnts in reg.A | valid |
| A9.6.4; # of pnts in reg.B | valid |
| A9.8.1; $C_2 < 1$ | valid |
| A9.8.2.1; $a_{0q} - a_0$ | #VALUE! |
| A9.8.2.2; # of pnts for J_a | valid |
| A9.8.2.2; # of pnts $< J_a$ | valid |
| A9.3.3.1; correlation | valid |

Qualification of J_a as J_{IC}

| | |
|-------------------|-------|
| A9.9.1; thickness | valid |
| A9.9.2; ligament | valid |
| A9.9.3; slope | valid |

| Index | Time | Force | Disp1 | Disp2 | Crack | Δa | CTOD | K561 | K1820 | KJ1820 | J1820 | Je | Jpl |
|-------|--------|--------|---------|---------|--------|---------|---------|-------------|-------------|-------------|--------|--------|--------|
| | Sec | lbf | inch | inch | inch | inch | inch | ksi sqr(in) | ksi sqr(in) | ksi sqr(in) | lbf/in | lbf/in | lbf/in |
| 6 | 330.8 | 476.7 | 0.00582 | 0.07477 | 1.2014 | 0.0000 | 0.00009 | 9.62 | 9.48 | 9.48 | 7.79 | 7.79 | 0.01 |
| 7 | 371.7 | 597.2 | 0.00736 | 0.09369 | 1.2010 | -0.0004 | 0.00017 | 12.14 | 11.87 | 11.95 | 12.39 | 12.20 | 0.18 |
| 8 | 410.7 | 716.7 | 0.00891 | 0.11292 | 1.2018 | 0.0004 | 0.00025 | 14.74 | 14.26 | 14.41 | 18.00 | 17.63 | 0.37 |
| 9 | 448.8 | 831.9 | 0.01046 | 0.13092 | 1.2026 | 0.0012 | 0.00036 | 17.34 | 16.58 | 16.85 | 24.60 | 23.83 | 0.77 |
| 10 | 486.3 | 945.3 | 0.01202 | 0.14893 | 1.2018 | 0.0004 | 0.00050 | 19.92 | 18.81 | 19.31 | 32.33 | 30.67 | 1.66 |
| 11 | 523.5 | 1053.5 | 0.01358 | 0.16602 | 1.2025 | 0.0011 | 0.00065 | 22.56 | 20.99 | 21.74 | 40.95 | 38.19 | 2.76 |
| 12 | 560.3 | 1158.8 | 0.01514 | 0.18219 | 1.2026 | 0.0012 | 0.00082 | 25.21 | 23.09 | 24.14 | 50.50 | 46.22 | 4.28 |
| 13 | 596.8 | 1257.3 | 0.01669 | 0.19806 | 1.2041 | 0.0027 | 0.00100 | 27.90 | 25.13 | 26.48 | 60.78 | 54.74 | 6.04 |
| 14 | 633.1 | 1350.1 | 0.01825 | 0.21362 | 1.2046 | 0.0032 | 0.00121 | 30.51 | 27.01 | 28.83 | 72.03 | 63.25 | 8.79 |
| 15 | 669 | 1434.8 | 0.01981 | 0.22553 | 1.2054 | 0.0040 | 0.00144 | 33.03 | 28.75 | 31.15 | 84.11 | 71.65 | 12.47 |
| 16 | 704.3 | 1493.8 | 0.02139 | 0.23498 | 1.2090 | 0.0076 | 0.00169 | 35.17 | 30.15 | 33.36 | 96.46 | 78.79 | 17.67 |
| 17 | 739.8 | 1553.5 | 0.02295 | 0.24475 | 1.2128 | 0.0114 | 0.00194 | 37.49 | 31.60 | 35.49 | 109.15 | 86.51 | 22.64 |
| 18 | 774.8 | 1574.3 | 0.02454 | 0.24750 | 1.2209 | 0.0195 | 0.00221 | 39.12 | 32.54 | 37.44 | 121.51 | 91.76 | 29.74 |
| 19 | 810.1 | 1603.1 | 0.02610 | 0.25238 | 1.2263 | 0.0249 | 0.00250 | 40.82 | 33.50 | 39.39 | 134.48 | 97.28 | 37.20 |
| 20 | 845.8 | 1617.0 | 0.02770 | 0.25574 | 1.2321 | 0.0307 | 0.00281 | 42.12 | 34.20 | 41.30 | 147.79 | 101.35 | 46.44 |
| 21 | 881.5 | 1636.1 | 0.02930 | 0.25757 | 1.2356 | 0.0342 | 0.00313 | 43.34 | 34.85 | 43.24 | 162.03 | 105.24 | 56.78 |
| 22 | 917.6 | 1656.8 | 0.03087 | 0.26001 | 1.2385 | 0.0371 | 0.00345 | 44.59 | 35.50 | 45.10 | 176.26 | 109.22 | 67.04 |
| 23 | 953.8 | 1666.4 | 0.03248 | 0.26459 | 1.2419 | 0.0405 | 0.00380 | 45.52 | 35.96 | 46.92 | 190.83 | 112.08 | 78.75 |
| 24 | 990 | 1687.5 | 0.03407 | 0.26489 | 1.2446 | 0.0432 | 0.00413 | 46.85 | 36.62 | 48.71 | 205.62 | 116.24 | 89.38 |
| 25 | 1026.1 | 1682.3 | 0.03566 | 0.26489 | 1.2480 | 0.0466 | 0.00449 | 47.19 | 36.77 | 50.41 | 220.20 | 117.16 | 103.03 |
| 26 | 1063 | 1696.6 | 0.03725 | 0.26672 | 1.2504 | 0.0490 | 0.00484 | 48.24 | 37.27 | 52.10 | 235.24 | 120.38 | 114.86 |
| 27 | 1099.2 | 1698.2 | 0.03884 | 0.26733 | 1.2536 | 0.0522 | 0.00519 | 48.89 | 37.55 | 53.71 | 249.98 | 122.23 | 127.75 |
| 28 | 1136.1 | 1706.4 | 0.04044 | 0.26886 | 1.2551 | 0.0537 | 0.00556 | 49.54 | 37.86 | 55.36 | 265.62 | 124.21 | 141.41 |
| 29 | 1172.7 | 1708.2 | 0.04204 | 0.26855 | 1.2576 | 0.0562 | 0.00593 | 50.10 | 38.10 | 56.92 | 280.82 | 125.81 | 155.01 |
| 30 | 1209.6 | 1708.7 | 0.04365 | 0.26764 | 1.2603 | 0.0588 | 0.00630 | 50.64 | 38.33 | 58.44 | 295.98 | 127.32 | 168.66 |
| 31 | 1246.6 | 1704.1 | 0.04527 | 0.26917 | 1.2628 | 0.0614 | 0.00669 | 50.93 | 38.44 | 59.94 | 311.41 | 128.03 | 183.38 |
| 32 | 1283.4 | 1699.4 | 0.04686 | 0.26703 | 1.2651 | 0.0637 | 0.00707 | 51.15 | 38.52 | 61.38 | 326.55 | 128.56 | 197.99 |
| 33 | 1320.6 | 1698.3 | 0.04845 | 0.26581 | 1.2671 | 0.0657 | 0.00745 | 51.52 | 38.66 | 62.80 | 341.77 | 129.53 | 212.24 |
| 34 | 1357.9 | 1685.9 | 0.05005 | 0.26520 | 1.2697 | 0.0683 | 0.00785 | 51.43 | 38.59 | 64.16 | 356.73 | 129.09 | 227.64 |
| 35 | 1395.4 | 1678.0 | 0.05163 | 0.26459 | 1.2721 | 0.0707 | 0.00824 | 51.53 | 38.61 | 65.47 | 371.51 | 129.20 | 242.30 |
| 36 | 1433.1 | 1665.2 | 0.05324 | 0.26215 | 1.2755 | 0.0741 | 0.00864 | 51.58 | 38.60 | 66.72 | 385.83 | 129.13 | 256.70 |
| 37 | 1470.9 | 1654.2 | 0.05483 | 0.26032 | 1.2792 | 0.0778 | 0.00903 | 51.80 | 38.66 | 67.89 | 399.50 | 129.52 | 269.97 |
| 38 | 1509 | 1638.5 | 0.05645 | 0.25726 | 1.2819 | 0.0805 | 0.00945 | 51.57 | 38.52 | 69.12 | 414.06 | 128.61 | 285.45 |
| 39 | 1546.9 | 1615.0 | 0.05804 | 0.25513 | 1.2840 | 0.0826 | 0.00987 | 50.79 | 38.14 | 70.33 | 428.72 | 126.09 | 302.62 |
| 40 | 1585.6 | 1610.4 | 0.05964 | 0.25360 | 1.2884 | 0.0869 | 0.01026 | 51.47 | 38.41 | 71.36 | 441.28 | 127.85 | 313.44 |
| 41 | 1624.5 | 1598.8 | 0.06122 | 0.25146 | 1.2917 | 0.0903 | 0.01066 | 51.58 | 38.42 | 72.41 | 454.44 | 127.92 | 326.52 |
| 42 | 1663.5 | 1581.6 | 0.06281 | 0.24841 | 1.2944 | 0.0930 | 0.01108 | 51.23 | 38.23 | 73.50 | 468.23 | 126.68 | 341.56 |
| 43 | 1702.7 | 1566.8 | 0.06441 | 0.24597 | 1.2982 | 0.0968 | 0.01150 | 51.27 | 38.21 | 74.48 | 480.78 | 126.51 | 354.27 |
| 44 | 1742.4 | 1528.5 | 0.06611 | 0.24078 | 1.3028 | 0.1014 | 0.01199 | 50.18 | 37.66 | 75.47 | 493.57 | 122.90 | 370.67 |
| 45 | 1782.5 | 1518.3 | 0.06768 | 0.23834 | 1.3065 | 0.1051 | 0.01239 | 50.42 | 37.73 | 76.36 | 505.37 | 123.37 | 382.00 |
| 46 | 1822.6 | 1491.8 | 0.06928 | 0.23498 | 1.3123 | 0.1109 | 0.01284 | 50.20 | 37.57 | 77.12 | 515.48 | 122.30 | 393.17 |
| 47 | 1863.1 | 1457.2 | 0.07084 | 0.22888 | 1.3188 | 0.1174 | 0.01329 | 49.67 | 37.25 | 77.77 | 524.12 | 120.27 | 403.85 |
| 48 | 1904.6 | 1445.9 | 0.07242 | 0.22766 | 1.3212 | 0.1198 | 0.01372 | 49.56 | 37.17 | 78.70 | 536.74 | 119.75 | 416.99 |
| 49 | 1946.2 | 1414.8 | 0.07405 | 0.22400 | 1.3279 | 0.1265 | 0.01419 | 49.23 | 36.95 | 79.31 | 545.19 | 118.32 | 426.87 |
| 50 | 1988.5 | 1395.1 | 0.07562 | 0.22034 | 1.3329 | 0.1314 | 0.01463 | 49.18 | 36.87 | 80.00 | 554.60 | 117.81 | 436.79 |
| 51 | 2031.4 | 1373.0 | 0.07729 | 0.21607 | 1.3377 | 0.1363 | 0.01510 | 48.95 | 36.71 | 80.73 | 564.79 | 116.80 | 447.98 |
| 52 | 2074.7 | 1351.2 | 0.07889 | 0.21271 | 1.3437 | 0.1423 | 0.01556 | 48.96 | 36.65 | 81.31 | 572.91 | 116.42 | 456.49 |
| 53 | 2118.6 | 1325.7 | 0.08048 | 0.20843 | 1.3486 | 0.1472 | 0.01603 | 48.53 | 36.40 | 81.94 | 581.83 | 114.81 | 467.01 |
| 54 | 2163.2 | 1312.6 | 0.08205 | 0.20660 | 1.3527 | 0.1513 | 0.01647 | 48.63 | 36.40 | 82.60 | 591.33 | 114.82 | 476.51 |
| 55 | 2208.1 | 1297.0 | 0.08362 | 0.20416 | 1.3580 | 0.1566 | 0.01692 | 48.85 | 36.44 | 83.15 | 599.18 | 115.08 | 484.10 |
| 56 | 2253.7 | 1275.9 | 0.08525 | 0.20294 | 1.3626 | 0.1612 | 0.01740 | 48.57 | 36.26 | 83.78 | 608.27 | 113.95 | 494.32 |
| 57 | 2299.7 | 1258.6 | 0.08685 | 0.19928 | 1.3672 | 0.1658 | 0.01787 | 48.52 | 36.18 | 84.36 | 616.81 | 113.47 | 503.33 |
| 58 | 2346.2 | 1237.9 | 0.08842 | 0.19562 | 1.3721 | 0.1707 | 0.01834 | 48.32 | 36.04 | 84.88 | 624.43 | 112.56 | 511.87 |
| 59 | 2393.4 | 1217.0 | 0.08998 | 0.19287 | 1.3764 | 0.1750 | 0.01882 | 47.95 | 35.82 | 85.44 | 632.64 | 111.20 | 521.44 |
| 60 | 2441.4 | 1200.9 | 0.09161 | 0.18982 | 1.3810 | 0.1796 | 0.01930 | 47.95 | 35.77 | 85.97 | 640.60 | 110.88 | 529.72 |
| 61 | 2489.9 | 1184.4 | 0.09323 | 0.18677 | 1.3854 | 0.1840 | 0.01979 | 47.87 | 35.68 | 86.52 | 648.74 | 110.35 | 538.39 |
| 62 | 2538.9 | 1152.2 | 0.09485 | 0.18280 | 1.3912 | 0.1898 | 0.02033 | 47.05 | 35.24 | 86.92 | 654.78 | 107.64 | 547.14 |
| 63 | 2588.7 | 1137.7 | 0.09644 | 0.18097 | 1.3962 | 0.1948 | 0.02080 | 47.22 | 35.26 | 87.34 | 661.15 | 107.77 | 553.38 |
| 64 | 2639.2 | 1113.1 | 0.09810 | 0.17731 | 1.4016 | 0.2002 | 0.02134 | 46.78 | 35.00 | 87.76 | 667.46 | 106.16 | 561.29 |
| 65 | 2690.9 | 1099.6 | 0.09970 | 0.17425 | 1.4050 | 0.2036 | 0.02183 | 46.63 | 34.89 | 88.31 | 675.86 | 105.50 | 570.36 |

Elastic-Plastic Fracture Toughness Analysis

| | | | |
|----------------|--------------|---------------|------|
| Specimen ID | 5383-FT-2 | Geometry | C(T) |
| Contract | SSC 10624-01 | Orientation | T-L |
| Material | 5383-H116 | Yield (ksi) | 35.4 |
| Temperature(F) | 75.0 | Tensile (ksi) | 53.3 |
| Environment | LAB AIR | Modulus (Msi) | 10.5 |

Specimen Dimensions

| | | | |
|--------------------|-------|------------------|-------|
| Thickness (in) | 0.487 | Notch Depth (in) | 1.100 |
| Net Thickness (in) | 0.487 | Gage Length (in) | 0.200 |
| Width (in) | 2.000 | Alpha Ratio | 1 |
| Pin Spacing (in) | 1.100 | | |

Precrack Parameters

| | | | |
|--------------|-------|----------------------|-----|
| Pmax (lbf) | 302.0 | Stress Ratio | 0.1 |
| Final a (in) | 1.200 | Kmax (ksi sqrt (in)) | 6.0 |
| Pf (lbf) | 1057 | | |

Initial measured crack lengths (in)

1.197 1.211 1.215 1.212 1.208 1.205 1.199 1.186 1.172

Final measured crack lengths (in)

1.301 1.371 1.500 1.629 1.652 1.558 1.408 1.320 1.291
x x x x x x x

| | | | |
|--------------------------------|-------|-------------------------|-------|
| Ave. initial crack length (in) | 1.202 | aoq (in) | n/a |
| Ave. final crack length (in) | 1.467 | Compliance Adj. Factor | 1.009 |
| Delta a measured (in) | 0.264 | Effective Modulus (Msi) | 10.6 |
| Delta a predicted (in) | 0.206 | | |

Results

| | |
|-------------------------|-----------------------------|
| J_Q (E1820) | 86.1 lbf-in/in ² |
| $K_{JIC}(E^*J_Q)^{1/2}$ | 31.5 ksi sqrt(in) |

Qualification of Data

| | |
|-------------------------------|---------|
| 7.4.2; precrack length | valid |
| 9.1.4.1; precrack | valid |
| 9.1.4.2; final crack | invalid |
| 9.1.5.1; Δa meas | invalid |
| 9.1.5.2; Δa pred | invalid |
| A9.6.4; # of pnts in reg.A | valid |
| A9.6.4; # of pnts in reg.B | valid |
| A9.8.1; $C_2 < 1$ | valid |
| A9.8.2.1; $a_{0q} - a_0$ | #VALUE! |
| A9.8.2.2; # of pnts for J_Q | valid |
| A9.8.2.2; # of pnts < J_Q | valid |
| A9.3.3.1; correlation | valid |

Qualification of J_Q as J_{IC}

| | |
|-------------------|-------|
| A9.9.1; thickness | valid |
| A9.9.2; ligament | valid |
| A9.9.3; slope | valid |

| Index | Time | Force | Disp1 | Disp2 | Crack | Δa | CTOD | K561 | K1820 | KJ1820 | J1820 | Je | Jpl |
|-------|--------|--------|---------|---------|--------|------------|---------|-------------|-------------|-------------|--------|--------|--------|
| | Sec | lbf | inch | inch | inch | inch | inch | ksi sqr(in) | ksi sqr(in) | ksi sqr(in) | lbf/in | lbf/in | lbf/in |
| 8 | 417.2 | 477.1 | 0.00571 | 0.07568 | 1.2027 | 0.0000 | 0.00007 | 9.64 | 9.50 | 9.51 | 7.84 | 7.83 | 0.02 |
| 9 | 457.8 | 598.3 | 0.00725 | 0.09491 | 1.2025 | -0.0003 | 0.00014 | 12.19 | 11.91 | 11.99 | 12.47 | 12.30 | 0.17 |
| 10 | 496.6 | 716.1 | 0.00878 | 0.11353 | 1.2024 | -0.0003 | 0.00024 | 14.73 | 14.26 | 14.44 | 18.07 | 17.61 | 0.46 |
| 11 | 534.5 | 834.2 | 0.01034 | 0.13184 | 1.2023 | -0.0005 | 0.00035 | 17.36 | 16.60 | 16.92 | 24.82 | 23.89 | 0.93 |
| 12 | 571.8 | 948.8 | 0.01190 | 0.15045 | 1.2029 | 0.0002 | 0.00048 | 20.04 | 18.91 | 19.37 | 32.53 | 30.98 | 1.55 |
| 13 | 609 | 1059.1 | 0.01347 | 0.16754 | 1.2026 | -0.0001 | 0.00063 | 22.68 | 21.09 | 21.83 | 41.30 | 38.56 | 2.74 |
| 14 | 645.8 | 1165.0 | 0.01502 | 0.18402 | 1.2032 | 0.0005 | 0.00080 | 25.38 | 23.23 | 24.23 | 50.87 | 46.77 | 4.11 |
| 15 | 682.3 | 1266.5 | 0.01659 | 0.20019 | 1.2024 | -0.0003 | 0.00100 | 28.00 | 25.21 | 26.66 | 61.61 | 55.09 | 6.53 |
| 16 | 718.6 | 1361.5 | 0.01814 | 0.21454 | 1.2044 | 0.0017 | 0.00120 | 30.78 | 27.21 | 28.98 | 72.79 | 64.17 | 8.62 |
| 17 | 754.5 | 1444.4 | 0.01970 | 0.22797 | 1.2050 | 0.0022 | 0.00143 | 33.24 | 28.90 | 31.31 | 84.95 | 72.38 | 12.57 |
| 18 | 790.1 | 1509.1 | 0.02127 | 0.23773 | 1.2084 | 0.0057 | 0.00167 | 35.55 | 30.40 | 33.53 | 97.44 | 80.10 | 17.34 |
| 19 | 825.8 | 1569.5 | 0.02286 | 0.24750 | 1.2116 | 0.0089 | 0.00193 | 37.83 | 31.82 | 35.72 | 110.60 | 87.75 | 22.85 |
| 20 | 860.5 | 1582.6 | 0.02448 | 0.24841 | 1.2195 | 0.0168 | 0.00223 | 39.19 | 32.60 | 37.74 | 123.43 | 92.08 | 31.35 |
| 21 | 896.1 | 1608.3 | 0.02620 | 0.25391 | 1.2264 | 0.0237 | 0.00254 | 40.97 | 33.59 | 39.84 | 137.56 | 97.78 | 39.77 |
| 22 | 932.1 | 1646.0 | 0.02782 | 0.26062 | 1.2296 | 0.0268 | 0.00284 | 42.79 | 34.60 | 41.87 | 151.90 | 103.75 | 48.16 |
| 23 | 967.6 | 1657.9 | 0.02943 | 0.26092 | 1.2341 | 0.0314 | 0.00317 | 43.92 | 35.18 | 43.77 | 166.06 | 107.25 | 58.80 |
| 24 | 1003.3 | 1665.8 | 0.03104 | 0.26215 | 1.2393 | 0.0366 | 0.00350 | 45.01 | 35.72 | 45.59 | 180.12 | 110.60 | 69.52 |
| 25 | 1039.5 | 1673.1 | 0.03265 | 0.26550 | 1.2429 | 0.0402 | 0.00385 | 45.89 | 36.15 | 47.40 | 194.74 | 113.28 | 81.46 |
| 26 | 1075.6 | 1683.8 | 0.03426 | 0.26520 | 1.2460 | 0.0432 | 0.00419 | 46.84 | 36.61 | 49.18 | 209.58 | 116.18 | 93.39 |
| 27 | 1112.1 | 1691.6 | 0.03587 | 0.26611 | 1.2485 | 0.0458 | 0.00455 | 47.61 | 36.98 | 50.93 | 224.78 | 118.51 | 106.28 |
| 28 | 1148.6 | 1701.1 | 0.03748 | 0.26733 | 1.2508 | 0.0481 | 0.00491 | 48.44 | 37.37 | 52.63 | 240.07 | 121.03 | 119.04 |
| 29 | 1185.2 | 1707.0 | 0.03909 | 0.26978 | 1.2531 | 0.0504 | 0.00527 | 49.13 | 37.68 | 54.29 | 255.40 | 123.07 | 132.33 |
| 30 | 1222.1 | 1710.2 | 0.04070 | 0.27039 | 1.2548 | 0.0521 | 0.00565 | 49.59 | 37.89 | 55.94 | 271.17 | 124.42 | 146.75 |
| 31 | 1258.7 | 1708.8 | 0.04229 | 0.26886 | 1.2587 | 0.0559 | 0.00601 | 50.25 | 38.17 | 57.41 | 285.62 | 126.25 | 159.37 |
| 32 | 1295.6 | 1705.8 | 0.04392 | 0.26855 | 1.2605 | 0.0578 | 0.00640 | 50.46 | 38.25 | 58.98 | 301.46 | 126.77 | 174.69 |
| 33 | 1332.9 | 1711.6 | 0.04552 | 0.27039 | 1.2620 | 0.0593 | 0.00677 | 51.05 | 38.51 | 60.50 | 317.21 | 128.50 | 188.71 |
| 34 | 1370.1 | 1709.0 | 0.04715 | 0.26855 | 1.2650 | 0.0623 | 0.00715 | 51.52 | 38.69 | 61.93 | 332.37 | 129.75 | 202.62 |
| 35 | 1407.5 | 1705.0 | 0.04877 | 0.26886 | 1.2675 | 0.0648 | 0.00754 | 51.83 | 38.81 | 63.34 | 347.71 | 130.53 | 217.18 |
| 36 | 1445.1 | 1695.6 | 0.05043 | 0.27008 | 1.2687 | 0.0660 | 0.00796 | 51.62 | 38.70 | 64.83 | 364.24 | 129.79 | 234.46 |
| 37 | 1482.6 | 1685.2 | 0.05201 | 0.26611 | 1.2726 | 0.0699 | 0.00834 | 51.91 | 38.79 | 66.03 | 377.91 | 130.40 | 247.51 |
| 38 | 1519.7 | 1667.8 | 0.05359 | 0.26337 | 1.2755 | 0.0728 | 0.00874 | 51.62 | 38.63 | 67.29 | 392.37 | 129.31 | 263.06 |
| 39 | 1557.7 | 1654.2 | 0.05520 | 0.26001 | 1.2788 | 0.0761 | 0.00914 | 51.63 | 38.59 | 68.48 | 406.45 | 129.08 | 277.38 |
| 40 | 1595.7 | 1639.3 | 0.05679 | 0.25757 | 1.2810 | 0.0783 | 0.00955 | 51.31 | 38.43 | 69.71 | 421.19 | 127.97 | 293.22 |
| 41 | 1634.1 | 1628.3 | 0.05838 | 0.25574 | 1.2846 | 0.0818 | 0.00995 | 51.50 | 38.47 | 70.81 | 434.53 | 128.28 | 306.26 |
| 42 | 1672.6 | 1607.7 | 0.05996 | 0.25421 | 1.2887 | 0.0860 | 0.01036 | 51.30 | 38.33 | 71.84 | 447.24 | 127.35 | 319.89 |
| 43 | 1711.6 | 1595.0 | 0.06157 | 0.25024 | 1.2921 | 0.0894 | 0.01077 | 51.36 | 38.32 | 72.90 | 460.56 | 127.28 | 333.28 |
| 44 | 1751 | 1574.6 | 0.06320 | 0.24811 | 1.2955 | 0.0928 | 0.01121 | 51.00 | 38.12 | 73.96 | 474.05 | 125.96 | 348.09 |
| 45 | 1790.6 | 1543.6 | 0.06487 | 0.24414 | 1.3012 | 0.0984 | 0.01167 | 50.54 | 37.85 | 74.85 | 485.59 | 124.18 | 361.41 |
| 46 | 1830.9 | 1533.5 | 0.06645 | 0.24200 | 1.3054 | 0.1026 | 0.01207 | 50.90 | 37.97 | 75.75 | 497.29 | 124.93 | 372.35 |
| 47 | 1871.1 | 1514.4 | 0.06804 | 0.23895 | 1.3089 | 0.1062 | 0.01250 | 50.62 | 37.80 | 76.68 | 509.57 | 123.84 | 385.72 |
| 48 | 1912 | 1491.7 | 0.06968 | 0.23438 | 1.3131 | 0.1104 | 0.01295 | 50.26 | 37.59 | 77.57 | 521.53 | 122.48 | 399.05 |
| 49 | 1953.1 | 1472.0 | 0.07129 | 0.23163 | 1.3173 | 0.1146 | 0.01339 | 50.08 | 37.46 | 78.41 | 532.81 | 121.64 | 411.16 |
| 50 | 1994.5 | 1461.6 | 0.07287 | 0.23041 | 1.3210 | 0.1183 | 0.01381 | 50.29 | 37.52 | 79.25 | 544.26 | 121.99 | 422.27 |
| 51 | 2036.1 | 1442.6 | 0.07448 | 0.22827 | 1.3254 | 0.1227 | 0.01425 | 50.17 | 37.42 | 80.02 | 554.98 | 121.32 | 433.66 |
| 52 | 2078.1 | 1407.2 | 0.07616 | 0.22247 | 1.3309 | 0.1282 | 0.01476 | 49.35 | 36.98 | 80.74 | 564.96 | 118.51 | 446.45 |
| 53 | 2120.9 | 1389.8 | 0.07773 | 0.21942 | 1.3348 | 0.1321 | 0.01520 | 49.20 | 36.86 | 81.47 | 575.30 | 117.78 | 457.52 |
| 54 | 2164.1 | 1364.1 | 0.07934 | 0.21515 | 1.3406 | 0.1379 | 0.01567 | 48.95 | 36.69 | 82.07 | 583.74 | 116.67 | 467.08 |
| 55 | 2207.9 | 1342.6 | 0.08095 | 0.21210 | 1.3458 | 0.1431 | 0.01613 | 48.81 | 36.56 | 82.69 | 592.64 | 115.87 | 476.77 |
| 56 | 2252.4 | 1325.8 | 0.08256 | 0.20966 | 1.3500 | 0.1473 | 0.01659 | 48.74 | 36.49 | 83.37 | 602.32 | 115.37 | 486.95 |
| 57 | 2296.9 | 1298.4 | 0.08416 | 0.20538 | 1.3561 | 0.1534 | 0.01707 | 48.41 | 36.27 | 83.86 | 609.42 | 114.01 | 495.41 |
| 58 | 2342.4 | 1267.2 | 0.08574 | 0.20111 | 1.3620 | 0.1593 | 0.01757 | 47.80 | 35.92 | 84.34 | 616.43 | 111.83 | 504.60 |
| 59 | 2388.9 | 1253.4 | 0.08732 | 0.19897 | 1.3662 | 0.1635 | 0.01802 | 47.87 | 35.91 | 84.92 | 625.06 | 111.74 | 513.32 |
| 60 | 2435.4 | 1235.5 | 0.08892 | 0.19653 | 1.3702 | 0.1675 | 0.01850 | 47.63 | 35.75 | 85.53 | 634.00 | 110.78 | 523.22 |
| 61 | 2482.4 | 1216.4 | 0.09048 | 0.19226 | 1.3753 | 0.1726 | 0.01897 | 47.55 | 35.66 | 86.00 | 640.97 | 110.22 | 530.75 |
| 62 | 2530.1 | 1181.5 | 0.09215 | 0.18829 | 1.3827 | 0.1800 | 0.01952 | 46.96 | 35.30 | 86.31 | 645.56 | 108.02 | 537.54 |
| 63 | 2578.6 | 1151.4 | 0.09370 | 0.18280 | 1.3900 | 0.1873 | 0.02002 | 46.61 | 35.06 | 86.54 | 649.03 | 106.55 | 542.47 |
| 64 | 2628.4 | 1135.1 | 0.09528 | 0.18005 | 1.3953 | 0.1926 | 0.02050 | 46.71 | 35.05 | 86.94 | 655.05 | 106.47 | 548.58 |
| 65 | 2678.4 | 1110.7 | 0.09687 | 0.17731 | 1.4010 | 0.1983 | 0.02101 | 46.36 | 34.82 | 87.28 | 660.28 | 105.10 | 555.19 |
| 66 | 2729.4 | 1079.1 | 0.09844 | 0.17273 | 1.4087 | 0.2060 | 0.02155 | 45.93 | 34.54 | 87.43 | 662.45 | 103.38 | 559.07 |

Elastic-Plastic Fracture Toughness Analysis

| | | | |
|----------------|--------------|---------------|------|
| Specimen ID | 5383-FT-3 | Geometry | C(T) |
| Contract | SSC 10624-01 | Orientation | T-L |
| Material | 5383-H116 | Yield (ksi) | 35.4 |
| Temperature(F) | 75.0 | Tensile (ksi) | 53.3 |
| Environment | LAB AIR | Modulus (Msi) | 10.5 |

Specimen Dimensions

| | | | |
|--------------------|-------|------------------|-------|
| Thickness (in) | 0.484 | Notch Depth (in) | 1.100 |
| Net Thickness (in) | 0.377 | Gage Length (in) | 0.200 |
| Width (in) | 2.000 | Alpha Ratio | 1 |
| Pin Spacing (in) | 1.100 | | |

Precrack Parameters

| | | | |
|--------------|-------|----------------------|-----|
| Pmax (lbf) | 300.9 | Stress Ratio | 0.1 |
| Final a (in) | 1.200 | Kmax (ksi sqrt (in)) | 6.1 |
| Pf (lbf) | 1044 | | |

Initial measured crack lengths (in)

| | | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 1.196 | 1.202 | 1.205 | 1.204 | 1.204 | 1.206 | 1.208 | 1.205 | 1.204 |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|

Final measured crack lengths (in)

| | | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 1.388 | 1.407 | 1.414 | 1.414 | 1.426 | 1.420 | 1.419 | 1.410 | 1.391 |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|

| | | | |
|--------------------------------|-------|-------------------------|-------|
| Ave. initial crack length (in) | 1.204 | aoq (in) | 1.205 |
| Ave. final crack length (in) | 1.413 | Compliance Adj. Factor | 1.027 |
| Delta a measured (in) | 0.208 | Effective Modulus (Msi) | 10.8 |
| Delta a predicted (in) | 0.202 | | |

Results

| | |
|-------------------------|-----------------------------|
| J_Q (E1820) | 90.3 lbf-in/in ² |
| $K_{JIC}(E^*J_Q)^{1/2}$ | 32.3 ksi sqrt(in) |

Qualification of Data

| | |
|-------------------------------|---------|
| 7.4.2: precrack length | valid |
| 9.1.4.1; precrack | valid |
| 9.1.4.2; final crack | valid |
| 9.1.5.1; Δa meas | valid |
| 9.1.5.2; Δa pred | valid |
| A9.6.4; # of pnts in reg.A | valid |
| A9.6.4; # of pnts in reg.B | valid |
| A9.8.1; $C_2 < 1$ | valid |
| A9.8.2.1; $a_{0q} - a_0$ | valid |
| A9.8.2.2; # of pnts for J_Q | invalid |
| A9.8.2.2; # of pnts $< J_Q$ | valid |
| A9.3.3.1; correlation | valid |

Qualification of J_Q as J_{IC}

| | |
|-------------------|-------|
| A9.9.1; thickness | valid |
| A9.9.2; ligament | valid |
| A9.9.3; slope | valid |

| Index | Time | Force | Disp1 | Disp2 | Crack | Δa | CTOD | K561 | K1820 | KJ1820 | J1820 | Je | Jpl |
|-------|-------|--------|---------|---------|--------|------------|---------|------------------------|------------------------|------------------------|--------|--------|--------|
| | Sec | lbf | inch | inch | inch | inch | inch | ksi $\sqrt{\text{in}}$ | ksi $\sqrt{\text{in}}$ | ksi $\sqrt{\text{in}}$ | lbf/in | lbf/in | lbf/in |
| 4 | 173.2 | 302.6 | 0.00378 | 0.04883 | 1.2045 | -0.0005 | 0.00003 | 6.96 | 6.90 | 6.91 | 4.14 | 4.13 | 0.01 |
| 5 | 279.4 | 423.1 | 0.00534 | 0.06744 | 1.2038 | -0.0012 | 0.00009 | 9.79 | 9.64 | 9.67 | 8.11 | 8.06 | 0.05 |
| 6 | 314.3 | 538.2 | 0.00687 | 0.08575 | 1.2040 | -0.0010 | 0.00017 | 12.57 | 12.27 | 12.36 | 13.24 | 13.04 | 0.19 |
| 7 | 347.8 | 651.3 | 0.00841 | 0.10376 | 1.2035 | -0.0016 | 0.00027 | 15.37 | 14.83 | 15.06 | 19.67 | 19.06 | 0.61 |
| 8 | 380.8 | 761.9 | 0.00996 | 0.12116 | 1.2040 | -0.0010 | 0.00040 | 18.24 | 17.37 | 17.74 | 27.28 | 26.14 | 1.13 |
| 9 | 413.6 | 869.3 | 0.01150 | 0.13916 | 1.2031 | -0.0020 | 0.00055 | 21.08 | 19.78 | 20.44 | 36.20 | 33.91 | 2.29 |
| 10 | 445.8 | 974.9 | 0.01306 | 0.15442 | 1.2041 | -0.0009 | 0.00072 | 24.11 | 22.23 | 23.09 | 46.20 | 42.82 | 3.38 |
| 11 | 477.8 | 1074.2 | 0.01462 | 0.17029 | 1.2040 | -0.0010 | 0.00091 | 27.04 | 24.49 | 25.76 | 57.49 | 51.97 | 5.52 |
| 12 | 509.3 | 1165.8 | 0.01618 | 0.18616 | 1.2054 | 0.0004 | 0.00112 | 29.99 | 26.65 | 28.34 | 69.60 | 61.54 | 8.05 |
| 13 | 540.6 | 1246.2 | 0.01774 | 0.19775 | 1.2085 | 0.0035 | 0.00134 | 32.92 | 28.66 | 30.86 | 82.54 | 71.20 | 11.33 |
| 14 | 571.1 | 1288.9 | 0.01931 | 0.20386 | 1.2185 | 0.0135 | 0.00158 | 35.39 | 30.24 | 33.13 | 95.10 | 79.27 | 15.82 |
| 15 | 601.8 | 1307.4 | 0.02089 | 0.20630 | 1.2341 | 0.0291 | 0.00181 | 37.81 | 31.67 | 35.13 | 106.97 | 86.91 | 20.06 |
| 16 | 631.3 | 1248.3 | 0.02243 | 0.19775 | 1.2628 | 0.0578 | 0.00204 | 38.87 | 32.11 | 36.51 | 115.53 | 89.38 | 26.15 |
| 17 | 663.5 | 1226.8 | 0.02399 | 0.19470 | 1.2845 | 0.0794 | 0.00227 | 40.84 | 33.09 | 38.02 | 125.28 | 94.88 | 30.40 |
| 18 | 696.1 | 1158.3 | 0.02554 | 0.18372 | 1.3130 | 0.1080 | 0.00252 | 41.69 | 33.33 | 39.14 | 132.74 | 96.27 | 36.47 |
| 19 | 730.8 | 1103.4 | 0.02709 | 0.17487 | 1.3374 | 0.1324 | 0.00279 | 42.64 | 33.62 | 40.27 | 140.57 | 97.98 | 42.58 |
| 20 | 766.3 | 995.5 | 0.02868 | 0.15808 | 1.3770 | 0.1720 | 0.00303 | 43.07 | 33.48 | 40.64 | 143.16 | 97.12 | 46.04 |
| 21 | 806 | 911.6 | 0.03024 | 0.14587 | 1.4063 | 0.2013 | 0.00334 | 42.90 | 33.10 | 41.27 | 147.65 | 94.98 | 52.67 |

Elastic-Plastic Fracture Toughness Analysis

| | | | |
|----------------|--------------|---------------|------|
| Specimen ID | 5383-FT-5 | Geometry | C(T) |
| Contract | SSC 10624-01 | Orientation | T-L |
| Material | 5383-H116 | Yield (ksi) | 35.4 |
| Temperature(F) | 75.0 | Tensile (ksi) | 53.3 |
| Environment | LAB AIR | Modulus (Msi) | 10.5 |

Specimen Dimensions

| | | | |
|--------------------|-------|------------------|-------|
| Thickness (in) | 0.485 | Notch Depth (in) | 2.200 |
| Net Thickness (in) | 0.485 | Gage Length (in) | 0.200 |
| Width (in) | 4.000 | Alpha Ratio | 1 |
| Pin Spacing (in) | 2.200 | | |

Precrack Parameters

| | | | |
|--------------|-------|----------------------|-----|
| Pmax (lbf) | 710.2 | Stress Ratio | 0.1 |
| Final a (in) | 2.400 | Kmax (ksi sqrt (in)) | 9.9 |
| Pf (lbf) | 2148 | | |

Initial measured crack lengths (in)

| | | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 2.338 | 2.370 | 2.387 | 2.398 | 2.402 | 2.407 | 2.405 | 2.394 | 2.375 |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|

Final measured crack lengths (in)

| | | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 2.475 | 2.495 | 2.587 | 2.729 | 2.825 | 2.713 | 2.579 | 2.526 | 2.503 |
| x | | | | x | | | | |

| | | | |
|--------------------------------|-------|-------------------------|-------|
| Ave. initial crack length (in) | 2.390 | aoq (in) | 2.394 |
| Ave. final crack length (in) | 2.618 | Compliance Adj. Factor | 0.975 |
| Delta a measured (in) | 0.228 | Effective Modulus (Msi) | 10.2 |
| Delta a predicted (in) | 0.211 | | |

Results

| | |
|--------------------------|-----------------------------|
| J_a (E1820) | 99.9 lbf-in/in ² |
| $K_{JIC}(E^{*}JQ)^{1/2}$ | 34.0 ksi sqrt(in) |

Qualification of Data

| | |
|-------------------------------|---------|
| 7.4.2; precrack length | valid |
| 9.1.4.1; precrack | valid |
| 9.1.4.2; final crack | invalid |
| 9.1.5.1; Δa meas | valid |
| 9.1.5.2; Δa pred | valid |
| A9.6.4; # of pnts in reg.A | valid |
| A9.6.4; # of pnts in reg.B | valid |
| A9.8.1; $C_2 < 1$ | valid |
| A9.8.2.1; $a_{0q} - a_0$ | valid |
| A9.8.2.2; # of pnts for J_a | valid |
| A9.8.2.2; # of pnts < J_a | invalid |
| A9.3.3.1; correlation | valid |

Qualification of J_a as J_{IC}

| | |
|-------------------|-------|
| A9.9.1; thickness | valid |
| A9.9.2; ligament | valid |
| A9.9.3; slope | valid |

| Index | Time | Force | Disp1 | Disp2 | Crack | Δa | CTOD | K561 | K1820 | KJ1820 | J1820 | Je | Jpl |
|-------|--------|--------|---------|---------|--------|---------|---------|---------------|---------------|---------------|--------|--------|--------|
| | Sec | lbf | inch | inch | inch | inch | inch | ksi sq(r)(in) | ksi sq(r)(in) | ksi sq(r)(in) | lbf/in | lbf/in | lbf/in |
| 18 | 637.1 | 2303.0 | 0.03057 | 0.75714 | 2.3911 | -0.0026 | 0.00164 | 34.94 | 32.13 | 32.08 | 89.19 | 89.46 | -0.27 |
| 19 | 669.1 | 2418.5 | 0.03275 | 0.79742 | 2.3943 | 0.0006 | 0.00192 | 37.16 | 33.85 | 34.46 | 102.89 | 99.28 | 3.61 |
| 20 | 701.1 | 2518.9 | 0.03490 | 0.82825 | 2.3993 | 0.0056 | 0.00221 | 39.27 | 35.42 | 36.72 | 116.86 | 108.75 | 8.11 |
| 21 | 733.1 | 2608.8 | 0.03709 | 0.86243 | 2.4047 | 0.0110 | 0.00252 | 41.28 | 36.88 | 38.98 | 131.66 | 117.89 | 13.76 |
| 22 | 765.1 | 2694.6 | 0.03925 | 0.89172 | 2.4091 | 0.0154 | 0.00285 | 43.22 | 38.26 | 41.16 | 146.85 | 126.86 | 20.00 |
| 23 | 797.6 | 2779.5 | 0.04143 | 0.92651 | 2.4121 | 0.0184 | 0.00319 | 45.13 | 39.58 | 43.36 | 162.94 | 135.79 | 27.15 |
| 24 | 830 | 2864.1 | 0.04358 | 0.94604 | 2.4143 | 0.0206 | 0.00354 | 47.04 | 40.88 | 45.51 | 179.52 | 144.81 | 34.70 |
| 25 | 862.3 | 2936.1 | 0.04578 | 0.96985 | 2.4171 | 0.0235 | 0.00392 | 48.78 | 42.02 | 47.65 | 196.75 | 153.04 | 43.71 |
| 26 | 894.6 | 3003.2 | 0.04794 | 0.98908 | 2.4211 | 0.0274 | 0.00429 | 50.55 | 43.15 | 49.68 | 213.93 | 161.37 | 52.56 |
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| 28 | 959 | 3135.5 | 0.05231 | 1.03882 | 2.4246 | 0.0310 | 0.00510 | 53.87 | 45.21 | 53.81 | 250.95 | 177.16 | 73.78 |
| 29 | 991.3 | 3193.5 | 0.05449 | 1.05621 | 2.4278 | 0.0341 | 0.00550 | 55.51 | 46.19 | 55.78 | 269.61 | 184.93 | 84.68 |
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- (U) The Ship Structure Committee (SSC) identified a lack of information required for structural integrity and damage tolerance analyses of aluminum marine structures. The development of such data is vital in light of the increased use of aluminum alloys in marine construction. Under SSC project SR-1447, Fracture Technology Associates was contracted to characterize, through experimental fracture mechanics, the fatigue crack growth (FCG) resistance and fracture toughness of three aluminum alloys (5083, 5086, 5383) used in marine structural applications. Fatigue crack growth testing was performed following ASTM Standard E 647-00 in laboratory air at room temperature and in simulated ocean water per ASTM Standard D 1141. Non-linear fracture toughness testing was performed in accordance with ASTM Standard E 1820-01 in laboratory air at room temperature. For the three different grades of material, the difference in fatigue crack growth rate in laboratory air was negligible. In simulated seawater environment, AA5086 showed a slightly superior performance. In addition, all samples showed the same ranking of toughness with the 5086 showing the highest toughness, followed by 5083 and then 5383.
- (U) Le Comité sur la structure des navires (CSN) a identifié des lacunes dans l'information requise pour l'analyse de l'intégrité structurale et de la tolérance aux avaries des structures maritimes en aluminium. Le développement de ces données est vital en ce sens que l'on utilise de plus en plus les alliages d'aluminium dans la construction maritime. Dans le cadre du projet SR-1447 du SSC, on a donné un contrat à la société Fracture Technology Associates pour qu'elle caractérise, grâce à des expériences de mécanique de la rupture, la résistance à la propagation des fissures en fatigue (PFF) et la ténacité (résistance à la propagation brutale de fissures) de trois alliages d'aluminium (5083, 5086, 5383) utilisés dans des applications structurales maritimes. Des essais sur la propagation des fissures en fatigue ont été réalisés, conformément à la norme ASTM Standard E 647-00, hors de l'eau et en laboratoire, à la température ambiante, ainsi que dans un milieu marin simulé en suivant la norme ASTM Standard D 1141. Des essais sur la résistance à la propagation de fissures non linéaires ont été réalisés, conformément à la norme ASTM Standard E 1820-01, hors de l'eau et en laboratoire, à la température ambiante. Pour les trois nuances d'alliages différentes, la différence dans le taux de propagation des fissures en laboratoire et hors de l'eau était négligeable. Dans le milieu marin simulé, l'alliage AA5086 a démontré une performance légèrement supérieure. En outre, tous les échantillons se sont situés à l'intérieur de la même plage de ténacité, l'alliage 5086 étant le plus résistant, suivi de l'alliage 5083, puis de l'alliage 5383.
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- (U) Fracture crack growth, fracture toughness, aluminum, marine

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